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REPORT NO. P68-06

# STUDY AND DEVELOPMENT OF A MATHEMATICAL ANALYSIS FOR THE PERFORMANCE ASSESSMENT OF SPACE COMMUNICATION SYSTEM PARAMETERS

By L. S. Stokes, K. L. Brinkman  
and  
W. K. Pratt

MARCH 1968

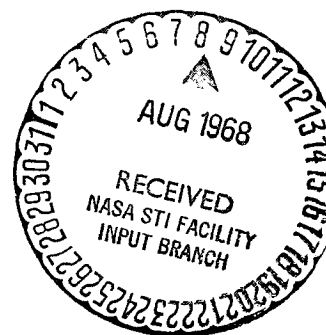
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ELECTRONICS RESEARCH CENTER  
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION  
CAMBRIDGE, MASSACHUSETTS

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## CONTENTS

| Section |   | Page |
|---------|---|------|
| 1.0     | SUMMARY . . . . .   | 1    |
| 1.1     | Program Goals . . . . .   | 1    |
| 1.2     | Sensitivity Analysis . . . . .  | 4    |
| 1.3     | COPTRAN Summary . . . . .   | 5    |
| 1.4     | Interface Equipment Summary . . . . .   | 11   |
| 2.0     | INTRODUCTION . . . . .  | 15   |
| 3.0     | SYMBOLS . . . . .   | 19   |
| 3.1     | COPS Nomenclature . . . . .   | 19   |
| 3.2     | COPTRAN Instruction Mnemonics . . . . .   | 33   |
| 4.0     | USER'S MANUAL FOR COPTRAN, A METHOD OF<br>OPTIMUM COMMUNICATION SYSTEM DESIGN . . . . . | 39   |
| 4.1     | Introduction . . . . .  | 39   |
| 4.2     | COPTRAN Programming Structure . . . . .   | 43   |
| 4.3     | COPTRAN Use . . . . .   | 47   |
| 4.4     | Program Examples . . . . .  | 69   |
| 4.5     | Library of Nominal System Burdens<br>Data for COPTRAN . . . . .                         | 119  |
| 4.6     | Automatic COPTRAN Burden Data Selection Logic . . . . .                                 | 135  |
| 4.7     | COPTRAN Coding Sheets and Data Forms . . . . .  | 145  |
| 5.0     | INTERFACE EQUIPMENT SUMMARY . . . . .   | 153  |
| 5.1     | Introduction . . . . .  | 153  |
| 5.2     | Possible Systems . . . . .  | 154  |
| 5.3     | Software Requirements . . . . .   | 156  |
| 5.4     | Available Equipment . . . . .   | 157  |
| 6.0     | CONTRACT END ITEM . . . . .   | 163  |
| 6.1     | Introduction . . . . .  | 163  |
| 6.2     | Phase I (NAS 12-566 Statement of Work) . . . . .  | 163  |
| 6.3     | Proposed Phase II . . . . .   | 165  |
| 6.4     | Potential Phase III . . . . .   | 170  |

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## ILLUSTRATIONS

| Figure |  | Page |
|--------|--|------|
| 1-1    | COPTRAN Programming . . . . .  | 8    |
| 1-2    | Remote Configurations for Computer Control . .                                 | 13   |
| 2-1    | Master Program Plan for Contract NAS 12-566 . .                                | 16   |
| 4-1    | COPTRAN Programming . . . . .  | 42   |
| 4-2    | COPTRAN Job Deck Structure . . . . .   | 47   |
| 4-3    | COPTRAN Coding Sheet A . . . . .   | 49   |
| 4-4    | COPTRAN Coding Sheet B . . . . .   | 58   |
| 4-5    | COPTRAN Coding Sheet C . . . . .   | 59   |
| 4-6    | "REPEAT" Example . . . . .   | 66   |
| 4-7    | Increment (NCRMNT) Example . . . . .   | 67   |
| 5-1    | Teletype/Plotter Remote Station . . . . .                                      | 155  |
| 5-2    | Keyboard/CRT Alphanumeric Output/Plotter/<br>Printer Remote Stations . . . . . | 155  |
| 5-3    | Complete Remote Graphic Processing<br>Remote Terminal . . . . .                | 156  |

TABLES

| <u>Table</u> |  | <u>Page</u> |
|--------------|--|-------------|
| I-I          | Summary of Programs Goals for NAS 12-566 . . .   | 2           |
| I-II         | Summary of Proposed Follow on Analysis . . .   | 3           |
| I-III        | Sensitivity Analysis Summary Results for Radio<br>Communication Systems Optimization Program (ROPS)-<br>Cost Optimized . . . . .             | 5           |
| I-IV         | Sensitivity Analysis Summary Results for Heterodyne<br>Detection Optical Receiver Optimization Program (HOPS)-<br>Cost Optimized . . . . .   | 6           |
| I-V          | Sensitivity Analysis Summary Results for Radio<br>Communication System Optimization Program (ROPS)-<br>Weight Optimized . . . . .            | 7           |
| I-VI         | Sensitivity Analysis Summary Results for Heterodyne<br>Detection Optical Receiver Optimization Program (HOPS)-<br>Weight Optimized . . . . . | 9           |
| I-VII        | Sensitivity Analysis Summary . . . . .   | 10          |
| I-VIII       | Equipment Summary . . . . .  | 14          |
| IV-I         | Complete Listing of COPTRAN Instructions Mnemonics   | 50          |
| IV-IIa       | COPTRAN Data . . . . .   | 60          |
| IV-IIb       | COPTRAN Data . . . . .   | 61          |
| IV-IIc       | COPTRAN Data . . . . .   | 64          |
| V-I          | Equipment Summary . . . . .  | 158         |
| V-II         | List of Manufactorers . . . . .  | 159         |
| VI-I         | Analysis for Deep Space Communications . . . . .   | 171         |

## 1.0 SUMMARY

The Hughes Aircraft Company entered into a six month contract, NAS 12-566, with the Electronics Research Center of NASA on 17 July 1967. This report is the Final Technical Report for that contract. In this summary section, four parts are given which form summaries of: 1) the contract goals and how they were met, 2) the sensitivity analysis, 3) the COPTRAN program and 4) the computer interface equipment summary.

### 1.1 Program Goals

The complete statement of work for contract NAS 12-566 is given in Section 6.0 and is summarized in this section as Table I-I. It is the purpose of this section to summarize these goals and to note where the documentation of their completion may be found, this now follows.

Under contract NAS 5-9637, between the Hughes Aircraft Company and GSFC-NASA, mathematical models for several types of communication were developed for transmission using laser and radio. These were combined into a single computer program, COPS, under contract NAS 12-566. The COPS program is documented in the Interim Technical Report for this contract, dated 15 October 1967. It contained the stops, detection methods and fixed values required and was delivered in the form of a FORTRAN deck also. The values for the many parameters in the COPS program were derived from actual experimental data as far as possible.

The flexible input/output investigation has resulted in COPTRAN, which enables the COPS program to be used easily. COPTRAN is documented in Section 4.0 of this report and summarized in Section 1.3 of this report. It enables a user to evaluate and select future work (Item 1d of Table I-I) and goes somewhat beyond the recommendations required by Item 2 (Table I-I).

The sensitivity analysis (Item 1f of Table I-I) was completed during the first half of the contract period and is documented in the Interim Technical Report. A summary of that analysis is contained in this report in Section 1.2.

TABLE I-I  
SUMMARY OF PROGRAM GOALS FOR NAS 12-566

1. Extend Math Model begun under Contract NAS 5-9637
  - a. It shall contain a method of evaluating and selecting future work.
  - b. Additional stops, detection method, fixed values shall be included. A FORTRAN deck shall be delivered.
  - c. Use of actual experimental data shall be included in the math model.
  - d. The math model shall have a flexible input/output.
  - e. Optimization criteria shall be reviewed.
  - f. A sensitivity analysis shall be performed.
2. Investigate Executive Models

Look at possible output forms, list steps for obtaining an executive program. A recommended approach shall be given. Factors to be included are:

  - a. Investigate remote computer usage
  - b. Investigate batch usage
3. Evaluate a follow-on math analysis considering the following:
  - a. The optimization criteria
  - b. The model versatility required
  - c. Identification of parameters and rate their importance
  - d. Determination of the applicability and specifications for future remote and batch analysis.

In addition to the development of COPTRAN (see Section 1.3), a second effort was expended to investigate executive use of the communications analysis. That effort was determining the equipment which would be appropriate as interface equipment between the user and the computer. The documentation of that effort is given in Section 5.0 of this report and is summarized in Section 1.4 of this report.

The evaluation of a follow-on mathematical analysis is given in Section 6.0 of this report (Item 3 of Table I-I). It is summarized in Table I-II.

TABLE I-II  
SUMMARY OF PROPOSED FOLLOW ON ANALYSIS

- |  |
|--|
| <ol style="list-style-type: none"><li>1. <u>Model Refinement, versatility</u><ol style="list-style-type: none"><li>a. Inclusion of PPM (1.06<math>\mu</math>, 0.84<math>\mu</math>, 0.51<math>\mu</math>)</li><li>b. Documentation of basic mathematics used in the methodology</li><li>c. Visit recognized authorities to check values used in methodology</li><li>d. Implement a discrete point input program</li><li>e. Represent parameter burdens by more than 3 constants</li><li>f. Investigate certain promising implementation techniques such as<ul style="list-style-type: none"><li>Solid state microwave sources</li><li>Antenna arrays</li><li>Power supplies</li></ul></li></ol></li><li>2. <u>Executive Model</u><ol style="list-style-type: none"><li>a. Develop a specific executive model No. 1</li><li>b. Develop a specific executive model No. 2</li><li>c. Develop an executive model check</li></ol></li><li>3. <u>Console for Executive/Computer Interface</u><p>Design a console for executive/computer interface for executive model No. 2</p></li><li>4. <u>Review optimization criteria</u></li><li>5. <u>Deviation Analysis</u> — determine the worth of extending the state of the art in certain technology areas.</li></ol> |
|--|

## 1.2 Sensitivity Analysis

The sensitivity analysis of the COPS program (Communication system Optimization Program with Stops) was designed to determine the sensitivity of each of the Major System Parameter values; transmitted power,  $P_{TO}$ ; transmitting antenna diameter,  $d_{TO}$ ; and receiving antenna diameter,  $d_{RO}$ ; to variations in each of the 25 constants used in the burden relationships. Analytical relationships were derived and the entire sensitivity analysis implemented into the computer. Four major cases were completed to determine the sensitivity of the optimized parameter values,  $P_{TO}$ ,  $d_{TO}$  and  $d_{RO}$ , to each of the 25 constants. The four major cases run were 1) a 2.3 GHz system, cost optimized, 2) a 10.6μ system, cost optimized, 3) a 2.3 GHz system, weight optimized, and 4) a 10.6μ system, weight optimized. Summary tables, Tables I-III through I-VI, show the variables which caused the greatest influence. These tables show three general areas of sensitivity. The first is the rather large effect various exponent values ( $m_T$ ,  $n_T$ , etc.) have when they are varied as compared to the linear constants ( $K_{WT}$ ,  $K_{SA}$ , etc.). The second is that all constants used to describe the power output have a strong effect. This is due to the influence the power output has on the power supply, the power prime source and the heat radiators. The third is the case of the optical calculation or HOPS in which the variation in the acquisition and tracking constants has a strong effect.

Two other observations should be made. The first is the sensitivity variation with bit rate. Since most burden values occur in only one term of a burden equation, the bit rate at which that term is dominant in the equation is the bit rate where a variation in the parameter value has the greatest effect. The second is a change in parameter value such as  $m_T$ , which is in the equation describing  $d_T$ , affects  $d_{TO}$  much more than it affects  $d_{RO}$  or  $P_{TO}$ . That is, there is relatively little crosstalk.

In addition to Tables I-III to I-VI, which summarize the most sensitive parameters, Table I-VII indicates the sensitivity range for all the parameters in the COPS program.

TABLE I-III  
SENSITIVITY ANALYSIS SUMMARY RESULTS FOR RADIO  
COMMUNICATION SYSTEMS OPTIMIZATION PROGRAM  
(ROPS) – COST OPTIMIZED

| 5 Percent<br>Change in | Percent Change in Optimized Parameters |                |              | Variable Description   |
|------------------------|--|----------------|--------------|--|
|                        | $d_{TO}$                               | $P_{TO}$       | $d_{RO}$     |  |
| $m_R$                  | 0.74 to 0.68*                          | 1.28 to 1.35   | 36.0 to 46.7 | Exponent relating receiver antenna fabrication cost to diameter    |
| $n_R$                  | 0.74 to 0.68                           | 1.28 to 1.35   | 36.0 to 46.7 | Exponent relating receiver antenna fabrication weight to diameter  |
| $g_T$                  | 0.99 to 0.91                           | -19.3 to -48.3 | 0.64 to 0.68 | Exponent relating transmitter fabrication cost to power            |
| $h_T$                  | 0.99 to 0.91                           | -19.3 to -48.3 | 0.64 to 0.68 | Exponent relating transmitter fabrication weight to power          |
| $m_T$                  | -16.0 to -28.9                         | 2.73 to 1.42   | 1.01 to 0.52 | Exponent relating transmitter antenna fabrication cost to diameter |
| $n_T$                  | -4.77 to -8.61                         | 0.82 to 0.43   | 0.3 to 0.157 | Exponent relating transmitter antenna weight to diameter           |
| $k_e$                  | 0.00                                   | -4.7           | 0.00         | Transmitter power efficiency                                       |

\*The maximum and minimum values over a bit rate range of 1 b/s to  $10^7$  b/s.

### 1.3 COPTRAN Summary

The analysis of a communication link for space involves many practical considerations framed within the bounds of the appropriate transmission equation. The practical considerations and the appropriate equations have been combined in a single set of mathematical expressions which provide an optimum\* solution to the problem. The mathematical expressions or the methodology is quite involved and its solution is tedious. A first step towards alleviating these drawbacks was to implement the methodology on a computer

---

\*Lightest weight or lowest cost.

TABLE I-IV  
SENSITIVITY ANALYSIS SUMMARY RESULTS FOR HETERODYNE  
DETECTION OPTICAL RECEIVER OPTIMIZATION PROGRAM  
(HOPS) – COST OPTIMIZED

| 5 Percent<br>Change in | Percent Change in Optimized Parameters |                |                  | Variable Description   |
|------------------------|--|----------------|------------------|--|
|                        | $d_{TO}$                               | $P_{RO}$       | $d_{RO}$         |  |
| $q_T$                  | -45.1 to -5.2*                         | 3.77 to -5.04  | 1.89 to -4.8     | Exponent relating transmitter acquisition and track system fabrication cost to transmitter beamwidth |
| $m_R$                  | 1.92 to 0.92                           | 0.58 to 1.57   | -25.3 to -32.8   | Exponent relating receiver antenna fabrication cost to diameter                                      |
| $n_R$                  | 1.92 to 0.92                           | 0.58 to 1.57   | -25.3 to -32.8   | Exponent relating receiver antenna fabrication weight to diameter                                    |
| $g_T$                  | 1.92 to 0.94                           | -13.5 to -28.5 | 0.29 to 0.79     | Exponent relating transmitter fabrication cost to power  |
| $h_T$                  | 1.92 to 0.94                           | -13.5 to -28.5 | 0.29 to 0.79     | Exponent relating transmitter fabrication weight to power  |
| $n_T$                  | 0.0056 to -20.1                        | 0.0049 to 4.2  | 0.0024 to 2.4    | Exponent relating transmitter antenna weight to diameter   |
| $K_{AT}$               | -16.2 to -1.39                         | -0.026 to -1.5 | 0.0133 to 1.66   | Constant relating transmitter tracking equipment fabrication cost to transmitter beamwidth           |
| $m_T$                  | 0.0012 to -4.3                         | 0.01 to 0.67   | 0.00052 to 0.335 | Exponent relating transmitter antenna fabrication cost to diameter                                   |
| $K_{SA}$               | 0.0054 to 1.75                         | -3.66 to -3.49 | 0.0015 to 0.2    | Cost per unit weight for transmitter system equipment  |

\*The maximum and minimum values over a bit rate range of 1 b/s to  $10^7$  b/s.

TABLE I-V  
SENSITIVITY ANALYSIS SUMMARY RESULTS FOR RADIO  
COMMUNICATION SYSTEM OPTIMIZATION PROGRAM  
(ROPS) - WEIGHT OPTIMIZED

| 5 Percent<br>Change in | Percent Change in<br>Optimized Parameter |               | Variable Description                                      |
|------------------------|--|---------------|---|
|                        | $d_{TO}$                                 | $P_{TO}$      |   |
| $n_T$                  | -19.5 to -39.6*                          | 2.5           | Exponent relating transmitter antenna weight to diameter  |
| $h_T$                  | 1.25                                     | -5.6 to -45.9 | Exponent relating transmitter fabrication weight to power |
| $K_{SA}$               | -2.5                                     | -5.0          | Cost per unit weight for transmitter system equipment     |
| $k_e$                  | 0  | -4.7          | Transmitter power efficiency                              |

\*The maximum and minimum values over a bit rate range of 1 b/s to  $10^7$  b/s.

(COPS program). This produced solutions easily but required the user have considerable knowledge of the computer or work through someone who did. An important step has been taken to reduce the amount of computer knowledge needed by the user. This has been done by developing COPTRAN, a special input interface method for the COPS computer program. COPTRAN allows the user to instruct the computer in terms which are familiar to him. These instructions are then key punched onto computer cards, combined with the previously prepared card decks, and run on a computer. The computer output is in the form of printed answers and in the form of graphical plots. Figure 1-1 summarizes the steps in the solution of a communications problem.

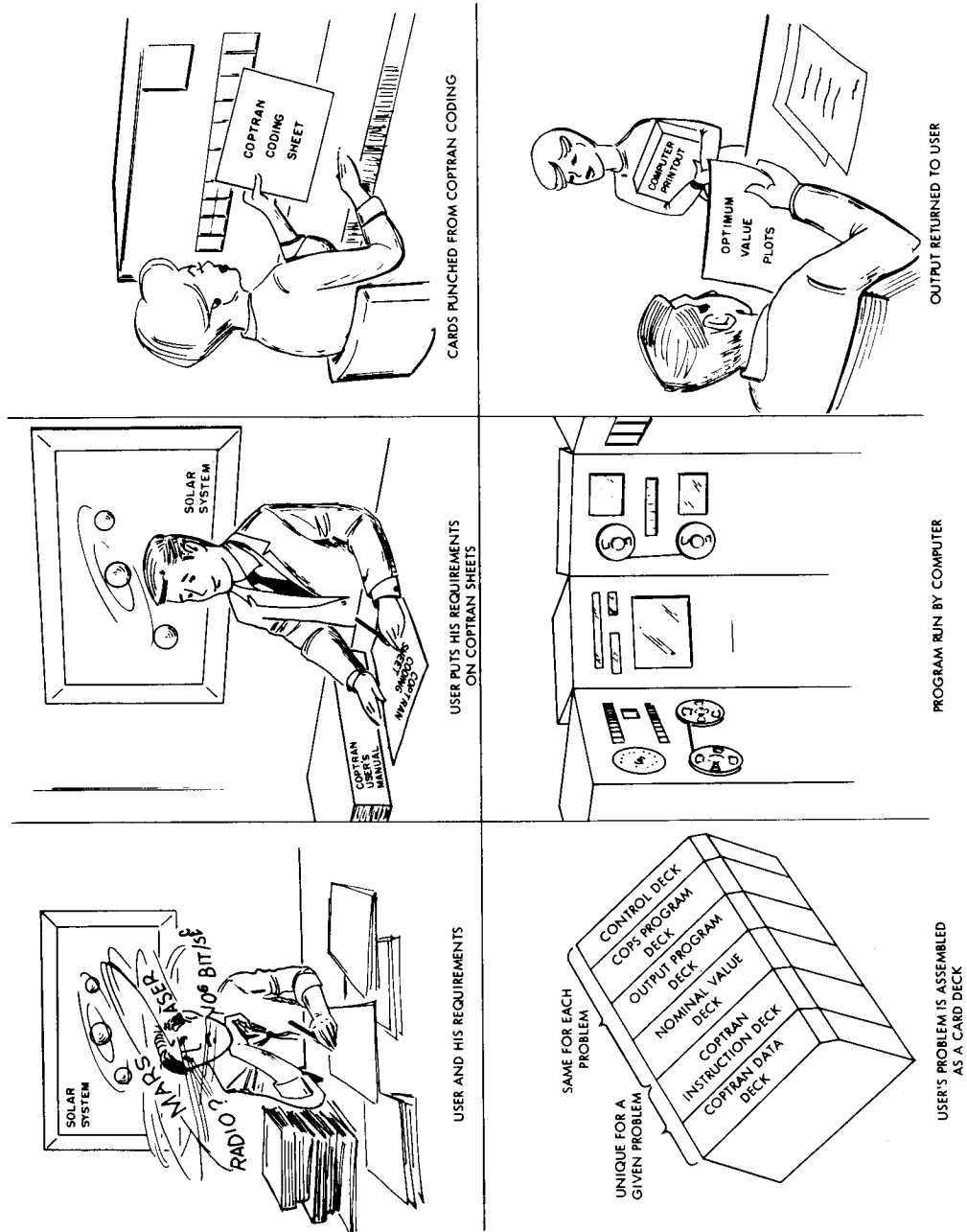


Figure 1-1. COPTRAN Programming

TABLE I-VI  
SENSITIVITY ANALYSIS SUMMARY RESULTS FOR HETERODYNE  
DETECTION OPTICAL RECEIVER OPTIMIZATION PROGRAM  
(HOPS) - WEIGHT OPTIMIZED

| 5 Percent<br>Change in | Percent Change in<br>Optimized Parameter |               | Variable Description                                      |
|------------------------|--|---------------|---|
|                        | $d_{TO}$                                 | $P_{TO}$      |   |
| $n_T$                  | -6.93 to -27.0*                          | 2.5           | Exponent relating transmitter antenna weight to diameter  |
| $h_T$                  | 1.25                                     | 33.7 to -28.4 | Exponent relating transmitter fabrication weight to power |
| $K_{SA}$               | -2.5                                     | -5.0          | Cost per unit weight for transmitter system equipment     |
| $k_e$                  | 0  | -3.45         | Transmitter power efficiency                              |

\*The maximum and minimum values over a bit rate range of 1 b/s to  $10^7$  b/s.

Section 4.0 of this report is a User's Manual for COPTRAN, a Method of Optimum Communication System Design. It presents the COPTRAN language, which is used to instruct the computer using terms familiar to the user. The user must only answer a series of questions pertinent to his problem.

For instance one question is: "Where is the transmitter?" The answer will be either "in space" or "on the earth." Following this question is a choice of two six letter mnemonics and their meanings. One of these, SPXMTR, may be chosen to tell the COPS methodology through the COPTRAN buffer language that the transmitter (XMTR) is located in space (SP).

In addition to describing how to instruct the COPTRAN program, the User's Manual describes how to insert data points which may be of particular concern to the user.

TABLE I-VII  
SENSITIVITY ANALYSIS SUMMARY

| 5 Percent Change in  | Percent Change in Optimized Parameters |                |              |                |                |                |                       |               |               |               |          |          |
|--|--|----------------|--------------|----------------|----------------|----------------|-----------------------|---------------|---------------|---------------|----------|----------|
|  | ROPS Cost Optimized                    |                |              |                |                |                | ROPS Weight Optimized |               |               |               |          |          |
|  | $d_{TO}$                               | $P_{TO}$       | $d_{RO}$     | $d_{TO}$       | $P_{TO}$       | $d_{RO}$       | $d_{TO}$              | $P_{TO}$      | $d_{TO}$      | $P_{TO}$      | $d_{TO}$ | $P_{TO}$ |
| $m_T$  | -16 to -29                             | 2.7 to 1.4     | 1.0 to 0.5   | 0 to -4.3      | 0.01 to 0.67   | 0 to 0.33      |                       |               |               |               |          |          |
| $n_T$  | -4.7 to -8.6                           | 0.8 to 0.4     | 0.3 to 0.2   | 0 to -20.1     | 0 to 4.2       | 0 to 2.4       | -19.4 to -39.6        | 2.5           | -6.9 to -27.0 | 2.5           |          |          |
| $q_T$  | 0.9 to 0.01                            | 0.4 to 0.01    | 0.15 to 0    | -45.1 to -5.28 | 3.77 to -5.0   | 1.89 to -4.8   |                       |               |               |               |          |          |
| $m_R$  | 0.7 to 0.67                            | 1.3 to 1.35    | -36 to -47   | 1.9 to 0.9     | 0.58 to 1.57   | -25.3 to -32.8 |                       |               |               |               |          |          |
| $n_R$  | 0.7 to 0.67                            | 1.3 to 1.35    | -36 to -47   | 1.9 to 0.9     | 0.58 to 1.57   | -25.3 to -32.8 |                       |               |               |               |          |          |
| $g_T$  | 0.99 to 0.91                           | -19.3 to -48.3 | 0.64 to 0.67 | 1.9 to 0.92    | -13.5 to -28.5 | 0.29 to 0.78   | 1.25                  | -5.6 to -45.9 | 1.25          | 33.7 to -28.4 |          |          |
| $h_T$  | 0.99 to 0.91                           | -19.3 to -48.3 | 0.64 to 0.67 | 1.9 to 0.92    | -13.5 to -28.5 | 0.29 to 0.78   |                       |               |               |               |          |          |
| $K_{PT}$   | 0                                      | 0.133          | 0            | 0              | 0              | 0              |                       |               |               |               |          |          |
| $K_{WT}$   | 0                                      | 0.181          | 0            | 0              | -1.15          | 0              | 0                     | -0.181        | 0             | 0.181         |          |          |
| $K_{SA}$   | -0.4 to -0.43                          | -3.2           | 0            | 0 to -1.75     | -3.5           | 0 to 0.2       | -2.5                  | -5.0          | -2.5          | -5.0          |          |          |
| $K_{WST}$  | -0.25                                  | -3.0           | 0            | 0 to -0.23     | -2.33          | 0 to -0.02     | -1.464                | -4.67         | -0.326        | -3.25         |          |          |
| $K_e$  | 0                                      | -4.7           | 0            | 0              | -3.85          | 0              | 0                     | -4.7          | 0             | -3.45         |          |          |
| $K_X$  | 0                                      | -0.038         | 0            | 0              | -0.13          | 0              | 0                     | -0.06         | 0             | -0.177        |          |          |
| $K_{ST}$   | -0.141                                 | -1.66          | 0            | 0 to -0.127    | -1.3           | 0 to 0.01      |                       |               |               |               |          |          |
| $K_H$  | 0                                      | 0              | 0            | 0              | 0              | 0              |                       |               |               |               |          |          |
| $K_{q_T}$  | -1.92                                  | 0.17 to 0      | 0.06 to 0    | 0 to -0.4      | 0 to 0.09      | 0 to 0.04      |                       |               |               |               |          |          |
| $K_{WAT}$  | -0.47                                  | 0.04 to 0      | 0.01 to 0    | 0 to -1.4      | 0 to 0.3       | 0 to 0.15      | -1.9                  | 0             | -1.85         | 0             |          |          |
| $K_{d_T}$  | -0.57                                  | 0.05 to 0      | 0.02 to 0    | 0 to -1.88     | 0 to 0.4       | 0 to 0.2       | -2.5                  | 0             | -2.5          | 0             |          |          |
| $K_{POT}$  | -0.39                                  | 0.03 to 0      | 0.01 to 0    | 0 to -0.35     | 0 to 0.07      | 0 to 0.039     | -1.46                 | 0             | -0.326        | 0             |          |          |
| $K_{AT}$   | -0.3 to 0                              | -1.48 to 0.01  | -0.5 to 0    | -16.6 to -1.39 | -0.02 to -3.3  | 0.01 to 1.66   |                       |               |               |               |          |          |
| $K_{q_R}$  | 0                                      | 0              | -1.85        | 0              | 0              | -2.25          |                       |               |               |               |          |          |
| $K_{d_R}$  |  |                |              | 0              | 0              | -0.248         |                       |               |               |               |          |          |
| $K_{WAR}$  |  |                |              | 0              | 0              | -0.248         |                       |               |               |               |          |          |
| $K_{PQR}$  |  |                |              | 0              | 0              | -0.248         |                       |               |               |               |          |          |
| $K_{SR}$   |  |                |              | 0              | 0              | -0.248         |                       |               |               |               |          |          |
| Variable Description   |  |                |              |                |                |                |                       |               |               |               |          |          |
| Exponent relating transmitter antenna fabrication cost to diameter   |  |                |              |                |                |                |                       |               |               |               |          |          |
| Exponent relating transmitter antenna weight to diameter   |  |                |              |                |                |                |                       |               |               |               |          |          |
| Exponent relating transmitter acquisition and track system fabrication cost to transmitter beamwidth to diameter |  |                |              |                |                |                |                       |               |               |               |          |          |
| Exponent relating receiver antenna fabrication cost to diameter  |  |                |              |                |                |                |                       |               |               |               |          |          |
| Exponent relating receiver antenna weight to diameter  |  |                |              |                |                |                |                       |               |               |               |          |          |
| Exponent relating transmitter fabrication cost to power  |  |                |              |                |                |                |                       |               |               |               |          |          |
| Exponent relating transmitter weight to transmitter power  |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating transmitter weight to transmitter power  |  |                |              |                |                |                |                       |               |               |               |          |          |
| Cost per unit weight for transmitter system equipment  |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating transmitter power supply weight to power requirement   |  |                |              |                |                |                |                       |               |               |               |          |          |
| Transmitter power efficiency   |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating transmitter heat exchanger weight to transmitter power dissipation                             |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating transmitter power supply fabrication cost to power requirement                                 |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating transmitter heat exchanger fabrication cost to transmitter power dissipation                   |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating transmitter antenna fabrication cost to transmitter aperture diameter                          |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating transmitter tracking equipment weight to transmitter antenna weight                            |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating transmitter antenna weight to transmitter aperture diameter                                    |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating transmitter acquisition and track equipment power requirement to equipment weight              |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating transmitter tracking equipment fabrication cost to transmitter beamwidth                       |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating receiver antenna fabrication cost to receiver aperture diameter                                |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating receiver antenna weight to receiver aperture diameter  |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating receiver tracking equipment weight to receiver antenna weight                                  |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating receiver acquisition and track equipment power requirement to equipment weight                 |  |                |              |                |                |                |                       |               |               |               |          |          |
| Constant relating receiver power supply fabrication cost to power requirement                                    |  |                |              |                |                |                |                       |               |               |               |          |          |

Four examples of COPTRAN use are given. Those examples exercise all the types of flexibilities that are incorporated into COPTRAN to aid the user in the solution of his problem.

The COPTRAN program is arranged such that "nominal" values are used unless otherwise specified by the user. The COPTRAN User's Manual documents these nominal data sets, notes the provision in the COPTRAN language for additional nominal sets to be defined by the user and documents the logic used in the selection of nominal data.

#### 1.4 Interface Equipment Summary

The COPS digital computer program can be controlled using COPTRAN, a buffer language between the user and the computer. This program presently operates in a batch processing mode. Program controls and data are input by means of a prepared card deck and the program operates on the input to produce tabular and graphical outputs.

To fully utilize the computer as a design tool, an interactive console terminal should be provided. Then with the appropriate conversational software, the designer will be able to control the computer directly using the COPTRAN program through a console. Results could be made available immediately and changes in input parameters could be made quickly to determine their effects. The user would converse with the computer in terms familiar to him or merely supply information to the computer as required in a question-and-answer session.

There is a wide spectrum of capability which can be made available to the user as interface equipment. Features which can be provided at a remote terminal include:

|         |                             |
|---------|-----------------------------|
| Input:  | Keyboard                    |
|         | Light pen graphics          |
|         | Stylus graphics             |
| Output: | Printer (High-or-Low-Speed) |
|         | Plotter                     |
|         | CRT Alpha-Numerics          |
|         | CRT Display graphics        |

These features may be combined in various ways to achieve many different degrees of sophistication. The configuration might run from something as simple as a teletype and plotter to a general purpose graphic display terminal with independent software, central processing unit, light pen, high speed printer, and graphic hard copy capability. (See Figure 1-2.)

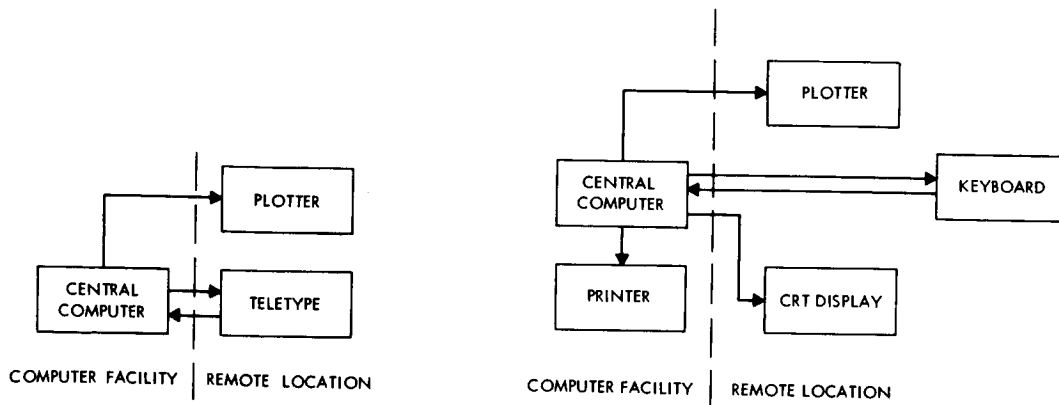
A survey of currently available equipment which could form a remote terminal has been made. The assumptions were: 1) the computer used would be a Honeywell DDP 516, with possible conversion at a later date to a larger computer in the SDS Sigma 5 class and 2) input/output capability should conform as closely as possible to the requirements of COPS and COPTRAN.

A summary of the input/output equipment investigated is given in Table I-VIII. As noted in the table further descriptive material of the various equipments is given in several appendices at the end of this report.

Perhaps the most prudent initial approach is to use a terminal similar to that given in Figure 1-2a, a typewriter or teletype with a plotter. There are two reasons for this choice: 1) it provides lowest cost and ease of interfacing, and 2) with a small initial investment, an operational conversational mode can be made operational.

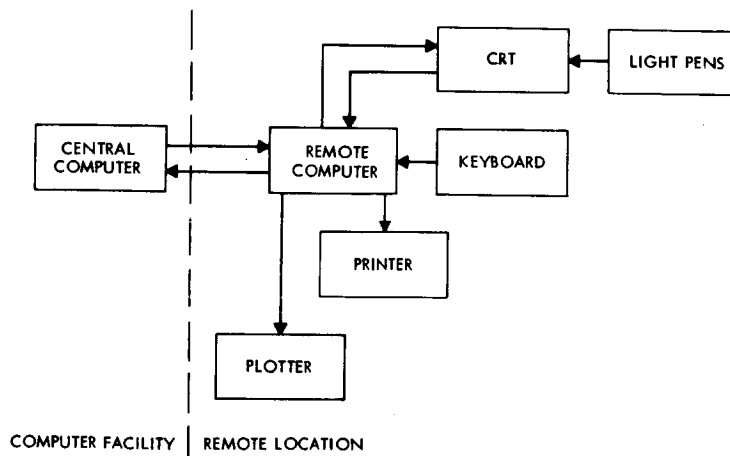
The most logical unit to serve as the interactive device is Honeywell's ASR33. It undoubtedly would present the least interfacing problem and could be either the existing console teletype or logically be made to appear as the same. Hard copy graphic output would be produced on a CalComp plotter. The present DDP-516 system configuration does not include such a plotter however, a standard interface to the DDP-516 does exist and there is a possibility that a plotter will be added to the ERC computer installation.

Because the DDP-516 system is at the outset a graphics oriented system, another option well worth considering is the use of an IDI display device (at a cost of about \$15,000).



a. Teletype/Plotter Remote Station

b. Keyboard/CRT Alphabetic Output/Plotter/Printer Remote Station



c. Complete Remote Graphic Processing Remote Terminal

Figure 1-2. Remote Configurations for Computer Control

TABLE I-VIII  
EQUIPMENT SUMMARY

| Name                       | 1. Description  | 2. Approximate Cost    | 3. Alpha-numeric Input | 4. Alpha-numeric Output | 5. Graphic Input | 6. Graphic Output | 7. Produces Hard Copy | 8. Software Supplied | 9. Program-mable Remote Processor |
|----------------------------|---|------------------------|------------------------|-------------------------|------------------|-------------------|-----------------------|----------------------|-----------------------------------|
| AGT/10<br>AGT/30<br>AGT/50 | This is a family of highly sophisticated graphics terminals - very flexible and expensive. Extensive software is provided for remote processor. AGT/10 probably sufficient for conversational COPS - later version. | 60 K<br>125 K<br>175 K | KBD                    | a. PRT<br>b. CRT        | LPEN             | CRT               | Yes                   | Yes<br>Extended      | Yes                               |
| Grafacon                   | Highly sophisticated. A major item is the graphic stylus which is probably unnecessary for COPS. Does include CRT, keyboard.  | N/A                    | KBD                    | CRT                     | Stylus           | CRT               | -                     | -                    | -                                 |
| CALCOMP                    | Incremental plotter. S16 interface available but manufacturer does not yet have S16 plotting routines. These may be available from other DDP S16/CALCOMP installations.   | \$4500                 | None                   | None                    | None             | Plotter           | Yes                   | No                   | No                                |
| CC-30                      | Modular remote system designed for data phone use. Uses standard TV set for alphanumeric and graphic output.  | \$12 K minimum         | KBD                    | TV,<br>PTR              | LPEN             | TV                | Yes                   | No                   | Yes,<br>limited                   |
| DEC-338                    | Provides remote graphic capability. PDP-8 computer serves as remote processor - much software available with it.  | \$56 K                 | KBD                    | CRT,<br>PTR             | LPEN             | CRT               | Yes                   | Yes                  | Yes                               |
| Friden 7100                | Typewriter terminal. 130 characters/line. Up to 12 characters/second.   | \$3200                 | KBD                    | TYP                     | None             | None              | Yes                   | No                   | No                                |
| Gerber 22                  | Smallest of Gerber line is 4 by 5-foot drafting table. Provides fairly high accuracy.   | N/A                    | None                   | None                    | None             | Plotter           | Yes                   | -                    | No                                |
| ASR 33                     | Teletype unit supplied with Honeywell computers. Easiest to interface. 72 characters/line, 12 characters/second maximum.  | \$1200                 | KBD                    | TYP                     | None             | None              | Yes                   | Yes                  | No                                |
| S54-00                     | Honeywell's alphanumeric CRT remote terminal.   | N/A                    | KBD                    | CRT                     | None             | None              | No                    | No                   | No                                |
| IBM-2740                   | IBM selectric remote terminal. Uses 6 bit code. 130 characters/line.  | N/A                    | KBD                    | TYP                     | None             | None              | Yes                   | Some                 | No                                |
| IBM-2250                   | IBM's sophisticated remote graphic terminal. Probably interface problems. 6-bit code.   | N/A                    | KBD                    | CRT                     | LPEN             | CRT               | Optional              | Some                 | Limited                           |
| IDIOM                      | Sophisticated graphics terminal. Versatile.   | N/A                    | KBD                    | CRT/<br>TYP             | LPEN             | CRT               | Yes                   | Yes                  | Yes                               |
| TEC-LITE                   | Small CRT alphanumeric terminal. Keyboard and function displays. Character display capability somewhat limited - to be increased this year (1968).  | N/A                    | KBD                    | CRT                     | None             | None              | No                    | -                    | No                                |

## 2.0 INTRODUCTION

The Hughes Aircraft Company entered into a six month contract NAS 12-566, with the Electronics Research Center of NASA on 17 July 1967. This report is the final technical report of the contract. The purpose of the contract was to establish a detailed mathematical model for the performance assessment of space communications system parameters. This goal was to be achieved by basing the work on the efforts of two other contracts, NAS 12-81 and NAS 5-9637.

The contractual goals may be seen in graphical form in Figure 2-1, the master program plan. This plan indicates the first half of the program was devoted to an examination of the mathematical model generated under contract NAS 5-9637 in two ways. The first is a reassessment of all the burden constants used in that model. The second method of examination is that of a sensitivity analysis, that is, of determining those constants which effect the overall results by the greatest amount. These tasks have been completed and were reported in the Interim Technical Report. (A summary of the sensitivity analysis is repeated in this report in Section 1.2.) An additional task accomplished during the first quarter of the contract was that of assembling four computer programs, developed under contract NAS 5-9637, into a single program. The second quarter goals have included: 1) a more detailed examination of a selected number of parametric relationship which the sensitivity analysis and burden review have shown to be the most important; 2) an examination of methods of implementing inputs and outputs to the computer to permit it to be used as an executive model; and 3) an evaluation and determination of the follow-on mathematical analysis for the next generation of communication system models.

Following the introduction, this report has been organized into the following sections:

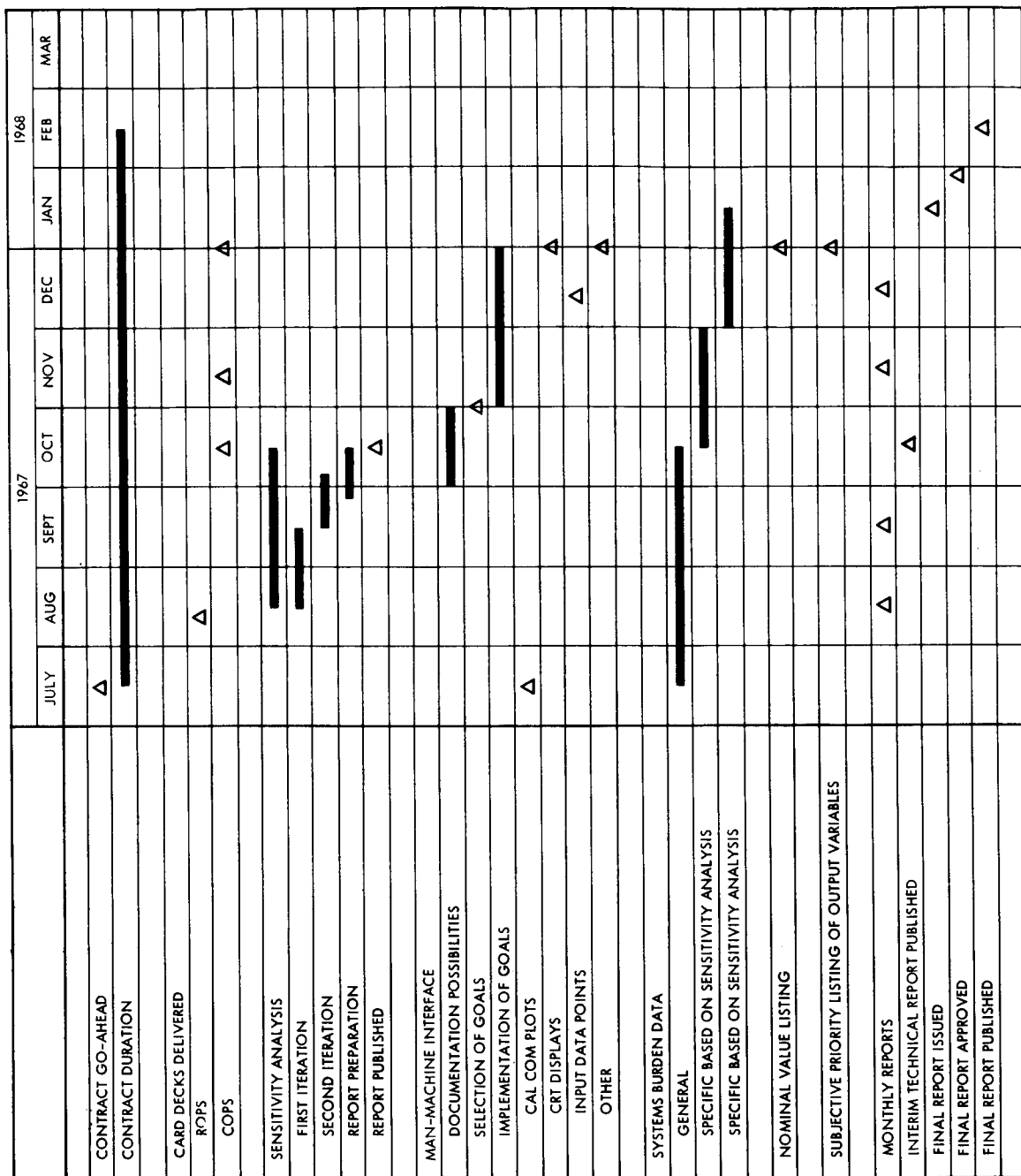


Figure 2-1. Master Program Plan for Contract NAS 12-566

## Symbols

This section contains nomenclature for the COPS program and for the COPTRAN program.

## User's Manual for COPTRAN, A Method of Optimum Communication System Design

This section describes COPTRAN programming. COPTRAN enables a user who is not familiar with computer operation to instruct the computer to solve a communication problem. The section contains the COPTRAN language, its usage, and gives examples of its use. In addition, a library of nominal data sets are given as is the logic used by COPTRAN to select automatically data from its data banks.

## Interface Equipment Summary

COPTRAN programming is presently run by a computer using batch processing. It is desired to use a faster processing method, preferably in a conversational mode between the computer and the user. For this reason interface equipment was investigated and its suitability documented.

## Contract End Item

A required end item for contract NAS 12-566 was to list potential areas for further development, study, and investigation. This has been documented in this section.

## 3.0 SYMBOLS

The symbols or nomenclature for this contract are listed in two parts, that part dealing with the COPS program and that part dealing with the COPTRAN program.

## 3.1 COPS Nomenclature

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description</u>   |
|----------------------------|------------------------|--|
|                            |                        | <u>System Parameters</u>   |
| ROP                        | ROP                    | mnemonic for Radio receiver Optimiza-<br>tion Program without component stops  |
| HOP                        | HOP                    | mnemonic for Heterodyne detection<br>optical receiver Optimization Program<br>without component stops                      |
| TOP                        | TOP                    | mnemonic for Thermal noise limited<br>direct detection optical receiver<br>Optimization Program without<br>component stops |
| SOP                        | SOP                    | mnemonic for Shot noise limited direct<br>detection optical receiver Optimization<br>Program without component stops       |
| ROPS                       | ROPS                   | mnemonic for Radio receiver Optimiza-<br>tion Program with component stops   |
| HOPS                       | HOPS                   | mnemonic for Heterodyne detection<br>optical receiver Optimization Program<br>with component stops                         |
| TOPS                       | TOPS                   | mnemonic for Thermal noise limited<br>direct detection optical receiver<br>Optimization Program with component<br>stops    |
| SOPS                       | SOPS                   | mnemonic for Shot noise limited direct<br>detection optical receiver Optimization<br>Program with component stops          |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description</u>                  |
|----------------------------|------------------------|-------------------------------------|
| PT                         | $P_T$                  | transmitter power                   |
| DT                         | $d_T$                  | transmitter antenna diameter        |
| GT                         | $G_T$                  | transmitter antenna gain            |
| DR                         | $d_R$                  | receiver antenna diameter           |
| GR                         | $G_R$                  | receiver antenna gain               |
| THER                       | $\theta_R$             | receiver field of view              |
| RB                         | $R_B$                  | information rate                    |
| PTO                        | $P_{TO}$               | optimum value of $P_T$              |
| DTO                        | $d_{TO}$               | optimum value of $d_T$              |
| GTO                        | $G_{TO}$               | optimum value of $G_T$              |
| DRO                        | $d_{RO}$               | optimum value of $d_R$              |
| GRO                        | $G_{RO}$               | optimum value of $G_R$              |
| THERO                      | $\theta_{RO}$          | optimum value of $\theta_R$         |
| PTI                        | $P_{TI}$               | initial program value of $P_T$      |
| DTI                        | $d_{TI}$               | initial program value of $d_T$      |
| GTI                        | $G_{TI}$               | initial program value of $G_T$      |
| DRI                        | $d_{RI}$               | initial program value of $d_R$      |
| GRI                        | $G_{RI}$               | initial program value of $G_R$      |
| THRI                       | $\theta_{RI}$          | initial program value of $\theta_R$ |
| PTB                        | $P_{TB}$               | limit value of $P_T$                |
| DTB                        | $d_{TB}$               | limit value of $d_T$                |
| GTB                        | $G_{TB}$               | limit value of $G_T$                |
| DRB                        | $d_{RB}$               | limit value of $d_R$                |
| GRB                        | $G_{RB}$               | limit value of $G_R$                |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description</u>                                |
|----------------------------|------------------------|---|
| THERB                      | $\theta_{RB}$          | limit value of $\theta_R$                         |
| PTM                        | $P_{TM}$               | fixed value of $P_T$ (= 0 for no constraint)      |
| DTM                        | $d_{TM}$               | fixed value of $d_T$ (= 0 for no constraint)      |
| GTM                        | $G_{TM}$               | fixed value of $G_T$ (= 0 for no constraint)      |
| DRM                        | $d_{RM}$               | fixed value of $d_R$ (= 0 for no constraint)      |
| GRM                        | $G_{RM}$               | fixed value of $G_R$ (= 0 for no constraint)      |
| THERM                      | $\theta_{RM}$          | fixed value of $\theta_R$ (= 0 for no constraint) |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description<br/>System Costs</u>   |
|----------------------------|------------------------|---|
| CDT                        | $C_{dT}$               | transmitter antenna cost  |
| CDR                        | $C_{dR}$               | receiver antenna cost   |
| CAT                        | $C_{AT}$               | transmitter acquisition and track<br>equipment fabrication cost independent<br>of transmitter beamwidth |
| CTHT                       | $C_{\theta T}$         | transmitter antenna fabrication cost  |
| CTHR                       | $C_{\theta R}$         | receiver antenna fabrication cost   |
| CQT                        | $C_{QT}$               | transmitter acquisition and track<br>equipment cost   |
| CNT                        | $C_{NT}$               | transmitter acquisition and track<br>equipment fabrication cost   |
| CAR                        | $C_{AR}$               | receiver acquisition and track equip-<br>ment fabrication cost independent of<br>receiver field of view |
| CQR                        | $C_{QR}$               | receiver acquisition and track<br>equipment cost  |
| CNR                        | $C_{NR}$               | receiver acquisition and track<br>equipment fabrication cost  |
| CFL                        | $C_{FL}$               | transmitter fabrication cost  |
| CPT                        | $C_{PT}$               | transmitter cost  |
| CM                         | $C_M$                  | modulation equipment cost   |
| CD                         | $C_D$                  | demodulation equipment cost   |
| CFM                        | $C_{FM}$               | modulation equipment fabrication cost   |
| CFD                        | $C_{FD}$               | demodulation equipment fabrication cost   |
| CKT                        | $C_{KT}$               | transmitter antenna fabrication cost<br>independent of transmitter aperture<br>diameter                 |
| CKR                        | $C_{KR}$               | receiver antenna fabrication cost inde-<br>pendent of receiver aperture diameter                        |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description</u>  |
|----------------------------|------------------------|---|
| CKH                        | $C_{KH}$               | transmitter heat exchanger fabrication cost independent of transmitter power dissipation                                |
| CST                        | $C_{ST}$               | transmitter power supply cost   |
| CSR                        | $C_{SR}$               | receiver power supply cost  |
| CH                         | $C_H$                  | heat exchanger fabrication cost   |
| CFT                        | $C_{FT}$               | transmitter power supply fabrication cost   |
| CFR                        | $C_{FR}$               | receiver power supply fabrication cost  |
| CKP                        | $C_{KP}$               | transmitter fabrication cost independent of transmitter power   |
| CKM                        | $C_{KM}$               | modulation equipment fabrication cost independent of information rate   |
| CKD                        | $C_{KD}$               | demodulation equipment fabrication cost independent of information rate   |
| CKE                        | $C_{KE}$               | transmitter power supply fabrication cost independent of transmitter power requirement                                  |
| CKF                        | $C_{KF}$               | receiver power supply fabrication cost independent of receiver power requirement  |
| CS                         | $C_S$                  | total system cost   |
| CV                         | $C_V$                  | variable part of total system cost (optimization cost)  |
| CFA                        | $C_{FA}$               | fixed part of total transmitter cost  |
| CFB                        | $C_{FB}$               | fixed part of total receiver cost   |
| CG                         | $C_G$                  | cost of transmitter, transmitter power supply, and transmitter heat exchanger which is dependent upon transmitter power |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description</u>  |
|----------------------------|------------------------|---|
| CT                         | $C_T$                  | cost of transmitter antenna, transmitter acquisition and track equipment, and associated power supply which is dependent upon transmitter aperture diameter |
| CQ                         | $C_Q$                  | cost of receiver acquisition and track equipment which is dependent upon receiver field of view   |
| CR                         | $C_R$                  | cost of receiver antenna, receiver acquisition and track equipment, and associated power supply which is dependent upon receiver aperture diameter          |
| CFA                        | $C_{FA}$               | total transmitter fabrication costs for optimum system parameters   |
| CFB                        | $C_{FB}$               | total receiver fabrication costs for optimum system parameters  |
| CA                         | $C_A$                  | total transmitter cost for optimum system parameters  |
| CB                         | $C_{BO}$               | total receiver cost for optimum system parameters   |
| CTO                        | $C_{TO}$               | value of $C_T$ for optimum system parameters  |
| CRO                        | $C_{RO}$               | value of $C_R$ for optimum system parameters  |
| CGO                        | $C_{GO}$               | value of $C_G$ for optimum system parameters  |
| CQO                        | $C_{QO}$               | value of $C_Q$ for optimum system parameters  |
| CVO                        | $C_{VO}$               | value of $C_V$ for optimum system parameters  |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description<br/>System Weights</u>   |
|----------------------------|------------------------|---|
| WDT                        | $W_{dT}$               | transmitter antenna weight  |
| WDR                        | $W_{dR}$               | receiver antenna weight   |
| WQT                        | $W_{QT}$               | transmitter acquisition and track equipment weight                                      |
| WBT                        | $W_{BT}$               | transmitter acquisition and track equipment weight independent of transmitter beamwidth |
| WQR                        | $W_{QR}$               | receiver acquisition and track equipment weight   |
| WBR                        | $W_{BR}$               | receiver acquisition and track equipment weight independent of receiver field of view.  |
| WT                         | $W_T$                  | transmitter weight  |
| WM                         | $W_M$                  | modulation equipment weight   |
| WD                         | $W_D$                  | demodulation equipment weight   |
| WSR                        | $W_{SR}$               | receiver power supply weight  |
| WST                        | $W_{ST}$               | transmitter power supply weight   |
| WH                         | $W_H$                  | transmitter heat exchanger weight   |
| WKT                        | $W_{KT}$               | transmitter antenna weight independent of transmitter aperture diameter                 |
| WKR                        | $W_{KR}$               | receiver antenna weight independent of receiver aperture diameter                       |
| WKP                        | $W_{KP}$               | transmitter weight independent of transmitter power                                     |
| WKH                        | $W_{KH}$               | transmitter heat exchanger weight independent of transmitter power dissipation          |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description</u>   |
|----------------------------|------------------------|--|
| WKM                        | $W_{KM}$               | modulation equipment weight independent of information rate                  |
| WKD                        | $W_{KD}$               | demodulation equipment weight independent of information rate                |
| WKE                        | $W_{KE}$               | transmitter power supply weight independent of transmitter power requirement |
| WKF                        | $W_{KF}$               | receiver power supply weight independent of receiver power requirement       |
| WA                         | $W_A$                  | total transmitter weight for optimum system parameters                       |
| WB                         | $W_B$                  | total receiver weight for optimum system parameters                          |

| <u>Computer<br/>Symbol</u>       | <u>Text<br/>Symbol</u> | <u>Description</u>   |
|----------------------------------|------------------------|--|
| <u>System Power Requirements</u> |                        |  |
| PQT                              | $P_{QT}$               | transmitter acquisition and track<br>equipment power requirement     |
| PQR                              | $P_{QR}$               | receiver acquisition and track<br>equipment power requirement        |
| PPT                              | $P_{PT}$               | transmitter power requirement  |
| PM                               | $P_M$                  | modulation equipment power<br>requirement                            |
| PD                               | $P_D$                  | demodulation equipment power<br>requirement                          |
| PST                              | $P_{ST}$               | transmitter power supply power<br>requirement                        |
| PSR                              | $P_{SR}$               | receiver power supply power<br>requirement                           |
| PA                               | $P_A$                  | total transmitter power requirement for<br>optimum system parameters |
| PB                               | $P_B$                  | total receiver power requirement for<br>optimum system parameters    |

| <u>Computer<br/>Symbol</u>                 | <u>Text<br/>Symbol</u> | <u>Description</u>   |
|--|------------------------|--|
| <u>System Constants of Proportionality</u> |                        |  |
| KA   | $K_A$                  | transmitter system optimization variable<br>( $K_A = 1$ indicates transmitter system fabrication cost optimization; $K_A = 0$ indicates no transmitter system fabrication cost optimization) |
| KB   | $K_B$                  | receiver system optimization variable<br>( $K_B = 1$ indicates receiver system fabrication cost optimization; $K_B = 0$ indicates no receiver system fabrication cost optimization)          |
| KC   | $K_C$                  | transmitter system optimization variable<br>( $K_C = 1$ indicates transmitter system weight optimization; $K_C = 0$ indicates no transmitter system weight optimization)                     |
| ZD   | $K_D$                  | receiver system optimization variable<br>( $K_D = 1$ indicates receiver system weight optimization; $K_D = 0$ indicates no receiver system weight optimization)                              |
| KSA  | $K_{SA}$               | cost per unit weight for transmitter system equipment  |
| KSB  | $K_{SB}$               | cost per unit weight for receiver system equipment   |
| KDT  | $K_{dT}$               | constant relating transmitter antenna weight to transmitter aperture diameter  |
| KTHT                                       | $K_{\theta T}$         | constant relating transmitter antenna fabrication cost to transmitter aperture diameter  |
| KDR  | $K_{dR}$               | constant relating receiver antenna weight to receiver aperture diameter  |
| KTHR                                       | $K_{\theta R}$         | constant relating receiver antenna fabrication cost to receiver aperture diameter  |
| KAT  | $K_{AT}$               | constant relating transmitter tracking equipment fabrication cost to transmitter beamwidth   |
| KWAT                                       | $K_{WAT}$              | constant relating transmitter tracking equipment weight to transmitter antenna weight  |
| KPQT                                       | $K_{PQT}$              | constant relating transmitter acquisition and track equipment power requirement to equipment weight  |
| KAR  | $K_{AR}$               | constant relating receiver tracking equipment fabrication cost to receiver field of view   |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description</u>   |
|----------------------------|------------------------|--|
| KWAR                       | $K_{W_{AR}}$           | constant relating receiver tracking equipment weight to receiver antenna weight                  |
| KPQR                       | $K_{P_{QR}}$           | constant relating receiver acquisition and track equipment power requirement to equipment weight |
| KWT                        | $K_{W_T}$              | constant relating transmitter weight to transmitter power  |
| KPT                        | $K_{P_T}$              | constant relating transmitter fabrication cost to transmitter power                              |
| KPM                        | $K_{P_M}$              | constant relating modulation equipment power requirement to equipment weight                     |
| KPD                        | $K_{P_D}$              | constant relating demodulation equipment power requirement to equipment weight                   |
| KST                        | $K_{ST}$               | constant relating transmitter power supply fabrication cost to power requirement                 |
| KWST                       | $K_{W_{ST}}$           | constant relating transmitter power supply weight to power requirement                           |
| KSR                        | $K_{SR}$               | constant relating receiver power supply fabrication cost to power requirement                    |
| KWR                        | $K_{WR}$               | constant relating receiver power supply weight to power requirement                              |
| KH                         | $K_H$                  | constant relating transmitter heat exchanger fabrication cost to transmitter power dissipation   |
| KX                         | $K_X$                  | constant relating transmitter heat exchanger weight to transmitter power dissipation             |
| KM                         | $K_M$                  | constant relating modulation equipment weight to information rate                                |
| KFM                        | $K_{FM}$               | constant relating modulation equipment fabrication cost to information rate                      |
| KD                         | $K_D$                  | constant relating demodulation equipment weight to information rate                              |
| KFD                        | $K_{FD}$               | constant relating demodulation equipment fabrication cost to information rate                    |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description</u>   |
|----------------------------|------------------------|--|
| KQT                        | $K_{q_T}$              | $K_A K_{AT} / (\lambda)^{q_T}$   |
| KMT                        | $K_{m_T}$              | $K_A K_{\theta_T}$   |
| KNT                        | $K_{n_T}$              | $K_A \left\{ K_{dT} K_{PQT} K_{WAT} K_{ST} \right\} + K_C K_{SA}$<br>$\left\{ K_{dT} [1 + K_{WAT} + K_{PQT} K_{WAT} K_{WST}] \right\}$ |
| KQR                        | $K_{q_R}$              | $K_B K_{AR}$   |
| KMR                        | $K_{m_R}$              | $K_B K_{\theta_R}$   |
| KNR                        | $K_{n_R}$              | $K_B \left\{ K_{dR} K_{PQP} K_{WAR} K_{SR} \right\} + K_D K_{SB}$<br>$\left\{ K_{dR} [1 + K_{WAR} + K_{PQR} K_{WAR} K_{WSR}] \right\}$ |
| KGt                        | $K_{g_T}$              | $K_C K_A K_{P_T}$  |
| KHT                        | $K_{h_T}$              | $K_{SA} K_{WT}$  |
| KJT                        | $K_{j_T}$              | $K_A \left\{ K_{ST}/k_e + K_H [1 - k_e/k_e] \right\} + K_C K_{SA}$<br>$\left\{ K_{WST}/k_e + K_x [1 - k_e/k_e] \right\}$               |
| QT                         | $q_T$                  | exponent relating transmitter acquisition<br>and track system fabrication cost to<br>transmitter beamwidth                             |
| MT                         | $m_T$                  | exponent relating transmitter antenna<br>fabrication cost to diameter  |
| NT                         | $n_T$                  | exponent relating transmitter antenna<br>weight to diameter  |
| QR                         | $q_R$                  | exponent relating receiver acquisition and<br>track system fabrication cost to receiver<br>field of view                               |
| MR                         | $m_R$                  | exponent relating receiver antenna fabri-<br>cation cost to diameter   |
| NR                         | $n_R$                  | exponent relating receiver antenna weight<br>to diameter   |
| ZT                         | $g_T$                  | exponent relating transmitter fabrication<br>cost to power   |
| HT                         | $h_T$                  | exponent relating transmitter weight to power  |
| JT                         | $j_T$                  | exponent of symmetrical convenience needed<br>in the sensitivity analysis  |
| KNS                        | $K_{NS}$               | SNR constant for shot noise limited direct<br>and heterodyne detection optical receiver  |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u> | <u>Description</u>   |
|----------------------------|------------------------|--|
| K                          | K                      | SNR constant for shot noise limited direct detection optical receiver    |
| KRB                        | KRB                    | SNR constant for shot noise limited direct detection optical receiver    |
| KM                         | $K_M$                  | SNR constant for thermal noise limited direct detection optical receiver |
| KN                         | $K_N$                  | SNR constant for heterodyne detection optical receiving                  |
| KR                         | $K_R$                  | SNR constant for radio receiver  |
| KE                         | $k_e$                  | transmitter power efficiency   |
| R                          | R                      | transmission range   |
| LMBDI                      | $\lambda_i$            | receiver input filter bandwidth in wavelength units                      |
|                            | $B_O$                  | receiver output filter bandwidth in frequency units                      |
|                            | $\Lambda$              | optimization dummy variable  |
|                            | Q                      | optimization dummy variable  |
|                            | G                      | detector current gain  |
|                            | $I_D$                  | detector dark current  |
| TAUT                       | $\tau_t$               | transmitter transmissivity   |
| TAUR                       | $\tau_r$               | receiver transmissivity  |
| TAUA                       | $\tau_a$               | atmospheric transmissivity   |
| ETA                        | $\eta$                 | detector quantum efficiency  |
| QB                         | $Q_B$                  | background radiation photon spectral radiance                            |
| LAMBDA                     | $\lambda$              | transmission wavelength  |
| RL                         | $R_L$                  | receiver load resistance   |
| SMK                        | k                      | Boltzmann's constant   |
| H                          | h                      | Planck's constant  |
| Q                          | q                      | electronic charge  |
| C                          | c                      | velocity of light  |
| TE                         | $T_e$                  | receiver temperature   |
| USTQ                       | $(\mu_{S,T})_{Req.}$   | number of signal photoelectrons required per decision interval           |
| UNTQ                       | $(\mu_{N,T})_{Req.}$   | number of noise photoelectrons required per decision interval            |

| <u>Computer<br/>Symbol</u> | <u>Text<br/>Symbol</u>     | <u>Description</u>   |
|----------------------------|----------------------------|--|
| USS                        | $\mu_{S, S}$               | number of signal photoelectrons per second                                 |
| UNS                        | $\mu_{N, S}$               | number of noise photoelectrons per second                                  |
| SN                         | $\left(\frac{S}{N}\right)$ | receiver output power signal-to-noise ratio                                |
| RB                         | $R_B$                      | information rate in bits per second  |
| RBQ                        | $(R_B)_{Req.}$             | required information rate in bits per second                               |
| CN                         | $\left(\frac{C}{N}\right)$ | constant relating shot noise powers due to signal and background radiation |
| RHOT                       | $\epsilon_T$               | transmitter antenna aperture efficiency                                    |
| RHOR                       | $\epsilon_R$               | receiver antenna aperture efficiency                                       |

### 3.2 COPTRAN Instruction Mnemonics

|        |  |
|--------|--|
| SPXMTR | Spacecraft transmitter   |
| EAXMTR | Earth transmitter  |
| SPRCVR | Spacecraft receiver  |
| EARCVR | Earth receiver   |
| RANMAR | Mars range ( $10^8$ km)  |
| RANJUP | Jupiter range ( $7.5 \times 10^8$ km)  |
| RANSAT | Synchronous satellite range ( $3.6 \times 10^4$ km)  |
| RANOTH | Other range value must be submitted with COPTRAN Data Deck. In addition all nominal burdens affected by range must be furnished by user and included in COPTRAN Data Deck. |
| LAM051 | $\lambda = 0.51$ micron  |
| LAM084 | $\lambda = 0.84$ micron  |
| LAM106 | $\lambda = 10.6$ microns   |
| LAM13C | $\lambda = 13$ cm  |
| LAMOTH | Other value must be submitted with COPTRAN Data Deck data. All nominal burdens affected by this wavelength must be furnished by user and included in COPTRAN Data Deck.    |
| BKMARS | Mars background  |
| BKJUPT | Jupiter background   |
| BKMOON | Moon background  |
| BKERTH | Earth background   |
| BKDSKY | Day sky background   |
| BKNSKY | Night sky background   |
| BKGALT | Galactic background  |
| BKOTHR | Other background value must be submitted with COPTRAN Data Deck  |
| PCM/AM | PCM amplitude modulation   |
| PCM/IM | PCM intensity modulation   |
| PCM/PL | PCM polarization modulation  |
| PCM/FM | PCM frequency modulation   |
| PCM/PM | PCM phase modulation   |
| PPM/IM | PPM intensity modulation   |

|         |   |
|---------|---|
| OPTDIR  | Optical direct detection  |
| OPTHET  | Optical heterodyne detection  |
| OPTHOM  | Optical homodyne detection  |
| RADHET  | Radio heterodyne detection  |
| RANHOM  | Radio homodyne detection  |
| XMWTOP  | Transmitter weight optimization   |
| RCWTOP  | Receiver weight optimization  |
| XMFCOP  | Transmitter fabrication cost optimization   |
| RCFCOP  | Receiver fabrication cost optimization  |
| DTDROP  | Transmitter antenna diameter and receiver antenna diameter optimization                           |
| GTDROP  | Transmitter antenna gain and receiver antenna diameter optimization                               |
| DTGROP  | Transmitter antenna diameter and receiver antenna gain optimization                               |
| GTGROP  | Transmitter antenna gain and receiver antenna gain optimization                                   |
| NXANT__ | Lists A to T, nominal transmitter antenna burdens   |
| NRANT__ | Lists A to T, nominal receiver antenna burdens  |
| NXACT__ | Lists A to T, nominal transmitter acquisition and track burdens                                   |
| NRACT__ | Lists A to T, nominal receiver acquisition and track burdens                                      |
| NMODE__ | Lists A to T, nominal modulator burdens   |
| NDMOD__ | Lists A to T, nominal demodulator burdens   |
| NXPWS__ | Lists A to T, nominal transmitter power supply burdens  |
| NRPWS__ | Lists A to T, nominal receiver power supply burdens   |
| NXMTR__ | Lists A to T, nominal transmitter burdens   |
| NBOOS__ | Lists A to T, nominal booster burdens   |
| RBFRQ__ | Number of information rate computations per decade, 1, 2, 4, 5, 8, 0 according to following table |

| <u>RBFRQ1</u> | <u>RBFRQ2</u>     | <u>RBFRQ4</u>      | <u>RBFRQ5</u>     | <u>RBFRQ8</u>       | <u>RBFRQ0</u>     |
|---------------|-------------------|--------------------|-------------------|---------------------|-------------------|
| $10^n$        | $10^n$            | $10^n$             | $10^n$            | $10^n$              | $10^n$            |
| $10^{n-1}$    | $0.5 \times 10^n$ | $0.75 \times 10^n$ | $0.8 \times 10^n$ | $0.875 \times 10^n$ | $0.9 \times 10^n$ |
|               | $10^{n-1}$        | $0.50 \times 10^n$ | $0.6 \times 10^n$ | $0.750 \times 10^n$ | $0.8 \times 10^n$ |
|               |                   | $0.25 \times 10^n$ | $0.4 \times 10^n$ | $0.625 \times 10^n$ | $0.7 \times 10^n$ |
|               |                   | $10^{n-1}$         | $0.2 \times 10^n$ | $0.500 \times 10^n$ | $0.6 \times 10^n$ |
|               |                   |                    | $10^{n-1}$        | $0.375 \times 10^n$ | $0.5 \times 10^n$ |
|               |                   |                    |                   | $0.250 \times 10^n$ | $0.4 \times 10^n$ |
|               |                   |                    |                   | $0.125 \times 10^n$ | $0.3 \times 10^n$ |
|               |                   |                    |                   | $10^{n-1}$          | $0.2 \times 10^n$ |
|               |                   |                    |                   |                     | $10^{n-1}$        |

RBINT\_\_\_\_ Initial information rate, exponent 0 to 8 (e.g.,  $R_B = 10^0, 10^1, \dots, 10^8$ )

RBFIN\_\_\_\_ Final information rate, exponent 1 to 9 (e.g.,  $R_B = 10^1, 10^2, \dots, 10^9$ ). Note that final information rate must be greater than initial information rate

PRTBUR Print system burdens data

PRTSPD Print system physical data

PRTSNC Print signal-to-noise ratio constants

PRTBRC Print system burden constants

PRTSPC Print system parameter constraints

PRTOPT Print optimum system parameters

PRTWGT Print weight burdens for optimum system parameters

PRTPPW Print power burdens for optimum system parameters

PRTFAB Print fabrication cost burdens for optimum system parameters

PRTSYC Print system cost burdens for optimum system parameters

PRTALL Prints all of above data

PRTDAT Print system burdens data, systems physical data, signal-to-noise ratio constants, system burden constants and system parameter constants.

|        |  |
|--------|--|
| PLTOPT | Plot optimum system parameters                                     |
| PLTOTO | Plot optimum value of transmitter antenna diameter                 |
| PLTGTO | Plot optimum value of transmitter antenna gain                     |
| PLTDRO | Plot optimum value of receiver antenna diameter                    |
| PLTGRO | Plot optimum value of receiver antenna gain                        |
| PLTPTO | Plot optimum value of transmitter power                            |
| PLTTRO | Plot optimum value of receiver field of view                       |
| PLTWDT | Plot transmitter antenna weight                                    |
| PLTWQT | Plot transmitter acquisition and track equipment weight            |
| PLTWQR | Plot receiver acquisition and track equipment weight               |
| PLTWX  | Plot transmitter weight  |
| PLTWH  | Plot transmitter heat exchanger weight                             |
| PLTWM  | Plot modulation equipment weight                                   |
| PLTWD  | Plot demodulation equipment weight                                 |
| PLTWST | Plot transmitter power supply weight                               |
| PLTWSR | Plot receiver power supply weight                                  |
| PLTWA  | Plot transmitter system weight                                     |
| PLTWB  | Plot receiver system weight  |
| PLTPQT | Plot transmitter acquisition and track equipment power requirement |
| PLTPX  | Plot transmitter power requirement                                 |
| PLTPM  | Plot modulation equipment power requirement                        |
| PLTPD  | Plot demodulation equipment power requirement                      |
| PLTPA  | Plot transmitter system power requirement                          |
| PLTPB  | Plot receiver system power requirement                             |
| PLTCDT | Plot transmitter antenna fabrication cost                          |
| PLTCDR | Plot receiver antenna fabrication cost                             |
| PLTCQT | Plot transmitter acquisition and track equipment fabrication cost  |
| PLTCQR | Plot receiver acquisition and track equipment fabrication cost     |
| PLTCX  | Plot transmitter fabrication cost                                  |
| PLTCH  | Plot transmitter heat exchanger fabrication cost                   |
| PLTCM  | Plot modulation equipment fabrication cost                         |

|        |  |
|--------|--|
| PLTCD  | Plot demodulation equipment fabrication cost   |
| PLTCST | Plot transmitter power supply fabrication cost |
| PLTCSR | Plot receiver power supply fabrication cost    |
| PLTCA  | Plot transmitter system fabrication cost       |
| PLTCB  | Plot receiver system fabrication cost          |
| PLTCTO | Plot transmitter antenna cost burden           |
| PLTCRO | Plot receiver antenna cost burden              |
| PLTCQO | Plot receiver field of view cost burden        |
| PLTCGO | Plot transmitter power cost burden             |
| PLTCV  | Plot optimization cost                         |
| PLTCS  | Plot total system cost                         |
| ENDINS | Instruction end                                |
| ENDDAT | Data end                                       |
| ENDCAS | Case end                                       |

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USER'S MANUAL FOR COPTRAN, A METHOD OF  
OPTIMUM COMMUNICATION SYSTEM DESIGN

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## 4.0 USER'S MANUAL FOR COPTRAN, A METHOD OF OPTIMUM COMMUNICATION SYSTEM DESIGN

### 4.1 Introduction

Calculations to determine communication capability of a transmission link are basically dependent on a single equation, the one way transmission equation. While there are variants in this equation to account for different types of noise, modulation and demodulation techniques, this one equation documents the interrelationships among the communication parameters of range, transmitter power, antenna gains, noise, etc. Since these parameters are multiplicative in the range equation it is possible to trade one parameter value against others while maintaining a given performance. Thus, it is difficult in many cases, to determine the "best" combination of parameters for a particular application although this is an important determination, especially to space missions.

It is therefore desirable to formulate an analytical method or methodology of not only selecting parameters which produce the desired performance within the regulation of the range equation but of selecting optimum parameter values which meet the desired performance.

Consider the following relatively simple optimization example for a deep space communication system. The effective radiated power from a spacecraft is to be maximized for a specified maximum weight. Now the effective radiated power may be increased by increasing either the size of the transmitting antenna or the transmitter power, or by some suitable combination of increases in these two parameters. The problem is to determine the proper split in weight between these two elements to maximize the effective radiated power subject to the given weight constraint. Clearly, the combination of an extremely large antenna using almost all the available weight with a minimal transmitter would not give the best possible performance, nor would the combination of an extremely heavy transmitter with a very low-gain antenna. The optimum configuration must therefore lie somewhere between these two extremes. In order to determine the optimum configuration, both transmitter power and antenna gain must be expressed in terms of weight. If these two relationships are known, a straight forward optimization

procedure can be employed to determine the optimum values for both transmitter power and the antenna size associated with the resulting antenna gain.

Such a concept has been expanded to all applicable parameter values in the range equation for both a weight optimization and a cost optimization. The resulting methodology has been implemented in a computer program known as COPS (Communication system Optimization Program with Stops).

The COPS program optimizes the values of the Major Communication Systems Parameters which are: the transmitter antenna diameter or gain, the receiver antenna diameter or gain, the transmitter power, and the receiver field of view. The program is implemented for radio frequency homodyne detection systems, optical frequency heterodyne detection systems, and for optical frequency thermal or shot noise limited direct detection systems.

The COPS program maximizes the signal-to-noise ratio, the transmission range, and the information rate and minimizes the probability of detection error for each communication system. The optimization uses as a criteria, the transmitter system weight, transmitter system fabrication cost, receiver system weight, receiver system fabrication cost either singly or in any combination. Fixed values for any of the Major System Parameters may be entered into the programs. In addition, maximum parameter values or "stops" may be placed on each of the Major System Parameters.

The COPS program provides a tabulation of optimum values of Major System Parameters as a function of information rate as outputs. Other outputs include: optimum transmitter antenna diameter or gain versus information rate; optimum receiver antenna diameter or gain versus information rate; optimum transmitter power versus information rate; and optimum receiver field of view versus information rate.

The inputs required for the COPS program are a tabulation of Systems Physical Data such as: range, sky noise background, wavelength, transmissivity losses etc; System Burdens Data such as: constants relating transmitter power to weight; antenna size to cost; etc., and System Parameter Constraints such as the maximum or fixed values for the Major Systems Parameters.

The COPS program has been written in Fortran IV language. In order to facilitate the use of the COPS program by persons unfamiliar with computer operation or programming, a buffer computer language called COPTRAN (Communication system Optimization Program TRANslator) has been developed.

To operate the COPS optimization program using the COPTRAN language involves answering a few simple questions which are written in the language of the user. For instance one question is: "What is the transmission range?" Following this question is a choice of four six letter mnemonics and their meanings. One of these, RANMAR, may be chosen to tell the COPS methodology through the COPTRAN buffer language that the range (RAN) is a Mars (MAR) distance,  $10^8$  km.

Similar simple questions, again using a multiple choice listing of mnemonics, are answered for such topics as the modulation type, the type of optimization desired, the type of output desired, etc.

The user may also use standard sets of data for the interrelationship of transmitter cost to power, etc. (burden relationships). Or if the user desires, he may change one or all the nominal constants, thus superceding the stored values.

The mnemonic answers and data values that are selected by the user to describe the problem he wishes to solve are written down by the user on a simple COPTRAN form. This form is then used to punch computer cards, one card per mnemonic or data value. The cards become part of the COPTRAN program and are batch processed by a computer.

The computer results are returned to the user either in a line printout or in Cal Compplots. [Section 5.4 of this final report lists several equipments which could be used with the COPTRAN language and the DDP-516 computer to implement a "conversational" operating procedure. This mode is proposed for a subsequent implementation phase. (See Section 6.3)]

Figure 4-1 summarizes the steps in obtaining optimized communications parameters using the COPS computer program with the COPTRAN language.

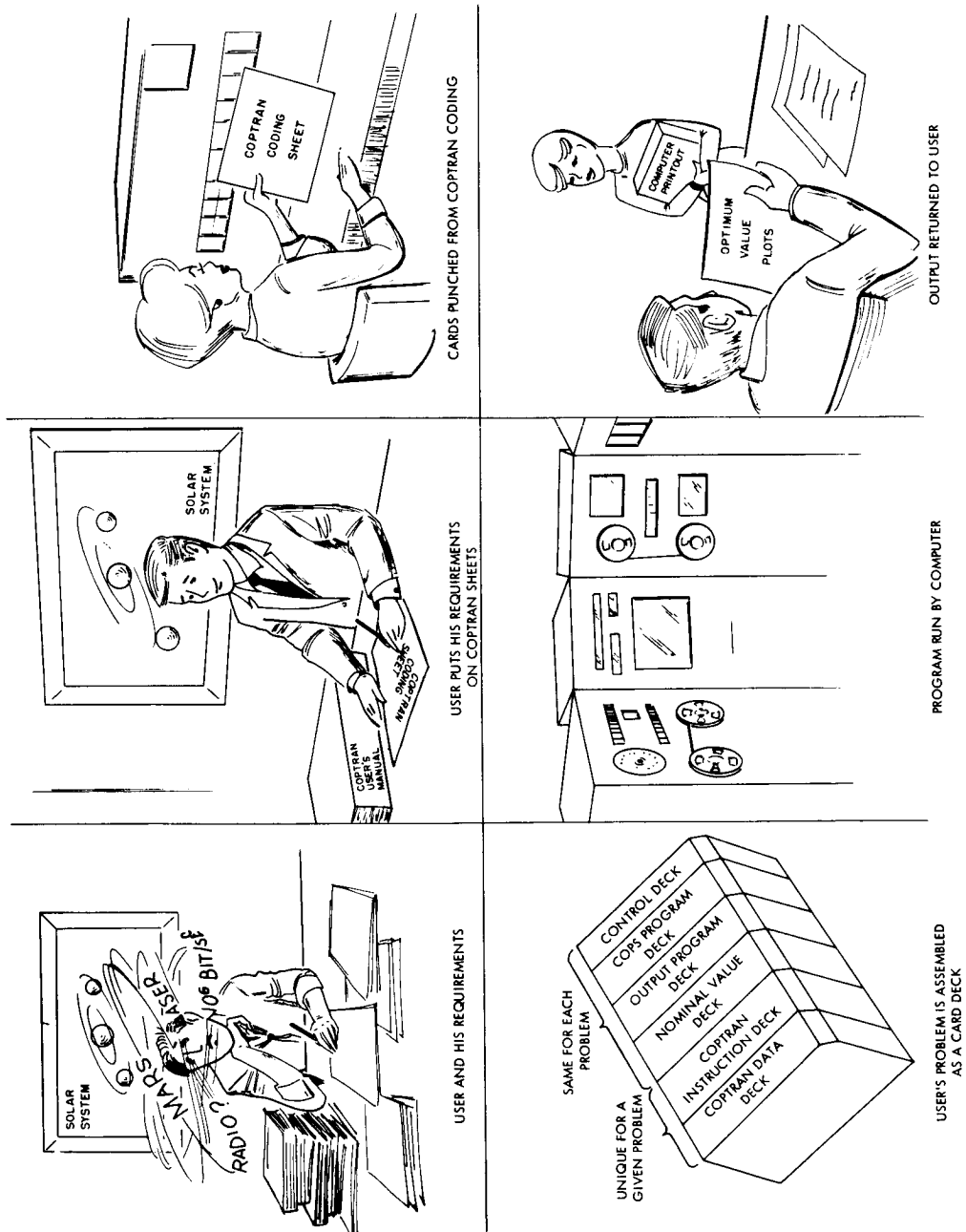


Figure 4-1. COPTRAN Programming

## 4.2 COPTRAN Programming Structure

4.2.1 Introduction. – COPTRAN programming language is a specialized, simple computer language used in the design of communication systems. COPTRAN allows a user to determine the optimum configuration of a communication system with relatively few instructions phrased in the context of his problem and without the necessity of supplying large quantities of data to the computer. This is accomplished by storing nominal values of the program data in the computer data banks. The pertinent data for a particular problem is then automatically fetched by the COPTRAN program unless countermanded by particular user selections.

The COPTRAN program structure is composed of six main parts. These parts are: 1) The Control Program Deck, 2) the COPS Program Deck, 3) the Output Program Deck, 4) the Nominal Value Decks, 5) The COPTRAN Instruction Deck, and 6) the COPTRAN Data Deck. Of these, only the last two are of concern to the COPTRAN user, and in many cases, only the COPTRAN Instruction Deck will be needed. It is the purpose of this instruction manual to describe these two portions of the COPTRAN Program in detail.

4.2.2 COPTRAN instruction deck. – The COPTRAN Instruction Deck is composed of punched cards, each of which has a single mnemonic. The mnemonics describe the communications problem to be solved in the following five categories.

### 1. Physical Environment

Transmitter location (spacecraft)

Receiver location (earth)

Transmission range (one of a set of selected ranges may be chosen to indicate physical environment or another range choice may be made and the environment specified)

Background (choice of physical source of background radiation)

### 2. Communication System

Transmission wavelength (one selected wavelength may be chosen)

Modulation and demodulation methods (choice of one of several sets are available)

3. Optimization

Optimization basis (transmitter system weight, transmitter system fabrication cost, receiver system weight, and receiver system fabrication cost may be minimized individually or in any combination)

Antenna parameter optimization (transmitter antenna gain or diameter and receiver antenna gain or diameter may be optimized)

4. Nominal System Burdens\* (see Section 4.5 for data description)

Choices of system burdens may be made from a data bank list if automatic selections are not desired. (Section 4.6 describes automatic data selection.) System burdens values may also be entered as new data if desired.

5. Processing

Computation format (choice of initial and final values of information rate and number of information rate data points calculated)

Print format (choice of data and results to be printed in tabular form)

Plot format (choice of results to be plotted by Cal Comp plotter)

4.2.3 COPTRAN data deck. — The COPTRAN Data Deck is the means by which individual burdens, physical data, stops, and fixed values are inserted into the COPTRAN program. If the automatic burdens and physical data

---

\*Burdens are the "constants" which represent the modeled relationship between system parameters such as transmitter power,  $P_T$ , and weight of the transmitter,  $W_{P_T}$ . In the following equation  $W_{KP}$ ,  $K_{W_T}$ , and  $h_T$  are "burdens":  
$$W_{P_T} = W_{KP} + K_{W_T}(P_T)^{h_T}.$$

selections provided by the COPTRAN instructions are acceptable to the user, and no parameter stops or fixed values are specified, there will be no COPTRAN Data Deck for the COPTRAN program (except an end data card, ENDDAT). The COPTRAN program has been developed so that input data in the COPTRAN Data Deck automatically replaces items of data normally selected from data banks. The program data is of three types.

1. System Physical Data

Physical data such as signal-to-noise rate, atmospheric transmissivity, receiver temperature, etc.

2. System Burdens Data

Weight, fabrication cost, and power requirement burdens for communication system components.

3. System Parameter Constraints

Fixed and stop values of the Major Communication System Parameters namely transmitting or receiving antenna gains or diameters, transmitter power, and receiver field of view. (A "fixed" parameter value is one that remains fixed throughout all portions of the optimization. A "stop" in the parameter value is the maximum value the parameter may take. For instance, a communication problem may require a fixed antenna size for a receiving antenna on earth of 64 meters and have a stop value for an antenna in space of 10 meters. The optimization program will determine the optimum split between the spacecraft antenna size as a function of data rate. As the data rate requirements increase, the transmitter power and antenna size will increase until the antenna size of 10 meters is reached. For larger data rates, the antenna size will remain at 10 meters and the transmitter power will increase, at a faster rate now, to meet the demands of higher data rates.)

### 4.3 COPTRAN Use

A COPTRAN program is considered to be the set of COPTRAN instructions and COPTRAN data cards which describe the communication system(s) to be optimized. This program, when submitted with the proper control cards and the COPTRAN card decks comprises a COPTRAN job. The COPTRAN card decks are supplied to the user and may not be altered. A typical COPTRAN job deck structure is shown in Figure 4-2. The COPTRAN instruction and data cards which must be supplied by the user are described in the following paragraphs.

The job deck set-up shown in Figure 4-2 is for a particular computer system: The GE 635 GECOS III system. No matter what physical system is used, the COPTRAN card decks and the COPTRAN program will be the same. The control cards, however, (identified by a '\$' in card column 1) will vary with the system. They are pictured here to indicate relative location in a job deck and the information required. The operations staff of a particular facility should be contacted for more specific information on control cards.

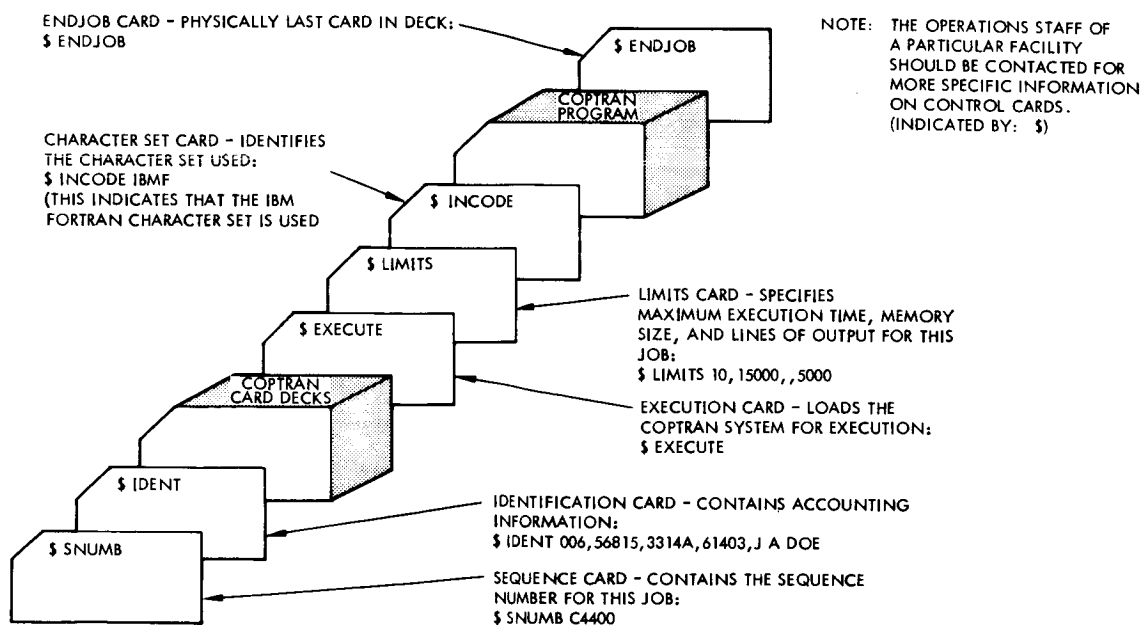


Figure 4-2. COPTRAN Job Deck Structure

4.3.1 COPTRAN program description. — A COPTRAN program is composed of single word COPTRAN instructions and a set of data values supplied to the program where they are different from the ones automatically supplied by the COPTRAN system. Each instruction is entered in columns 1-6 of one line of the COPTRAN coding sheet (see Figure 4-3). In order to properly specify a problem, the user should supply at least one instruction from each of the categories in Table IV-I. In some cases, more than one instruction in one category may be supplied. The remarks in each category in Table IV-I indicate the options which are available. It is suggested that the user prepare his program by examining each category in Table IV-I in sequence and selecting the instruction(s) from that category which best describe(s) his problem. It is important to note the restrictions which are placed on the use of certain instructions.

# COPTRAN CODING SHEET A

NAME \_\_\_\_\_ DATE \_\_\_\_\_ PROBLEM \_\_\_\_\_

## COPTRAN INSTRUCTIONS AND DATA

|    |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
|----|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 1  | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 1  |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 2  |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 3  |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 4  |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 5  |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 6  |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7  |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 8  |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 9  |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 11 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 12 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 13 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 14 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 15 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 16 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 17 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 18 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 19 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 20 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 21 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 22 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 23 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 24 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 25 |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |

Figure 4-3. COPTRAN Coding Sheet A

TABLE IV-I  
COMPLETE LISTING OF COPTRAN INSTRUCTION MNEMONICS

- |    |  |   |
|----|--|---|
| 1. | <u>Transmitter Location</u> (Only one available) |   |
|    | SPXMTR   | Spacecraft transmitter  |
| 2. | <u>Receiver Location</u> (Only one available)    |   |
|    | EARCVR   | Earth receiver  |
| 3. | <u>Transmitter Range</u> (Choose only one)       |   |
|    | RANMAR   | Mars range ( $10^8$ km)   |
|    | RANJUP   | Jupiter range ( $7.5 \times 10^8$ km)   |
|    | RANSAT   | Synchronous satellite range ( $3.6 \times 10^4$ km)   |
|    | RANOTH   | Range other than those above will be supplied with COPTRAN data. In addition, power supply burdens affected by range must be supplied by the user and included with COPTRAN data. |
| 4. | <u>Transmission Wavelength</u> (Choose only one) |   |
|    | LAM051   | $\lambda = 0.51$ micron   |
|    | LAM084   | $\lambda = 0.84$ micron   |
|    | LAM106   | $\lambda = 10.6$ microns  |
|    | LAM13C   | $\lambda = 13$ cm (2.3 GHz)   |
| 5. | <u>Background</u> (Choose only one)              |   |
|    | BKDSKY   | Day sky   |
|    | BKNSKY   | Night sky   |
|    | BKGALT   | Galactic  |

TABLE IV-I (continued)  
COMPLETE LISTING OF COPTRAN INSTRUCTION MNEMONICS

6. Modulation and Demodulation Methods (Choose only one modulation and demodulation method pair)
- |   |        |  |
|---|--------|--|
| { | PCM/AM | PCM amplitude modulation   |
| { | OPTDIR | Optical direct detection (Use only when $\lambda = 10.6$ microns. No other burdens are available.)     |
| { | PCM/PL | PCM polarization modulation  |
| { | OPTDIR | Optical direct detection (Use only when $\lambda = 0.51$ microns. No other burdens are available.)     |
| { | PCM/FM | PCM frequency modulation   |
| { | OPTHET | Optical heterodyne detection (Use only when $\lambda = 10.6$ microns. No other burdens are available.) |
| { | PCM/PM | PCM phase modulation   |
| { | RADHOM | Radio homodyne detection (Use only when $\lambda = 13$ cm. No other burdens are available.)            |
7. Optimization Basis (Choose at least one)
- [Note: If receiver parameters  $d_R$  and  $\theta_R$  or transmitter parameters  $d_T$  and  $P_T$  are not to be optimized in weight or fabrication cost, their fixed values must be given in the COPTRAN data deck. Selection of more than one instruction in this category provides joint optimization or burdens (i. e., fabrication cost or weight) selected.]
- |        |   |
|--------|---|
| XMWTOP | Transmitter weight optimization           |
| RCWTOP | Receiver weight optimization              |
| XMFTOP | Transmitter fabrication cost optimization |
| RCFCOP | Receiver fabrication cost optimization    |
8. Antenna Parameter Optimization (Choose only one)
- |        |  |
|--------|--|
| DTDROP | Transmitter antenna diameter and receiver antenna diameter optimization                            |
| GTDROP | Transmitter antenna gain and receiver antenna diameter optimization. (Use only with radio systems) |

TABLE IV-I (continued)  
COMPLETE LISTING OF COPTRAN INSTRUCTION MNEMONICS

|        |  |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
|--------|--|--------|--------------------------------------|--------|--------------------------------------|--------|--------------------------------------|--------|---|--------|---|--------|---|--------|---|--------|---|--------|---|--------|---|--------|--|--------|--|
| DTGROP | Transmitter antenna diameter and receiver antenna gain optimization. (Use only with radio systems)   |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| GTGROP | Transmitter antenna gain and receiver antenna gain optimization. (Use only one radio systems)  |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| 9.     | <p><u>Nominal System Burdens Data</u> (Choose one from each set desired. See section 4.5 for detail value Listing.)</p> <p>(Note: If no choice is made, program automatically selects burdens based on internal logic. See section 4.6.)</p> <p style="text-align: center;">Transmitter Antenna Burdens</p> <tr> <td>NXANTA</td><td><math>\lambda = 0.51</math> microns, spacecraft</td></tr> <tr> <td>NXANTC</td><td><math>\lambda = 0.84</math> microns, spacecraft</td></tr> <tr> <td>NXANTD</td><td><math>\lambda = 10.6</math> microns, spacecraft</td></tr> <tr> <td>NXANTF</td><td><math>\lambda = 13</math> cm, diameter burdens, spacecraft</td></tr> <tr> <td>NXANTG</td><td><math>\lambda = 13</math> cm, gain burdens, spacecraft</td></tr> <p style="text-align: center;">Receiver Antenna Burdens</p> <tr> <td>NRANTA</td><td><math>\lambda = 0.51</math> microns, optical direct detection, earth</td></tr> <tr> <td>NRANTB</td><td><math>\lambda = 0.51</math> microns, optical heterodyne or homodyne detection, earth</td></tr> <tr> <td>NRANTC</td><td><math>\lambda = 0.84</math> microns, optical direct detection, earth</td></tr> <tr> <td>NRANTD</td><td><math>\lambda = 10.6</math> microns, optical direct detection, earth</td></tr> <tr> <td>NRANTE</td><td><math>\lambda = 10.6</math> microns, optical heterodyne or homodyne detection, earth</td></tr> <tr> <td>NRANTF</td><td><math>\lambda = 13</math> cm, diameter burdens, earth</td></tr> <tr> <td>NRANTG</td><td><math>\lambda = 13</math> cm, gain burdens, earth</td></tr> | NXANTA | $\lambda = 0.51$ microns, spacecraft | NXANTC | $\lambda = 0.84$ microns, spacecraft | NXANTD | $\lambda = 10.6$ microns, spacecraft | NXANTF | $\lambda = 13$ cm, diameter burdens, spacecraft | NXANTG | $\lambda = 13$ cm, gain burdens, spacecraft | NRANTA | $\lambda = 0.51$ microns, optical direct detection, earth | NRANTB | $\lambda = 0.51$ microns, optical heterodyne or homodyne detection, earth | NRANTC | $\lambda = 0.84$ microns, optical direct detection, earth | NRANTD | $\lambda = 10.6$ microns, optical direct detection, earth | NRANTE | $\lambda = 10.6$ microns, optical heterodyne or homodyne detection, earth | NRANTF | $\lambda = 13$ cm, diameter burdens, earth | NRANTG | $\lambda = 13$ cm, gain burdens, earth |
| NXANTA | $\lambda = 0.51$ microns, spacecraft   |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NXANTC | $\lambda = 0.84$ microns, spacecraft   |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NXANTD | $\lambda = 10.6$ microns, spacecraft   |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NXANTF | $\lambda = 13$ cm, diameter burdens, spacecraft  |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NXANTG | $\lambda = 13$ cm, gain burdens, spacecraft  |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NRANTA | $\lambda = 0.51$ microns, optical direct detection, earth  |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NRANTB | $\lambda = 0.51$ microns, optical heterodyne or homodyne detection, earth  |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NRANTC | $\lambda = 0.84$ microns, optical direct detection, earth  |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NRANTD | $\lambda = 10.6$ microns, optical direct detection, earth  |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NRANTE | $\lambda = 10.6$ microns, optical heterodyne or homodyne detection, earth  |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NRANTF | $\lambda = 13$ cm, diameter burdens, earth   |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |
| NRANTG | $\lambda = 13$ cm, gain burdens, earth   |        |                                      |        |                                      |        |                                      |        |   |        |   |        |   |        |   |        |   |        |   |        |   |        |  |        |  |

TABLE IV-I (continued)  
COMPLETE LISTING OF COPTRAN INSTRUCTION MNEMONICS

Transmitter Acquisition and Track Burdens

|        |   |
|--------|---|
| NXACTA | Optical frequencies, spacecraft                 |
| NXACTB | Radio frequencies, spacecraft, diameter burdens |
| NXACTC | Radio frequencies, spacecraft, gain burdens     |

Receiver Acquisition and Track Burdens

|        |  |
|--------|--|
| NRACTA | Optical frequencies, earth                 |
| NRACTB | Radio frequencies, earth, diameter burdens |
| NRACTC | Radio frequencies, earth, gain burdens     |

Modulation Equipment Burdens

|        |  |
|--------|--|
| NMODEA | $\lambda = 0.51$ microns, CW laser, spacecraft     |
| NMODEB | $\lambda = 0.84$ microns, CW laser, spacecraft     |
| NMODEC | $\lambda = 0.84$ microns, pulsed laser, spacecraft |
| NMODED | $\lambda = 10.6$ microns, CW laser, spacecraft     |
| NMODEE | $\lambda = 13$ cm, spacecraft                      |
| NMODEF | $\lambda = 0.51$ microns, CW laser, earth          |
| NMODEG | $\lambda = 0.84$ microns, CW laser, earth          |
| NMODEH | $\lambda = 0.84$ microns, pulsed laser, earth      |
| NMODEI | $\lambda = 10.6$ microns, CW laser, earth          |
| NMODEJ | $\lambda = 13$ cm, earth                           |

Demodulation Equipment Burdens

|        |  |
|--------|--|
| NDMODA | Optical direct detection, earth            |
| NDMODB | Optical heterodyne detection, earth        |
| NDMODC | Optical homodyne detection, earth          |
| NDMODE | 13 cm radio homodyne detection, earth      |
| NDMODF | Optical direct detection, spacecraft       |
| NDMODG | Optical heterodyne detection, spacecraft   |
| NDMODH | Optical homodyne detection, spacecraft     |
| NDMODI | 13 cm radio direct detection, spacecraft   |
| NDMODJ | 13 cm radio homodyne detection, spacecraft |

TABLE IV-I (continued)  
COMPLETE LISTING OF COPTRAN INSTRUCTION MNEMONICS

Transmitter Power Supply Burdens

|        |                                   |
|--------|-----------------------------------|
| NXPWSA | RTG, spacecraft                   |
| NXPWSB | Reactor, spacecraft               |
| NXPWSC | Solar cell, Mars, Spacecraft      |
| NXPWSD | Generator, earth                  |
| NXPWSE | Solar cell, satellite, spacecraft |
| NXPWSF | Solar cell, Venus, spacecraft     |
| NXPWSG | Solar cell, Mercury, spacecraft   |

Receiver Power Supply Burdens

|        |                                   |
|--------|-----------------------------------|
| NRPWSA | RTG, spacecraft                   |
| NRPWSB | Reactor, spacecraft               |
| NRPWSC | Solar cell, Mars, spacecraft      |
| NRPWSD | Generator, earth                  |
| NRPWSE | Solar cell, satellite, spacecraft |
| NRPWSF | Solar cell, Venus, spacecraft     |
| NRPWSG | Solar cell, Mercury, spacecraft   |

Transmitter Burdens

|        |                                      |
|--------|--------------------------------------|
| NXMTRA | $\lambda = 0.51$ microns, spacecraft |
| NXMTRB | $\lambda = 0.51$ microns, earth      |
| NXMTRE | $\lambda = 10.6$ microns, spacecraft |
| NXMTRF | $\lambda = 10.6$ microns, earth      |
| NXMTRG | $\lambda = 13$ cm, spacecraft        |
| NXMTRH | $\lambda = 13$ cm, earth             |

TABLE IV-I (continued)  
COMPLETE LISTING OF COPTRAN INSTRUCTION MNEMONICS

| 10. <u>Computation Format</u> Choose one of each   |                   |                    |                   |                     |                   |
|--|-------------------|--------------------|-------------------|---------------------|-------------------|
| RBFQRQ____    Number of information rate computations per decade, 1, 2, 4, 5, 8, 0 according to following table  |                   |                    |                   |                     |                   |
| RBFQRQ1  | RBFQRQ2           | RBFQRQ4            | RBFQRQ5           | RBFQRQ8             | RBFQRQ0           |
| $10^n$   | $10^n$            | $10^n$             | $10^n$            | $10^n$              | $10^n$            |
| $10^{n-1}$   | $0.5 \times 10^n$ | $0.75 \times 10^n$ | $0.8 \times 10^n$ | $0.875 \times 10^n$ | $0.9 \times 10^n$ |
|  | $10^{n-1}$        | $0.50 \times 10^n$ | $0.6 \times 10^n$ | $0.750 \times 10^n$ | $0.8 \times 10^n$ |
|  |                   | $0.25 \times 10^n$ | $0.4 \times 10^n$ | $0.625 \times 10^n$ | $0.7 \times 10^n$ |
|  |                   | $10^{n-1}$         | $0.2 \times 10^n$ | $0.500 \times 10^n$ | $0.6 \times 10^n$ |
|  |                   |                    | $10^{n-1}$        | $0.375 \times 10^n$ | $0.5 \times 10^n$ |
|  |                   |                    |                   | $0.250 \times 10^n$ | $0.4 \times 10^n$ |
|  |                   |                    |                   | $0.125 \times 10^n$ | $0.3 \times 10^n$ |
|  |                   |                    |                   | $10^{n-1}$          | $0.2 \times 10^n$ |
|  |                   |                    |                   |                     | $10^{n-1}$        |
| RBINT____    Initial information rate, exponent 0 to 8<br>(e.g., $R_B = 10^0, 10^1, \dots, 10^8$ )   |                   |                    |                   |                     |                   |
| RBFIN____    Final information rate, exponent 1 to 9<br>(e.g., $R_B = 10^1, 10^2, \dots, 10^9$ )<br>Note that final information rate must be greater than initial information rate |                   |                    |                   |                     |                   |
| 11. <u>Print Format</u> Choose sets desired  |                   |                    |                   |                     |                   |
| PRTBUR    Print system burdens data  |                   |                    |                   |                     |                   |
| PRTSPD    Print system physical data   |                   |                    |                   |                     |                   |

TABLE IV-I (continued)  
COMPLETE LISTING OF COPTRAN INSTRUCTION MNEMONICS

|        |   |
|--------|---|
| PRTSNC | Print signal-to-noise ratio constants   |
| PRTBRC | Print system burden constants   |
| PRTSPC | Print parameter constraints   |
| PRTOPT | Print optimum system parameters   |
| PRTWGT | Print weight burdens for optimum system parameters  |
| PRTPPW | Print power burdens for optimum system parameters   |
| PRTFAB | Print fabrication cost burdens for optimum system parameters  |
| PRTSYC | Print system cost burdens for optimum system parameters   |
| PRTALL | Prints all of above data  |
| PRTDAT | Print system burdens data, systems physical data, signal-to-noise ratio constants, system burden constants, and system parameter constraints. |
| 12.    | <u>Plot Format</u> (Choose those desired)   |
| PLTOPT | Plot optimum system parameters  |
| PLTWA  | Plot transmitter system weight  |
| PLTCS  | Plot total system cost  |
| 13.    | <u>Instruction End</u> (This card must be placed at the end of COPTRAN instructions)  |
|        | ENDINS  |
| 14.    | <u>Data End</u> (This card must be placed at the end of COPTRAN data. It must appear after the "ENDINS" card if there is no data.)            |
|        | ENDDAT  |
| 15.    | <u>Case End</u> (This card must physically be the last card of the COPTRAN deck, following all instructions and data for all cases run.)      |
|        | ENDCAS  |

4.3.2 COPTRAN data format. — COPTRAN data is in two parts, a label consisting of up to six characters and a field consisting of up to fourteen characters in either fixed or floating point form. Small amounts of data are usually entered on COPTRAN Coding Sheet A (see Figure 4-3) by the user for subsequent key punching with the COPTRAN instructions. If a large amount of data is to be entered, COPTRAN Coding Sheets B and C shown in Figures 4-4 and 4-5 respectively may be utilized. These coding sheets contain preprinted data labels. Each data parameter will be punched on a single card, the total of these cards is the COPTRAN Data Deck. (Section 4.7 contains blank forms which are convenient for recoding large amounts of data.)

The data label must be justified left in columns 1 to 6 on the coding sheet. Columns 7, 8, 23, and 24 are left blank. The data value is entered in columns 9 to 22. Columns 25 to 80 may be employed for users comments.

Examples of fixed and floating point entries in the data field are given below. The decimal point in both cases is always in column 14.

Floating point entry:  $7.5 \times 10^{13}$

| 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
|   |   |   |    |    |    | 7  | .  | 5  |    |    |    | E  | +  | 1  | 3  |    |    |

Fixed point entry: 0.95

| 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
|   |   |   |    |    |    |    | .  | 9  | 5  |    |    |    |    |    |    |    |    |

A control card with the characters ENDDAT in columns 1 to 6 must be placed at the end of the COPTRAN Data Deck. This card is required even if there are no new data entries. If any item of data is not included in the COPTRAN Data Deck by the user, the COPTRAN program automatically selects the value of the data item from the nominal value data bank. The labels and definitions of the COPTRAN data which may be used are listed in Table IV-II.

# COPTRAN CODING SHEET B

NAME \_\_\_\_\_ DATE \_\_\_\_\_ PROBLEM \_\_\_\_\_

| SYSTEM BURDENS DATA |   |   |   |   |   |   |   |   |    |    |    |    | SYSTEM BURDENS DATA |   |   |   |   |   |   |   |   |    |    |    |    |
|---------------------|---|---|---|---|---|---|---|---|----|----|----|----|---------------------|---|---|---|---|---|---|---|---|----|----|----|----|
| 1                   | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 1                   | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
| 1                   | K | T | H | T |   |   |   |   |    |    |    |    | 1                   | K | T | H | R |   |   |   |   |    |    |    |    |
| 2                   | K | D | T |   |   |   |   |   |    |    |    |    | 2                   | K | D | R |   |   |   |   |   |    |    |    |    |
| 3                   | C | K | T |   |   |   |   |   |    |    |    |    | 3                   | C | K | R |   |   |   |   |   |    |    |    |    |
| 4                   | W | K | T |   |   |   |   |   |    |    |    |    | 4                   | W | K | R |   |   |   |   |   |    |    |    |    |
| 5                   | M | T |   |   |   |   |   |   |    |    |    |    | 5                   | M | R |   |   |   |   |   |   |    |    |    |    |
| 6                   | N | T |   |   |   |   |   |   |    |    |    |    | 6                   | N | R |   |   |   |   |   |   |    |    |    |    |
| 7                   |   |   |   |   |   |   |   |   |    |    |    |    | 7                   |   |   |   |   |   |   |   |   |    |    |    |    |
| 8                   | K | A | T |   |   |   |   |   |    |    |    |    | 8                   | K | A | R |   |   |   |   |   |    |    |    |    |
| 9                   | K | W | A | T |   |   |   |   |    |    |    |    | 9                   | K | W | A | R |   |   |   |   |    |    |    |    |
| 10                  | K | P | Q | T |   |   |   |   |    |    |    |    | 10                  | K | P | Q | R |   |   |   |   |    |    |    |    |
| 11                  | C | A | T |   |   |   |   |   |    |    |    |    | 11                  | C | A | R |   |   |   |   |   |    |    |    |    |
| 12                  | W | B | T |   |   |   |   |   |    |    |    |    | 12                  | W | B | R |   |   |   |   |   |    |    |    |    |
| 13                  | Q | T |   |   |   |   |   |   |    |    |    |    | 13                  | Q | R |   |   |   |   |   |   |    |    |    |    |
| 14                  |   |   |   |   |   |   |   |   |    |    |    |    | 14                  |   |   |   |   |   |   |   |   |    |    |    |    |
| 15                  | K | F | M |   |   |   |   |   |    |    |    |    | 15                  | K | F | D |   |   |   |   |   |    |    |    |    |
| 16                  | K | M |   |   |   |   |   |   |    |    |    |    | 16                  | K | D |   |   |   |   |   |   |    |    |    |    |
| 17                  | K | P | M |   |   |   |   |   |    |    |    |    | 17                  | K | P | D |   |   |   |   |   |    |    |    |    |
| 18                  | C | K | M |   |   |   |   |   |    |    |    |    | 18                  | C | K | D |   |   |   |   |   |    |    |    |    |
| 19                  | W | K | M |   |   |   |   |   |    |    |    |    | 19                  | W | K | D |   |   |   |   |   |    |    |    |    |
| 20                  |   |   |   |   |   |   |   |   |    |    |    |    | 20                  |   |   |   |   |   |   |   |   |    |    |    |    |
| 21                  | K | S | T |   |   |   |   |   |    |    |    |    | 21                  | K | S | R |   |   |   |   |   |    |    |    |    |
| 22                  | K | W | S | T |   |   |   |   |    |    |    |    | 22                  | K | W | S | R |   |   |   |   |    |    |    |    |
| 23                  | C | K | E |   |   |   |   |   |    |    |    |    | 23                  | C | K | F |   |   |   |   |   |    |    |    |    |
| 24                  | W | K | E |   |   |   |   |   |    |    |    |    | 24                  | W | K | F |   |   |   |   |   |    |    |    |    |
| 25                  |   |   |   |   |   |   |   |   |    |    |    |    | 25                  |   |   |   |   |   |   |   |   |    |    |    |    |

Figure 4-4. COPTRAN Coding Sheet B

# COPTRAN CODING SHEET C

NAME \_\_\_\_\_ DATE \_\_\_\_\_ PROBLEM \_\_\_\_\_

| SYSTEM BURDENS DATA |   |   |   |   |   |   |   |   |    |    |    | SYSTEM PHYSICAL DATA |   |   |   |   |   |   |   |   |    |    |    |  |
|---------------------|---|---|---|---|---|---|---|---|----|----|----|----------------------|---|---|---|---|---|---|---|---|----|----|----|--|
| 1                   | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 1                    | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |  |
| 1                   | K | P | T |   |   |   |   |   |    |    |    | 1                    | R |   |   |   |   |   |   |   |    |    |    |  |
| 2                   | K | W | T |   |   |   |   |   |    |    |    | 2                    | L | A | M | B | D | A |   |   |    |    |    |  |
| 3                   | K | H |   |   |   |   |   |   |    |    |    | 3                    | S | N |   |   |   |   |   |   |    |    |    |  |
| 4                   | K | X |   |   |   |   |   |   |    |    |    | 4                    | C | N |   |   |   |   |   |   |    |    |    |  |
| 5                   | K | E |   |   |   |   |   |   |    |    |    | 5                    | U | S | B | R | E | Q |   |   |    |    |    |  |
| 6                   | C | K | P |   |   |   |   |   |    |    |    | 6                    | T | A | U | T |   |   |   |   |    |    |    |  |
| 7                   | C | K | H |   |   |   |   |   |    |    |    | 7                    | T | A | U | R |   |   |   |   |    |    |    |  |
| 8                   | W | K | P |   |   |   |   |   |    |    |    | 8                    | T | A | U | A |   |   |   |   |    |    |    |  |
| 9                   | W | K | H |   |   |   |   |   |    |    |    | 9                    | T | E |   |   |   |   |   |   |    |    |    |  |
| 10                  | G | T |   |   |   |   |   |   |    |    |    | 10                   | E | T | A |   |   |   |   |   |    |    |    |  |
| 11                  | H | T |   |   |   |   |   |   |    |    |    | 11                   | R | L |   |   |   |   |   |   |    |    |    |  |
| 12                  | J | T |   |   |   |   |   |   |    |    |    | 12                   | L | M | B | D | I |   |   |   |    |    |    |  |
| 13                  |   |   |   |   |   |   |   |   |    |    |    | 13                   | Q | B |   |   |   |   |   |   |    |    |    |  |
| 14                  | K | S | A |   |   |   |   |   |    |    |    | 14                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 15                  | K | S | B |   |   |   |   |   |    |    |    | 15                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 16                  |   |   |   |   |   |   |   |   |    |    |    | 16                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 17                  |   |   |   |   |   |   |   |   |    |    |    | 17                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 18                  |   |   |   |   |   |   |   |   |    |    |    | 18                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 19                  |   |   |   |   |   |   |   |   |    |    |    | 19                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 20                  |   |   |   |   |   |   |   |   |    |    |    | 20                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 21                  |   |   |   |   |   |   |   |   |    |    |    | 21                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 22                  |   |   |   |   |   |   |   |   |    |    |    | 22                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 23                  |   |   |   |   |   |   |   |   |    |    |    | 23                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 24                  |   |   |   |   |   |   |   |   |    |    |    | 24                   |   |   |   |   |   |   |   |   |    |    |    |  |
| 25                  |   |   |   |   |   |   |   |   |    |    |    | 25                   |   |   |   |   |   |   |   |   |    |    |    |  |

Figure 4-5. COPTRAN Coding Sheet C

TABLE IV-IIa  
COPTRAN DATA

| <u>System Physical Data</u> Choose as desired |   |
|---|---|
| <u>Label</u>                                  | <u>Description</u>                            |
| R   | Transmission range                            |
| LAMBDA  | Transmission wavelength                       |
| SN  | Signal-to-noise power ratio                   |
| CN  | Carrier-to-background radiation power ratio   |
| USBREQ  | Required signal photoelectron count per bit   |
| TAUT  | Transmitter transmissivity                    |
| TAUR  | Receiver transmissivity                       |
| TAUA  | Atmospheric transmissivity                    |
| RHOT  | Transmitter antenna efficiency                |
| RHOR  | Receiver antenna efficiency                   |
| TE  | Receiver equivalent temperature               |
| ETA   | Detector quantum efficiency                   |
| RL  | Receiver output load resistance               |
| LMBDI   | Optical filter bandwidth                      |
| QB  | Background radiation photon spectral radiance |

TABLE IV-IIb  
COPTRAN DATA

| <u>Systems Burdens Data</u> Choose as desired |   |
|---|---|
| <u>Symbol</u>                                 | <u>Description</u>  |
| KTHT  | Constant Relating Transmitter Antenna Fabrication Cost to Transmitter Antenna Diameter                |
| KDT   | Constant Relating Transmitter Antenna Weight to Transmitter Antenna Diameter                          |
| CKT   | Transmitter Antenna Fabrication Cost Independent of Transmitter Antenna Diameter                      |
| WKT   | Transmitter Antenna Weight Independent of Transmitter Antenna Diameter                                |
| MT  | Exponent Relating Transmitter Antenna Fabrication Cost to Transmitter Antenna Diameter                |
| NT  | Exponent Relating Transmitter Antenna Weight to Transmitter Antenna Diameter                          |
| KAT   | Constant Relating Transmitter Acquisition – Track Equipment Fabrication Cost to Transmitter Beamwidth |
| KWAT  | Constant Relating Transmitter Acquisition – Track Equipment Weight to Transmitter Antenna Weight      |
| KPQT  | Constant Relating Transmitter Acquisition – Track Equipment Power Requirement to Weight               |
| CAT   | Transmitter Acquisition – Track Equipment Fabrication Cost Independent of Transmitter Beamwidth       |
| WBT   | Transmitter Acquisition – Track Equipment Weight Independent of Transmitter Beamwidth                 |
| QT  | Exponent Relating Transmitter Acquisition – Track Equipment Fabrication Cost to Transmitter Beamwidth |
| KFM   | Constant Relating Modulation Equipment Fabrication Cost to Information Rate                           |
| KM  | Constant Relating Modulation Equipment Weight to Information Rate                                     |
| KPM   | Constant Relating Modulation Equipment Power Requirement to Information Rate                          |
| CKM   | Modulation Equipment Fabrication Cost Independent of Information Rate                                 |
| WKM   | Modulation Equipment Weight Independent of Information Rate   |
| KST   | Constant Relating Transmitter Power Supply Fabrication Cost to Power Requirement                      |

TABLE IV-IIb (continued)  
COPTRAN DATA

| <u>Systems Burdens Data</u> |   | Choose as desired |
|-----------------------------|---|-------------------|
| <u>Symbol</u>               | <u>Description</u>  |                   |
| KWST                        | Constant Relating Transmitter Power Supply Weight to Power Requirement                          |                   |
| CKE                         | Transmitter Power Supply Fabrication Cost Independent of Power Requirement                      |                   |
| WKE                         | Transmitter Power Supply Weight Independent of Power Requirement                                |                   |
| KTHR                        | Constant Relating Receiver Antenna Fabrication Cost to Receiver Antenna Diameter                |                   |
| KDR                         | Constant Relating Receiver Antenna Weight to Receiver Antenna Diameter                          |                   |
| CKR                         | Receiver Antenna Fabrication Cost Independent of Receiver Antenna Diameter                      |                   |
| WKR                         | Receiver Antenna Weight Independent of Receiver Antenna Diameter                                |                   |
| MR                          | Exponent Relating Receiver Antenna Fabrication Cost to Receiver Antenna Diameter                |                   |
| NR                          | Exponent Relating Receiver Antenna Weight to Receiver Antenna Diameter                          |                   |
| KAR                         | Constant Relating Receiver Acquisition - Track Equipment Fabrication Cost to Receiver Beamwidth |                   |
| KWAR                        | Constant Relating Receiver Acquisition - Track Equipment Weight to Receiver Antenna Weight      |                   |
| KPQR                        | Constant Relating Transmitter Acquisition - Track Equipment Power Requirement to Weight         |                   |
| CAR                         | Receiver Acquisition - Track Equipment Fabrication Cost Independent of Receiver Beamwidth       |                   |
| WBR                         | Exponent Relating Receiver - Track Equipment Fabrication Cost to Receiver Beamwidth             |                   |
| QR                          | Exponent Relating Receiver Track Equipment Fabrication Cost to Receiver Beamwidth               |                   |
| KFD                         | Constant Relating Demodulation Equipment Fabrication Cost to Information Rate                   |                   |
| KD                          | Constant Relating Demodulation Equipment Weight to Information Rate                             |                   |
| KPD                         | Constant Relating Demodulation Equipment Power Requirement to Information Rate                  |                   |

TABLE IV-IIb (continued)  
COPTRAN DATA

| <u>Systems Burdens Data</u> Choose as desired |  |
|---|--|
| <u>Symbol</u>                                 | <u>Description</u>   |
| CKD   | Demodulation Equipment Fabrication Cost Independent of Information Rate                        |
| WKD   | Demodulation Equipment Weight Independent of Information Rate                                  |
| KSR   | Constant Relating Receiver Power Supply Fabrication Cost to Power Requirement                  |
| KWSR  | Constant Relating Receiver Power Supply Weight to Power Requirement                            |
| CKF   | Receiver Power Supply Fabrication Cost Independent of Power Requirement                        |
| WKF   | Receiver Power Supply Weight Independent of Power Requirement                                  |
| KPT   | Constant Relating Transmitter Fabrication Cost to Transmitter Power                            |
| KWT   | Constant Relating Transmitter Weight to Transmitter Power                                      |
| KH  | Constant Relating Transmitter Heat Exchanger Fabrication Cost to Transmitter Power Dissipation |
| KX  | Constant Relating Transmitter Heat Exchanger Weight to Transmitter Power Dissipation           |
| KE  | Transmitter Power Efficiency   |
| CKP   | Transmitter Fabrication Cost Independent of Transmitter Power                                  |
| CKH   | Transmitter Heat Exchanger Fabrication Cost Independent of Transmitter Power                   |
| WKP   | Transmitter Weight Independent of Transmitter Power  |
| WKH   | Transmitter Heat Exchanger Weight Independent of Transmitter Power                             |
| GT  | Exponent Relating Transmitter Fabrication Cost to Transmitter Power                            |
| HT  | Exponent Relating Transmitter Weight to Transmitter Power                                      |
| JT  | Exponent Relating Transmitter Power Supply-Heat Exchanger Burdens to Transmitter Power         |
| KSA   | Cost per Unit Weight for Spaceborne Transmitter System Equipment                               |
| KSB   | Cost per Unit Weight for Spaceborne Receiver System Equipment                                  |

TABLE IV-IIc  
COPTRAN DATA

| <u>Major System Parameter Constraints</u> |  | <u>Choose as indicated below</u>              |
|---|--|---|
|   | <u>Label</u>   | <u>Description</u>                            |
| A.  | DTM  | Fixed value of transmitter antenna diameter   |
|   | GTM  | Fixed value of transmitter antenna gain       |
| B.  | DRM  | Fixed value of receiver antenna diameter      |
|   | GRM  | Fixed value of receiver antenna gain          |
|   | PTM  | Fixed value of transmitter power              |
|   | THERM  | Fixed value of receiver field of view         |
| A.  | DTB  | Stop value of transmitter antenna diameter    |
|   | GTB  | Stop value of transmitter antenna gain        |
| B.  | DRB  | Stop value of receiver antenna diameter       |
|   | GRB  | Stop value of receiver antenna gain           |
|   | PTB  | Stop value of transmitter power               |
|   | THERB  | Stop value of receiver field of view          |
| C.  | DTI  | Initial value of transmitter antenna diameter |
|   | GTI  | Initial value of transmitter antenna gain     |
|   | DRI  | Initial value of receiver antenna diameter    |
|   | GRI  | Initial value of receiver antenna gain        |
|   | PTI  | Initial value of transmitter power            |
|   | THERI  | Initial value of receiver field of view       |
| A.  | Choose DTM (DTB) for transmitter antenna diameter optimization and GTM (GTB) for transmitter antenna gain optimization.        |   |
| B.  | Choose DRM (DRB) for receiver antenna diameter optimization and GRM (GRB) for receiver antenna gain optimization.              |   |
| C.  | Initial values of the system parameters may be chosen, if desired, to speed the convergence to a solution by the COPS program. |   |

4.3.3 COPTRAN Multiple Runs. — Two additional features are available with the COPTRAN system as a programming aid. These are the REPEAT (repeat) and INCRMNT (increment) features. They are used when more than one job is to be run in which only a few variables are to be changed. Figure 4-6 summarizes the use of these features. Each is described in more detail below.

REPEAT — This instruction signals the COPTRAN processor that more data or instructions follow which will be used to modify the case just completed. The cards following the REPEAT and preceding the next REPEAT or ENDCAS card will affect only those variables or instructions mentioned. As in normal COPTRAN programming, instructions must be terminated by an ENDINS card and precede all data. Data must be terminated by an ENDDAT card. Refer to Figure 4-6 for an example of the use of this feature.

Instructions following a REPEAT override all instructions in the same category in previous runs. Here category is defined to mean a group of similar instructions such as those referring to transmission range (Category 3) or those referring to optimization basis (Category 7). (Refer to Table IV-I.) Data entries of the previous run remain in effect unless specifically named in the REPEAT sequence.

NCRMNT (mnemonic for increment) — This instruction set permits the user to specify a series of runs in which one data value is varied from an initial value to a final value in finite step sizes. Figure 4-7 shows the three instructions and their use. The sequence

|             |          |
|-------------|----------|
| NCRMNT      | XXX E±XX |
| (DATA NAME) | XXX E±XX |
| FINALE      | XXX E±XX |

will cause a series of COPS runs to be made in which the variable named (DATA NAME) assumes the values from that on the (DATA NAME) card to that on the FINALE card in step sizes specified on the NCRMNT card. The variable (DATA NAME) will be incremented until its value is strictly greater than the final value specified. When this condition occurs, control returns to the COPTRAN processor and the case is finished.

NAME \_\_\_\_\_ DATE \_\_\_\_\_ PROBLEM \_\_\_\_\_

## COPTRAN INSTRUCTIONS AND DATA

|    |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
|----|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
|    | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 1  | S | P | X | M | I | R |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 2  | E | A | R | C | V | R |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 3  | • |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 4  | • |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 5  | • |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 6  | E | N | D | D | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7  | R | E | P | E | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 8  | X | X | X | X | X | X |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 9  | E | N | D | I | N | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10 | X | X | X | X | X | X |   |   | Y | •  | Y  | Y  |    | E  | Y  | Y  |    |    |    |    |    |    |    |    |
| 11 | E | N | D | D | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 12 | R | E | P | E | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 13 | X | X | X | X | X | X |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 14 | E | N | D | I | N | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 15 | X | X | X | X | X | X |   |   | Y | •  | Y  | Y  |    | E  | Y  | Y  |    |    |    |    |    |    |    |    |
| 16 | E | N | D | D | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 17 | • |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 18 | • |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 19 | • |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 20 | E | N | D | C | A | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 21 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 22 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 23 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 24 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 25 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |

COPTRAN PROGRAM

REPEAT  
(NEW INSTRUCTION(S)  
END OF NEW INSTRUCTIONS  
(NEW DATA)  
END OF NEW DATA  
REPEAT  
(NEW INSTRUCTION(S)  
END OF NEW INSTRUCTIONS  
(NEW DATA)  
END OF NEW DATA

END OF CASES TO BE RUN

COPTRAN PROGRAM

REPEAT

(NEW INSTRUCTION(S))

END OF NEW INSTRUCTIONS

(NEW DATA)

END OF NEW DATA

REPEAT

(NEW INSTRUCTION(S))

END OF NEW INSTRUCTIONS

(NEW DATA)

END OF NEW DATA

END OF CASES TO BE RUN

NOTE: Either new instructions or new data, or both, may follow a REPEAT.

Figure 4-6. "REPEAT" example.

NAME \_\_\_\_\_

DATE \_\_\_\_\_

## PROBLEM

## COPTRAN INSTRUCTIONS AND DATA

## COPTRAN INSTRUCTIONS AND DATA

(STEP SIZE)

(INITIAL VALUE)

(FINAL VALUE)

END OF DATA

END OF CASES TO BE RUN

[illegible]

**NOTE:** Final value must be greater than initial value. All three cards must be present.

Figure 4-7. Increment (NCR MNT) Example.

4.3.4 Error Messages. — As mentioned before, certain COPTRAN instruction combinations are either invalid or not yet implemented in the COPTRAN system. When such combinations are encountered, appropriate messages will be printed for the user and the job will not be run. The error messages are listed below:

'nnnnnn' NOT YET IMPLEMENTED

where nnnnnn is the name of the illegal instruction mnemonic

THE ONLY BURDENS AVAILABLE WITH 'PCM/AM' and 'PCM/FM'  
ARE FOR 'LAM106'

THE ONLY BURDENS AVAILABLE WITH 'PCM/PL' ARE FOR  
'LAM051'

THE ONLY BURDENS AVAILABLE WITH 'PCM/PM' ARE FOR  
'LAM13C'

THE ONLY BURDENS AVAILABLE WITH 'OPTDIR' ARE FOR  
'PCM/PL' AND 'LAM051'

THE ONLY BURDENS AVAILABLE WITH 'OPTHET' ARE FOR  
'PCM/FM' AND 'LAM106'

THE ONLY BURDENS AVAILABLE WITH 'RADHOM' ARE FOR  
'PCM/PM' AND 'LAM13C'

IF 'DRM' AND 'THERM' OR 'DTM' AND 'PTM' ARE NOT OPTI-  
MIZED IN WEIGHT OR COST, FIXED VALUES MUST BE  
GIVEN

#### 4.4 Program Examples

The following pages contain four examples of COPTRAN use. Each example contains a short description of the problem followed by a COPTRAN coding sheet as it might be coded for that problem. The output from that COPTRAN program concludes the data for a particular example.

Example A. Synchronous Satellite Transmitter to Earth Receiver Link

10.6 micron wavelength

PCM Intensity Modulation and Optical Direct Detection Receiver

Thermal Noise Limited Operation

Transmitter system weight and fabrication cost, and receiver fabrication cost jointly optimized.

Parameters to be optimized:

- a. Transmitter antenna diameter
- b. Receiver antenna diameter
- c. Transmitter power

Fixed Parameters: Receiver field of view at 1 milliradian

Parameter Stops: None

NAME \_\_\_\_\_ DATE \_\_\_\_\_ PROBLEM EXAMPLE A

## COPTRAN INSTRUCTIONS AND DATA

INSTRUCTION  
TYPE\*

|      | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 1    | S | P | X | M | T | R |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 2    | E | A | R | C | V | R |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 3    | R | A | N | S | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 4    | L | A | M | I | 0 | 6 |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 5    | B | K | D | S | K | Y |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 6    | P | C | M | / | A | M |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 6    | O | P | T | I | R |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7    | X | M | W | T | O | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7    | X | M | F | C | O | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7    | R | C | F | C | O | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 8    | D | T | D | R | O | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10   | R | B | F | R | Q | 2 |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10   | R | B | I | N | T | 2 |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10   | R | B | F | I | N | 8 |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 11   | P | R | T | A | L | L |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 12   | P | L | T | O | P | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 13   | E | N | D | I | N | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| DATA | T | H | E | R | M |   |   |   |   |    |    |    |    |    |    |    |    | 1  | 0  |    | E  | -  | 0  | 3  |
| 14   | E | N | D | D | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 15   | E | N | D | C | A | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 21   |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 22   |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 23   |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 24   |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 25   |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |

SPACECRAFT TRANSMITTER  
EARTH RECEIVER  
SYNCHRONOUS SATELLITE RANGE  
10.6 MICRON TRANSMISSION WAVELENGTH  
DAY SKY BACKGROUND  
PCM INTENSITY MODULATION  
OPTICAL DIRECT DETECTION  
TRANSMITTER SYSTEM WEIGHT AND  
FABRICATION COST AND RECEIVER SYSTEM  
FABRICATION COST OPTIMIZATION  
XMTR & RCVR ANT DIAMETER OPTIMIZATION  
DATA POINTS AT  $R_B = 10^2, 0.5 \times 10^3, 10^3,$   
...,  $10^8$  BPS

PRINT ALL DATA VALUES AND RESULTS OF OPT.  
PLOT RESULTS OF OPTIMIZATION  
END OF COPTRAN INSTRUCTIONS  
1 MILLIRADIAN FIELD OF VIEW  
END OF COPTRAN DATA  
END OF COPTRAN CASES

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

SPACECRAFT TRANSMITTER  
EARTH RECEIVER  
SYNCHRONOUS SATELLITE RANGE (3.6F4 KM)  
TRANSMISSION WAVELENGTH LAMBDA = 10.6 MICRONS  
DAY SKY BACKGROUND  
PCM AMPLITUDE MODULATION  
OPTICAL DIRECT DETECTION  
TRANSMITTER WEIGHT OPTIMIZATION  
TRANSMITTER FABRICATION COST OPTIMIZATION  
RECEIVER FABRICATION COST OPTIMIZATION  
TRANSMITTER ANTENNA DIAMETER AND RECEIVER ANTENNA DIAMETER OPTIMIZATION

## SYSTEM BURDENS DATA

|                     |      |         |     |        |     |          |     |       |    |      |    |         |
|---------------------|------|---------|-----|--------|-----|----------|-----|-------|----|------|----|---------|
| TRANSMITTER ANTENNA | KIHT | 14.0000 | KDI | 0.0100 | CKT | 20000.00 | WKT | 25.00 | MT | 2.00 | NT | 2.00000 |
|---------------------|------|---------|-----|--------|-----|----------|-----|-------|----|------|----|---------|

|                  |      |         |     |           |     |          |     |          |    |         |    |         |
|------------------|------|---------|-----|-----------|-----|----------|-----|----------|----|---------|----|---------|
| RECEIVER ANTENNA | KTHR | 8.75000 | KDR | 0.0230000 | CKR | 25000.00 | WKR | 20.00000 | MR | 2.00000 | NR | 2.00000 |
|------------------|------|---------|-----|-----------|-----|----------|-----|----------|----|---------|----|---------|

|  |     |        |      |         |      |         |     |         |     |       |    |         |
|--|-----|--------|------|---------|------|---------|-----|---------|-----|-------|----|---------|
| TRANSMITTER ACQUISITION AND TRACK SYSTEM | KAT | 71000. | KWAT | 0.46000 | KPQT | 0.48000 | CAT | 400000. | WBT | 5.000 | QT | 0.30000 |
|--|-----|--------|------|---------|------|---------|-----|---------|-----|-------|----|---------|

|                                       |     |        |      |         |      |         |     |         |     |       |    |         |
|---------------------------------------|-----|--------|------|---------|------|---------|-----|---------|-----|-------|----|---------|
| RECEIVER ACQUISITION AND TRACK SYSTEM | KAR | 71000. | KWAR | 0.46000 | KPOR | 0.48000 | CAR | 200000. | WBR | 5.000 | QR | 0.30000 |
|---------------------------------------|-----|--------|------|---------|------|---------|-----|---------|-----|-------|----|---------|

|             |     |         |     |         |     |         |    |         |    |         |     |         |
|-------------|-----|---------|-----|---------|-----|---------|----|---------|----|---------|-----|---------|
| TRANSMITTER | KPT | 1.43000 | KWT | 2.00000 | KH  | 1.97000 | KX | 0.02500 | KE | 0.10000 | CKP | 2000.00 |
|             | CKH | 13800.  | WKP | 25.000  | WKH | 0.      | JT | 1.000   | GI | 1.00000 | HT  | 1.00000 |

|                      |     |         |    |         |     |         |     |        |     |       |  |  |
|----------------------|-----|---------|----|---------|-----|---------|-----|--------|-----|-------|--|--|
| MODULATION EQUIPMENT | KPM | 0.00050 | KM | 0.00000 | KPM | 5.00000 | CKM | 15000. | WKM | 10.00 |  |  |
|----------------------|-----|---------|----|---------|-----|---------|-----|--------|-----|-------|--|--|

|                        |     |           |    |            |     |         |     |        |     |        |  |  |
|------------------------|-----|-----------|----|------------|-----|---------|-----|--------|-----|--------|--|--|
| DEMODULATION EQUIPMENT | KFD | 0.0000550 | KD | 0.00000011 | KPD | 3.33000 | CKD | 15000. | WKD | 30.000 |  |  |
|------------------------|-----|-----------|----|------------|-----|---------|-----|--------|-----|--------|--|--|

|                          |     |         |      |          |     |    |     |    |  |  |  |  |
|--------------------------|-----|---------|------|----------|-----|----|-----|----|--|--|--|--|
| TRANSMITTER POWER SUPPLY | KST | 166.000 | KWST | 0.157000 | CKE | 0. | WKE | 0. |  |  |  |  |
|--------------------------|-----|---------|------|----------|-----|----|-----|----|--|--|--|--|

|                       |     |        |      |    |     |        |     |    |  |  |  |  |
|-----------------------|-----|--------|------|----|-----|--------|-----|----|--|--|--|--|
| RECEIVER POWER SUPPLY | KSR | 25.000 | KWSR | 0. | CKF | 10000. | WKF | 0. |  |  |  |  |
|-----------------------|-----|--------|------|----|-----|--------|-----|----|--|--|--|--|

|                 |     |          |     |          |  |  |  |  |  |  |  |  |
|-----------------|-----|----------|-----|----------|--|--|--|--|--|--|--|--|
| BOOSTER BURDENS | KSA | 1640.000 | KSB | 1640.000 |  |  |  |  |  |  |  |  |
|-----------------|-----|----------|-----|----------|--|--|--|--|--|--|--|--|

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# SYSTEM PHYSICAL DATA

R 0.36000E 10 LAMBDA 0.10600E-02 S/M 0.26000E 02 C/M 0.60000E 01 USBREO 0.30000E 02 TAU-I 0.80000E 00  
 TAU-R 0.70000E 00 TAU-A 0.80000E 00 TE 0.30000E 03 ETA 0.50000E 00 RL 0.10000E 03 LMBD-I 0.10000E-02  
 QB 0. RHO-I 0.98000E 00 RHO-R 0.98000E 00

## SIGNAL-TO-NOISE RATIO CONSTANTS

K 0. KN 0. KM 0.36017E-06 KR 0. KS 0.

## SYSTEM BURDEN CONSTANTS

KMf 0.14000E 02 KNf 0.24879E 02 KQf 0.55420E 06 KMR 0.87500E 01 KNR 0.12696E 00 KQR 0.71000E 05  
 KGf 0.14300E 01 KHf 0.32800E 04 KJf 0.46219E 04

## PARAMETER CONSTRAINTS

DfI 0.50000E 02 GfI 0. DRf 0.50000E 03 GRf 0. PTf 0.25000E 03 YHERf 0.10000E-02  
 DfM 0. GfM 0. DRM 0. GRM 0. PTM 0. YHERM 0.10000E-02  
 DfB 0.10000E 03 GfB 0. DRB 0.10000E 04 GRB 0. PTB 0.50000E 03 YHERB 0.10000E-02

|   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
|---|--|--|--|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|
| INFORMATION RATE,RB   |  |  |  |  |  |  |  |  |  | 0.1000E 09  |  |  |  |  |  |  |  |  |  |
| OPTIMUM SYSTEM PARAMETERS   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| OPTIMUM WEIGHT BURDENS  |  |  |  |  |  |  |  |  |  | 0.255074E 02 WDR 0.413279E 03 WD1 0.523339E 01 WQR 0.185908E 03 WX 0.634130E 02   |  |  |  |  |  |  |  |  |  |
| WH 0.432174E 01 WH 0.400000E 02 WD 0.410000E 02 WST 0.619485E 02 MSR 0.             |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| WA 0.200424E 03 WB 0.640188E 03   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| OPTIMUM POWER BURDENS   |  |  |  |  |  |  |  |  |  | 0.251203E 01 PQR 0.892361E 02 PX 0.192065E 03 PM 0.200000E 03 PD 0.136530E 03     |  |  |  |  |  |  |  |  |  |
| PA 0.394577E 03 PB 0.225766E 03   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| OPTIMUM FABRICATION COST BURDENS  |  |  |  |  |  |  |  |  |  | CDT 0.207103E 05 CDR 0.174617E 06 CQI 0.139877E 07 COR 0.763973E 06               |  |  |  |  |  |  |  |  |  |
| CX 0.202747E 04 CH 0.141405E 05 CM 0.650000E 05 CD 0.205000E 05 CST 0.654997E 05    |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| CSR 0.156442E 05 CA 0.156615E 07 CB 0.974734E 06                                    |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| OPTIMUM SYSTEM COST BURDENS   |  |  |  |  |  |  |  |  |  | C1O 0.100074E 07 CRO 0.151788E 06 CQO 0.563973E 06 CGO 0.151788E 06               |  |  |  |  |  |  |  |  |  |
| CV 0.186829E 07 CS 0.391948E 07   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| XX        |  |  |  |  |  |  |  |  |  | XX      |  |  |  |  |  |  |  |  |  |
| XX        |  |  |  |  |  |  |  |  |  | XX      |  |  |  |  |  |  |  |  |  |
| INFORMATION RATE,RB   |  |  |  |  |  |  |  |  |  | 0.50001E 0A   |  |  |  |  |  |  |  |  |  |
| OPTIMUM SYSTEM PARAMETERS   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| OPTIMUM WEIGHT BURDENS  |  |  |  |  |  |  |  |  |  | DTO 0.624660E 01 DRO 0.128047E 03 PTO 0.184167E 02 THERO 0.1000E-02               |  |  |  |  |  |  |  |  |  |
| WD1 0.253902E 02 WDR 0.397107E 03 WD1 0.517949E 01 WQR 0.178469E 03 WX 0.618334E 02 |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| WH 0.414376E 01 WH 0.250003E 02 WD 0.355001E 02 WST 0.489298E 02 MSR 0.             |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| WA 0.170477E 03 WB 0.611077E 03   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| OPTIMUM POWER BURDENS   |  |  |  |  |  |  |  |  |  | PQT 0.248614E 01 PQR 0.856653E 02 PX 0.184167E 03 PH 0.125002E 03 PD 0.118215E 03 |  |  |  |  |  |  |  |  |  |
| PA 0.311655E 03 PB 0.203881E 03   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| OPTIMUM FABRICATION COST BURDENS  |  |  |  |  |  |  |  |  |  | CDT 0.205463E 05 CDR 0.168465E 06 CQI 0.136020E 07 COR 0.763973E 06               |  |  |  |  |  |  |  |  |  |
| CX 0.202634E 04 CH 0.141265E 05 CM 0.400006E 05 CD 0.177501E 05 CST 0.517347E 05    |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| CSR 0.150970E 05 CA 0.148863E 07 CB 0.965285E 06                                    |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |
| OPTIMUM SYSTEM COST BURDENS   |  |  |  |  |  |  |  |  |  | C1O 0.901712E 06 CRO 0.145546E 06 CQO 0.563973E 06 CGO 0.145546E 06               |  |  |  |  |  |  |  |  |  |
| CV 0.181678E 07 CS 0.373566E 07   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |









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XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
INFORMATION RATE,RB      0.10000E 04
OPTIMUM SYSTEM PARAMETERS
      DTO  0.785941E 00  DR0  0.933518E 02  PTO  0.978058E 01  THERO  0.1000E-02

OPTIMUM WEIGHT BURDENS  WD1  0.250062E 02  WDR  0.220435E 03  WQT  0.500284E 01  WQR  0.972000E 02  WX  0.445772E 02
                        WH  0.220243E 01  WM  0.100003E 02  WD  0.300001E 02  WST  0.235953E 02  WSR  0.
                        WA  0.110384E 03  WB  0.347635E 03

OPTIMUM POWER BURDENS  PU1  0.240136E 01  PUR  0.466560E 02  PX  0.978058E 02  PH  0.500015E 02  PD  0.999004E 02
                        PA  0.150289E 03  PB  0.146556E 03

OPTIMUM FABRICATION COST BURDENS  CDT  0.200086E 05  CDR  0.101252E 06  CDT  0.915565E 06  CQR  0.763973E 06
                        CX  0.201400E 04  CH  0.139736E 05  CM  0.150005E 05  CD  0.150001E 05  CST  0.249479E 05
                        CSR  0.136639E 05  CA  0.991510E 06  CB  0.893889E 06

OPTIMUM SYSTEM COST BURDENS  CTO  0.515889E 06  CHU  0.773588E 05  CCO  0.563973E 06  CGO  0.773588E 05
                        CV  0.123428E 07  CS  0.263655E 07

XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
INFORMATION RATE,RB      0.50001E 03
OPTIMUM SYSTEM PARAMETERS
      DTO  0.687896E 00  DR0  0.915017E 02  PTO  0.940443E 01  THERO  0.1000E-02

OPTIMUM WEIGHT BURDENS  WD1  0.250047E 02  WDR  0.212569E 03  WQT  0.500218E 01  WQR  0.935816E 02  WX  0.438089E 02
                        WH  0.211600E 01  WM  0.100001E 02  WD  0.300001E 02  WST  0.229920E 02  WSR  0.
                        WA  0.108924E 03  WB  0.336150E 03

OPTIMUM POWER BURDENS  PU1  0.240104E 01  PUR  0.449192E 02  PX  0.940443E 02  PH  0.500007E 02  PD  0.999002E 02
                        PA  0.146446E 03  PB  0.144819E 03

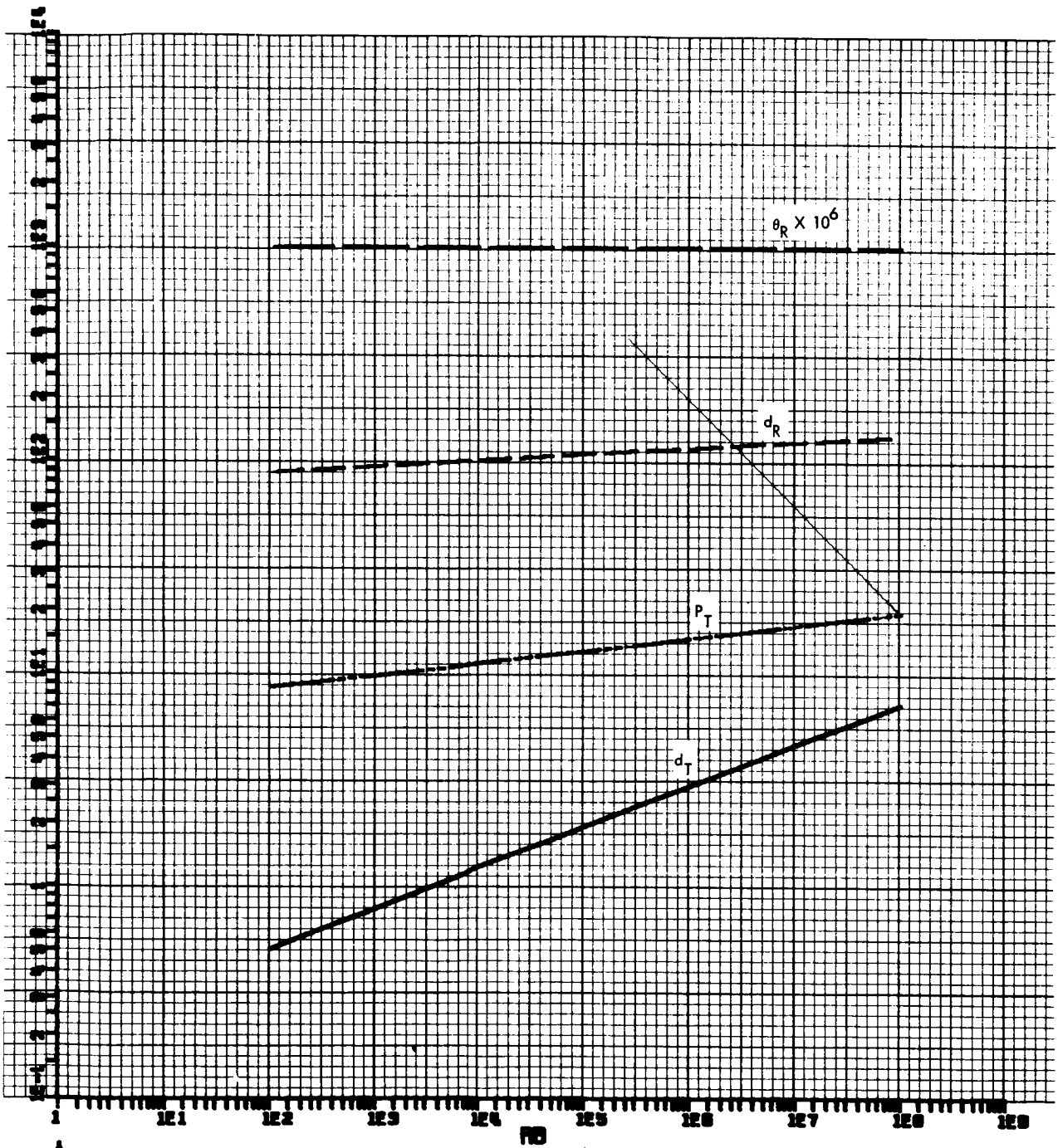
OPTIMUM FABRICATION COST BURDENS  CDT  0.200066E 05  CDR  0.982599E 05  CDT  0.895363E 06  CQR  0.763973E 06
                        CX  0.201345E 04  CH  0.139667E 05  CM  0.150003E 05  CD  0.150000E 05  CST  0.243101E 05
                        CSK  0.136205E 05  CA  0.970660E 06  CB  0.890853E 06

OPTIMUM SYSTEM COST BURDENS  CTO  0.495381E 06  CHU  0.743228E 05  CCO  0.563973E 06  CGO  0.743228E 05
                        CV  0.120800E 07  CS  0.259144E 07

XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX

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Example B: Mars Spacecraft Transmitter to Earth Receiver Link

0.51 micron wavelength

PCM polarization modulation

Shot Noise Limited Operation

Transmitter system weight and fabrication cost, and receiver fabrication cost jointly optimized.

Parameters to be optimized:

- a. Transmitter antenna diameter
- b. Receiver antenna diameter
- c. Transmitter power
- d. Receiver field of view

Fixed Parameters: None

Parameter Stops:

- a. Transmitter antenna diameter at 50 cm
- b. Receiver field of view at 2.5 microradians

NAME \_\_\_\_\_ DATE \_\_\_\_\_ PROBLEM EXAMPLE B

COPTRAN INSTRUCTIONS AND DATA

INSTRUCTION  
TYPE

|      | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 1    | S | P | X | M | T | R |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 2    | E | A | R | C | V | R |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 3    | R | A | N | M | A | R |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 4    | L | A | M | 0 | 5 | 1 |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 5    | B | K | D | S | K | Y |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 6    | P | C | M | / | P | L |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 6    | O | P | T | D | I | R |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7    | X | M | W | T | O | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7    | X | M | F | C | O | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7    | R | C | F | C | O | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 8    | D | T | D | R | O | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10   | R | B | F | R | Q | O |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10   | R | B | I | N | T | O |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10   | R | B | F | I | N | 8 |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 11   | P | R | I | D | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 12   | P | L | T | O | P | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 13   | E | N | D | I | N | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| DATA | T | H | E | R | B |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| DATA | D | T | B |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| DATA | D | T | I |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 14   | E | N | D | D | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 15   | E | N | D | C | A | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 23   |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 24   |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 25   |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |

SPACECRAFT TRANSMITTER  
EARTH RECEIVER  
MARS RANGE  
0.51 MICRON TRANSMISSION WAVELENGTH  
DAY SKY BACKGROUND  
PCM POLARIZATION MODULATION  
OPTICAL DIRECT DETECTION  
TRANSMITTER SYSTEM WEIGHT & FABRICATION  
COST AND RECEIVER SYSTEM FABRICATION  
COST JOINTLY OPTIMIZED  
TRANSMITTER & RECEIVER ANTENNA DIAMETER OPT.  
DATA POINTS AT  $R_B = 10^0, 0.2 \times 10^1,$   
 $0.3 \times 10^1, \dots, 10^8$  BITS PER SECOND

PRINT OUT ALL SYSTEM DATA  
PLOT VALUES OF OPT. SYSTEM PARAMETERS  
END OF COPTRAN INSTRUCTIONS  
2.5 RAD STOPS ON RECEIVING FIELD OF VIEW  
50 CM STOP ON TRANSMITTER ANT. DIAM.  
INITIAL VALUE OF TRANSMITTER ANT. DIAM.  
END OF COPTRAN DATA DECK  
END OF COPTRAN CASES

|   |
|---|
| SPACECRAFT TRANSMITTER  |
| EARTH RECEIVER  |
| MARS RANGE (1.E8 KM)  |
| TRANSMISSION WAVELENGTH LAMBDA = 0.51 MICRONS                           |
| DAY SKY BACKGROUND  |
| PCM POLARIZATION MODULATION   |
| OPTICAL DIRECT DETECTION  |
| TRANSMITTER WEIGHT OPTIMIZATION   |
| TRANSMITTER FABRICATION COST OPTIMIZATION                               |
| RECEIVER FABRICATION COST OPTIMIZATION                                  |
| TRANSMITTER ANTENNA DIAMETER AND RECEIVER ANTENNA DIAMETER OPTIMIZATION |

SYSTEM BURDENS DATA

|   |      |           |      |            |      |          |     |          |     |         |     |         |
|---|------|-----------|------|------------|------|----------|-----|----------|-----|---------|-----|---------|
| TRANSMITTER<br>ANTENNA                            | KTH  | 14.00000  | KDT  | 0.01000    | CKT  | 20000.00 | WKT | 25.00    | MT  | 2.00    | NT  | 2.00000 |
| RECEIVER<br>ANTENNA                               | KTHR | 8.75000   | KDR  | 0.0230000  | CKR  | 25000.00 | WKR | 20.00000 | MR  | 2.00000 | NR  | 2.00000 |
| TRANSMITTER<br>ACQUISITION<br>AND TRACK<br>SYSTEM | KAT  | 71000.    | KWAT | 0.46000    | KPOT | 0.48000  | CAT | 400000.  | WBT | 5.000   | QT  | 0.30000 |
| RECEIVER<br>ACQUISITION<br>AND TRACK<br>SYSTEM    | KAR  | 71000.    | KWAR | 0.46000    | KPOR | 0.48000  | CAR | 200000.  | WBR | 5.000   | QR  | 0.30000 |
| TRANSMITTER                                       | KPT  | 150.00000 | KWT  | 51.00000   | KH   | 0.58000  | KX  | 0.00700  | KE  | 0.00100 | CKP | 3500.00 |
|   | CKH  | 15800.    | WKP  | 40.000     | WKH  | 0.       | JT  | 1.000    | GT  | 1.00000 | HT  | 1.00000 |
| MODULATION<br>EQUIPMENT                           | KFM  | 0.00007   | KM   | 0.00000    | KPM  | 5.00000  | CKM | 7500.    | WKM | 5.00    |     |         |
| DEMODULATION<br>EQUIPMENT                         | KFD  | 0.0000550 | KD   | 0.00000011 | KPD  | 3.33000  | CKD | 15000.   | WKD | 30.000  |     |         |
| TRANSMITTER<br>POWER SUPPLY                       | KST  | 112.000   | KWST | 0.11000    | CKE  | 0.       | WKE | 0.       |     |         |     |         |
| RECEIVER<br>POWER SUPPLY                          | KSR  | 25.000    | KWSR | 0.         | CKF  | 10000.   | WKF | 0.       |     |         |     |         |
| BOOSTER<br>BURDENS                                | KSA  | 1640.000  | KSB  | 1640.000   |      |          |     |          |     |         |     |         |

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## SYSTEM PHYSICAL DATA

|       |             |        |             |       |             |     |             |        |             |        |             |
|-------|-------------|--------|-------------|-------|-------------|-----|-------------|--------|-------------|--------|-------------|
| R     | 0.10000E 14 | LAMBDA | 0.51000E-04 | S/N   | 0.12000E 02 | C/N | 0.30000E 01 | USBKEQ | 0.15000E 02 | TAU-T  | 0.80000E 00 |
| TAU-R | 0.70000E 00 | TAU-A  | 0.80000E 00 | TE    | 0.          | EIA | 0.20000E 00 | RL     | 0.10000E 03 | LMBD-I | 0.10000E-02 |
| QB    | 0.20000E 17 | RHO-I  | 0.90000E 00 | RHO-R | 0.98000E 00 |     |             |        |             |        |             |

## SIGNAL-10-NOISE RATIO CONSTANTS

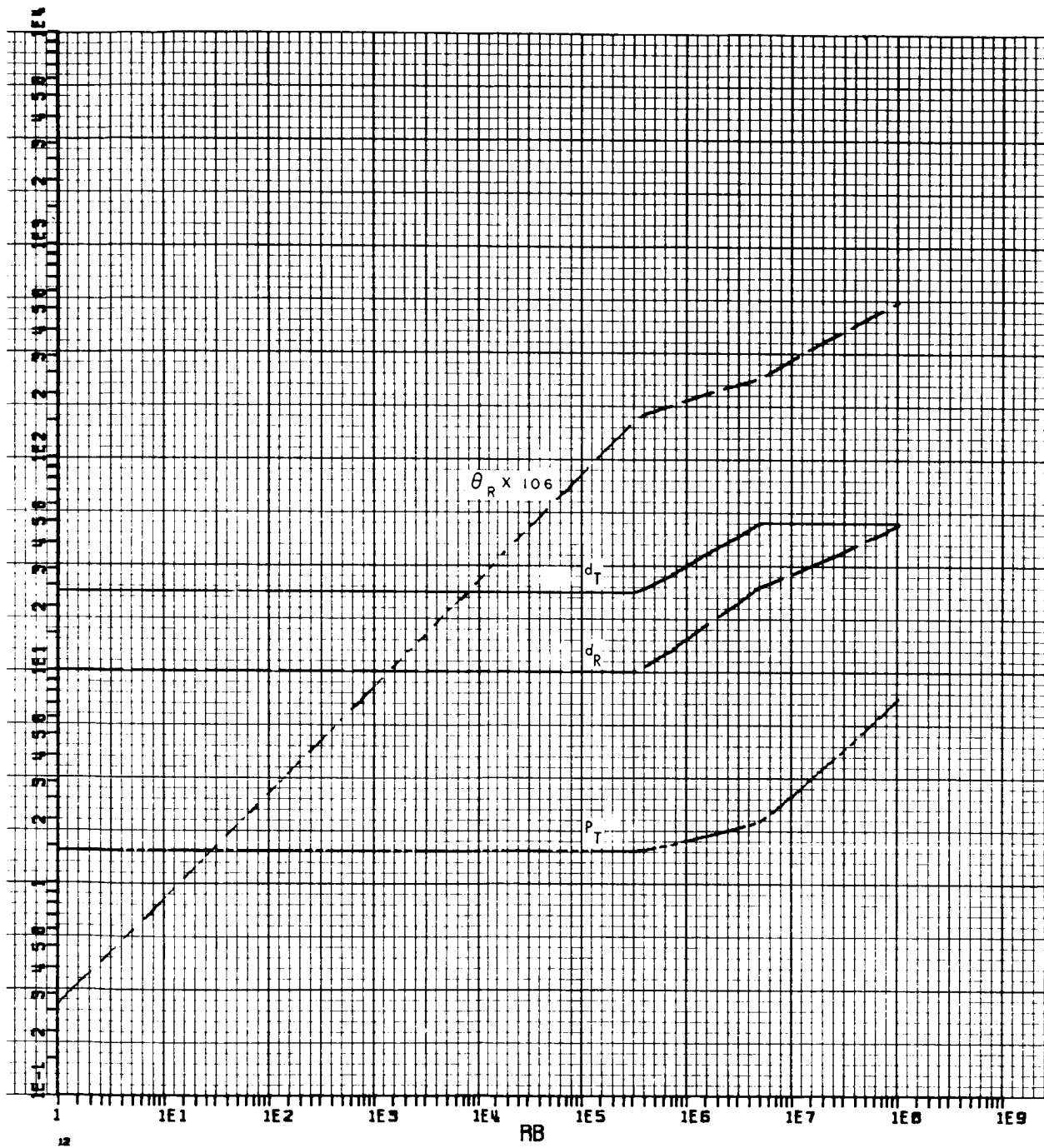
|   |             |    |    |    |    |    |    |    |             |
|---|-------------|----|----|----|----|----|----|----|-------------|
| K | 0.26052E 13 | KM | 0. | KM | 0. | KR | 0. | KS | 0.17679E-01 |
|---|-------------|----|----|----|----|----|----|----|-------------|

## SYSTEM BURDEN CONSTANTS

|     |             |     |             |     |             |     |             |     |             |     |             |
|-----|-------------|-----|-------------|-----|-------------|-----|-------------|-----|-------------|-----|-------------|
| KMT | 0.14000E 02 | KNI | 0.24590E 02 | KQT | 0.13772E 07 | KMR | 0.87500E 01 | KNR | 0.12696E 00 | KOR | 0.71000E 05 |
| KGT | 0.15000E 03 | KHI | 0.81640E 05 | KJT | 0.30445E 06 |     |             |     |             |     |             |

## PARAMETER CONSTRAINTS

|     |             |     |    |     |             |     |    |     |             |       |             |
|-----|-------------|-----|----|-----|-------------|-----|----|-----|-------------|-------|-------------|
| DTI | 0.45000E 02 | GTI | 0. | DRI | 0.50000E 03 | GRI | 0. | PTI | 0.25000E 02 | THERI | 0.20000E-04 |
| DTM | 0.          | GTM | 0. | DRM | 0.          | GRM | 0. | PTM | 0.          | THERM | 0.          |
| DTB | 0.50000E 02 | GTB | 0. | DRB | 0.10000E 04 | GRB | 0. | PTB | 0.50000E 02 | THERB | 0.10000E-04 |



Example C: Jupiter Spacecraft Transmitter to Earth Receiver Link

10.6 micron wavelength

PCM frequency shift keying

Shot noise limited operation

Transmitter system weight optimization

Parameters to be optimized:

- a. Transmitter antenna diameter
- b. Receiver antenna diameter
- c. Transmitter power

Fixed Parameters

- a. Receiver field of view at 1 milliradian

Parameter Stops

- a. Transmitter power at 1 kw
- b. Receiver antenna diameter at 1 meter
- c. Receiver antenna diameter at 50 cm

NAME \_\_\_\_\_ DATE \_\_\_\_\_ PROBLEM EXAMPLE C

# COPTRAN INSTRUCTIONS AND DATA

INSTRUCTION  
TYPE\*

|        | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|--------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 1      | S | P | X | M | T | R |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 2      | E | A | R | C | V | R |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 3      | R | A | N | J | U | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 4      | L | A | M | I | 0 | 6 |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 5      | B | K | D | S | K | Y |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 6      | P | C | M | / | F | M |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 6      | O | P | T | H | E | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7      | X | M | W | T | O | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 8      | D | T | D | R | O | P |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10     | R | B | F | R | Q | 0 |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10     | R | B | I | N | T | 0 |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10     | R | B | F | I | N | 7 |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 11     | P | R | T | D | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 12     | P | L | T | O | P | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 13     | E | N | D | I | N | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| DATA   | P | T | B |   |   |   |   |   |   |    |    |    |    |    |    | 1  | 0  |    | E  | +  | 0  | 3  |    |    |
| DATA   | D | R | M |   |   |   |   |   |   |    |    |    |    |    |    | 1  | 0  | 0  |    |    |    |    |    |    |
| DATA   | D | T | B |   |   |   |   |   |   |    |    |    |    |    |    | 5  | 0  |    |    |    |    |    |    |    |
| DATA   | T | H | E | R | M |   |   |   |   |    |    |    |    |    |    | 1  | 0  | 0  | E  | -  | 0  | 3  |    |    |
| 14     | E | N | D | D | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| REPEAT | R | E | P | E | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 13     | E | N | D | I | N | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| DATA   | D | T | B |   |   |   |   |   |   |    |    |    |    |    |    | 8  | 0  |    |    |    |    |    |    |    |
| 14     | E | N | D | D | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 15     | E | N | D | C | A | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |

SPACECRAFT TRANSMITTER  
EARTH RECEIVER  
JUPITER RANGE  
10.6 MICRON TRANSMISSION WAVELENGTH  
DAY SKY BACKGROUND  
PCM FREQUENCY SHIFT KEYING  
OPTICAL HETERODYNE DETECTION  
TRANSMITTER SYSTEM WEIGHT OPTIMIZATION  
TRANSMITTER & RECEIVER ANTENNA WT. OPT.  
DATA POINTS AT RB = 10°, 0.2 x 10', 0.3 x 10',  
... , 10<sup>7</sup> BPS  
PRINT SYSTEM DATA & CONSTANTS  
PLOT VALUES OF OPTIMUM SYSTEM PARAMETERS  
END OF COPTRAN INSTRUCTIONS  
1 KW STOP ON XMTR POWER  
1 METER STOP ON RECEIVER ANT. DIAMETER  
50 CM STOP ON TRANSMITTER ANT. DIAMETER  
1 MILLIRADIAN FIXED RECEIVER FIELD OF VIEW  
END OF COPTRAN DATA  
REPEAT PRECEDING CASE  
END OF COPTRAN INSTRUCTIONS  
NEW XMTR ANT. DIAM. STOP = 80 CM  
END OF DATA  
END OF CASES

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SPACECRAFT TRANSMITTER  
EARTH RECEIVER  
JUPITER RANGE(7.5E8 KM)  
TRANSMISSION WAVELENGTH LAMBDA - 10.6 MICRONS  
DAY SKY BACKGROUND  
PCM FREQUENCY MODULATION  
OPTICAL HETERODYNE DETECTION  
TRANSMITTER WEIGHT OPTIMIZATION  
TRANSMITTER ANTENNA DIAMETER AND RECEIVER ANTENNA DIAMETER OPTIMIZATION

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SYSTEM BURDENS DATA

|   |      |           |      |            |      |          |     |          |     |         |     |         |
|---|------|-----------|------|------------|------|----------|-----|----------|-----|---------|-----|---------|
| TRANSMITTER<br>ANTENNA                            | KHT  | 14.0000   | KDT  | 0.0100     | CKT  | 20000.00 | WKT | 25.00    | MT  | 2.00    | NT  | 2.00000 |
| RECEIVER<br>ANTENNA                               | KTHR | 8.7500    | KDR  | 0.0230000  | CKR  | 25000.00 | WKR | 20.00000 | MR  | 2.00000 | NR  | 2.00000 |
| TRANSMITTER<br>ACQUISITION<br>AND TRACK<br>SYSTEM | KAT  | 71000.    | KWAT | 0.46000    | KPAT | 0.48000  | CAT | 400000.  | WBT | 5.000   | QT  | 0.30000 |
| RECEIVER<br>ACQUISITION<br>AND TRACK<br>SYSTEM    | KAR  | 71000.    | KWAR | 0.46000    | KPAR | 0.48000  | CAR | 200000.  | WBR | 5.000   | QR  | 0.30000 |
| TRANSMITTER                                       | KPT  | 1.43000   | KWT  | 2.00000    | KH   | 1.97000  | KX  | 0.02500  | KE  | 0.10000 | CKP | 2000.00 |
|   | CKH  | 13800.    | WKP  | 25.000     | WKH  | 0.       | JT  | 1.000    | GT  | 1.00000 | HT  | 1.00000 |
| MODULATION<br>EQUIPMENT                           | KPM  | 0.00050   | KM   | 0.00000    | KPM  | 5.00000  | CKM | 15000.   | WKM | 10.00   |     |         |
| DEMODULATION<br>EQUIPMENT                         | KPD  | 0.0001000 | KD   | 0.00000020 | KPD  | 3.33000  | CKD | 27500.   | WKD | 55.000  |     |         |
| TRANSMITTER<br>POWER SUPPLY                       | KST  | 500.000   | KWST | 0.625000   | CKE  | 1200000. | WKE | 400.000  |     |         |     |         |
| RECEIVER<br>POWER SUPPLY                          | KSR  | 25.000    | KWSR | 0.         | CKF  | 10000.   | WKF | 0.       |     |         |     |         |
| BOOSTER<br>BURDENS                                | KSA  | 1640.000  | KSB  | 1640.000   |      |          |     |          |     |         |     |         |

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## SYSTEM PHYSICAL DATA

|       |             |        |             |       |             |     |             |        |             |        |             |
|-------|-------------|--------|-------------|-------|-------------|-----|-------------|--------|-------------|--------|-------------|
| R     | 0.75000E 14 | LAMBDA | 0.10600E-02 | S/N   | 0.15000E 02 | C/N | 0.          | USBREQ | 0.          | TAU-T  | 0.80000E 00 |
| TAU-R | 0.60000E 00 | TAU-A  | 0.80000E 00 | TE    | 0.          | ETA | 0.50000E 00 | RL     | 0.10000E 03 | LMBD-I | 0.10000E-02 |
| QB    | 0.          | RHO-T  | 0.98000E 00 | RHO-R | 0.98000E 00 |     |             |        |             |        |             |

## SIGNAL-TO-NOISE RATIO CONSTANTS

|   |    |    |             |    |    |    |    |    |    |
|---|----|----|-------------|----|----|----|----|----|----|
| K | 0. | KN | 0.16202E-04 | KM | 0. | KP | 0. | KS | 0. |
|---|----|----|-------------|----|----|----|----|----|----|

## SYSTEM BURDEN CONSTANTS

|     |    |     |             |     |             |     |    |     |    |     |    |
|-----|----|-----|-------------|-----|-------------|-----|----|-----|----|-----|----|
| KMT | 0. | KMI | 0.26207E 02 | KOT | 0.          | KMR | 0. | KNR | 0. | KOR | 0. |
| KGJ | 0. | KHT | 0.32800E 04 | KJT | 0.10619E 05 |     |    |     |    |     |    |

## PARAMETER CONSTRAINTS

|     |             |     |    |     |             |     |    |     |             |       |             |
|-----|-------------|-----|----|-----|-------------|-----|----|-----|-------------|-------|-------------|
| DTI | 0.50000E 02 | GTI | 0. | DRI | 0.10000E 03 | GR1 | 0. | PTI | 0.25000E 03 | THER1 | 0.10000E-02 |
| DTM | 0.          | GTM | 0. | DRM | 0.10000E 03 | GRM | 0. | PTM | 0.          | THERM | 0.10000E-02 |
| DTB | 0.80000E 02 | GTB | 0. | DRB | 0.10000E 03 | GRB | 0. | PTB | 0.50000E 03 | THERB | 0.10000E-02 |

SPACECRAFT TRANSMITTER  
EARTH RECEIVER  
JUPITER RANGE (7.5E8 KM)  
TRANSMISSION WAVELENGTH LAMBDA = 10.6 MICRONS  
DAY SKY BACKGROUND  
PCM FREQUENCY MODULATION  
OPTICAL HETERODYNE DETECTION  
TRANSMITTER WEIGHT OPTIMIZATION  
TRANSMITTER ANTENNA DIAMETER AND RECEIVER ANTENNA DIAMETER OPTIMIZATION

SYSTEM BURDENS DATA

|   |      |           |      |            |      |          |     |          |     |         |     |         |
|---|------|-----------|------|------------|------|----------|-----|----------|-----|---------|-----|---------|
| TRANSMITTER<br>ANTENNA                            | KTHY | 14.00000  | KDY  | 0.01000    | CKT  | 20000.00 | WKT | 25.00    | HT  | 2.00    | NT  | 2.00000 |
| RECEIVER<br>ANTENNA                               | KTHR | 8.75000   | KDR  | 0.0230000  | CKR  | 25000.00 | WKR | 20.00000 | HR  | 2.00000 | NR  | 2.00000 |
| TRANSMITTER<br>ACQUISITION<br>AND TRACK<br>SYSTEM | KAT  | 71000.    | KWAT | 0.46000    | KPQT | 0.48000  | CAT | 400000.  | WBT | 5.000   | QT  | 0.30000 |
| RECEIVER<br>ACQUISITION<br>AND TRACK<br>SYSTEM    | KAR  | 71000.    | KWAR | 0.46000    | KPOR | 0.48000  | CAR | 200000.  | WBR | 5.000   | OR  | 0.30000 |
| TRANSMITTER                                       | KPT  | 1.43000   | KWT  | 2.00000    | KH   | 1.97000  | KX  | 0.02500  | KE  | 0.10000 | CKP | 2000.00 |
|   | CKH  | 13800.    | WKP  | 25.000     | WKH  | 0.       | JT  | 1.000    | GT  | 1.00000 | HT  | 1.00000 |
| MODULATION<br>EQUIPMENT                           | KFM  | 0.00050   | KM   | 0.00000    | KPM  | 5.00000  | CKM | 15000.   | WKM | 10.00   |     |         |
| DEMODULATION<br>EQUIPMENT                         | KFD  | 0.0001000 | KD   | 0.00000020 | KPD  | 3.33000  | CKD | 27500.   | WKD | 55.000  |     |         |
| TRANSMITTER<br>POWER SUPPLY                       | KST  | 500.000   | KWST | 0.625000   | CKE  | 1200000. | WKE | 400.000  |     |         |     |         |
| RECEIVER<br>POWER SUPPLY                          | KSR  | 25.000    | KWSR | 0.         | CKF  | 10000.   | WKF | 0.       |     |         |     |         |
| BOOSTER<br>BURDENS                                | KSA  | 1640.000  | KSB  | 1640.000   |      |          |     |          |     |         |     |         |

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# SYSTEM PHYSICAL DATA

|       |             |        |             |       |             |     |             |        |             |        |             |
|-------|-------------|--------|-------------|-------|-------------|-----|-------------|--------|-------------|--------|-------------|
| R     | 0.75000E 14 | LAMBDA | 0.10600E-02 | S/N   | 0.15000E 02 | C/M | 0.          | USBREO | 0.          | TAU-T  | 0.80000E 00 |
| TAU-R | 0.60000E 00 | TAU-A  | 0.80000E 00 | TE    | 0.          | ETA | 0.50000E 00 | RL     | 0.10000E 03 | LMBD-I | 0.10000E-02 |
| QB    | 0.          | RHO-T  | 0.98000E 00 | RHO-R | 0.98000E 00 |     |             |        |             |        |             |

## SIGNAL-TO-NOISE RATIO CONSTANTS

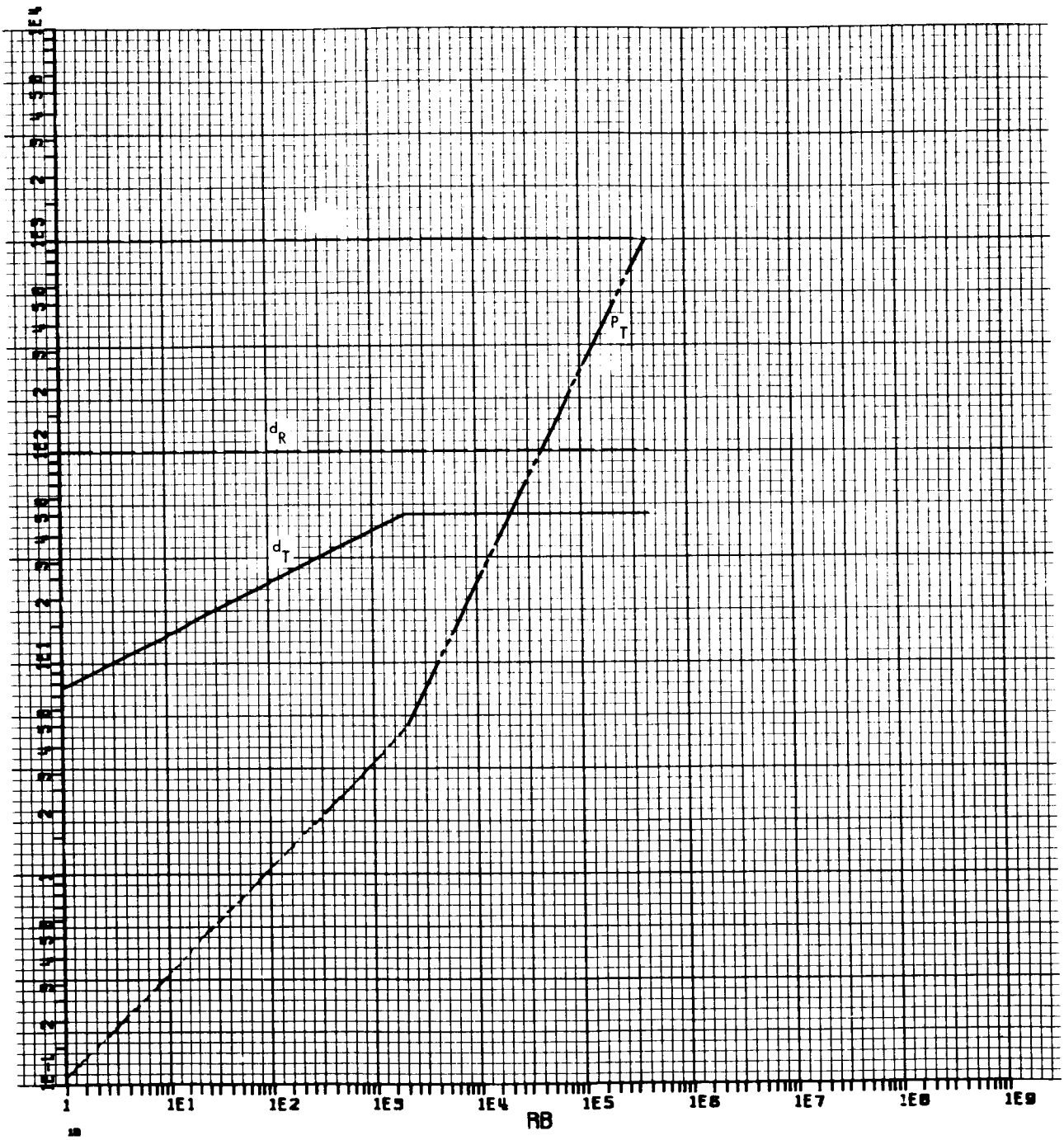
|   |    |    |             |    |    |    |    |    |    |
|---|----|----|-------------|----|----|----|----|----|----|
| K | 0. | KN | 0.16202E-04 | KM | 0. | KR | 0. | KS | 0. |
|---|----|----|-------------|----|----|----|----|----|----|

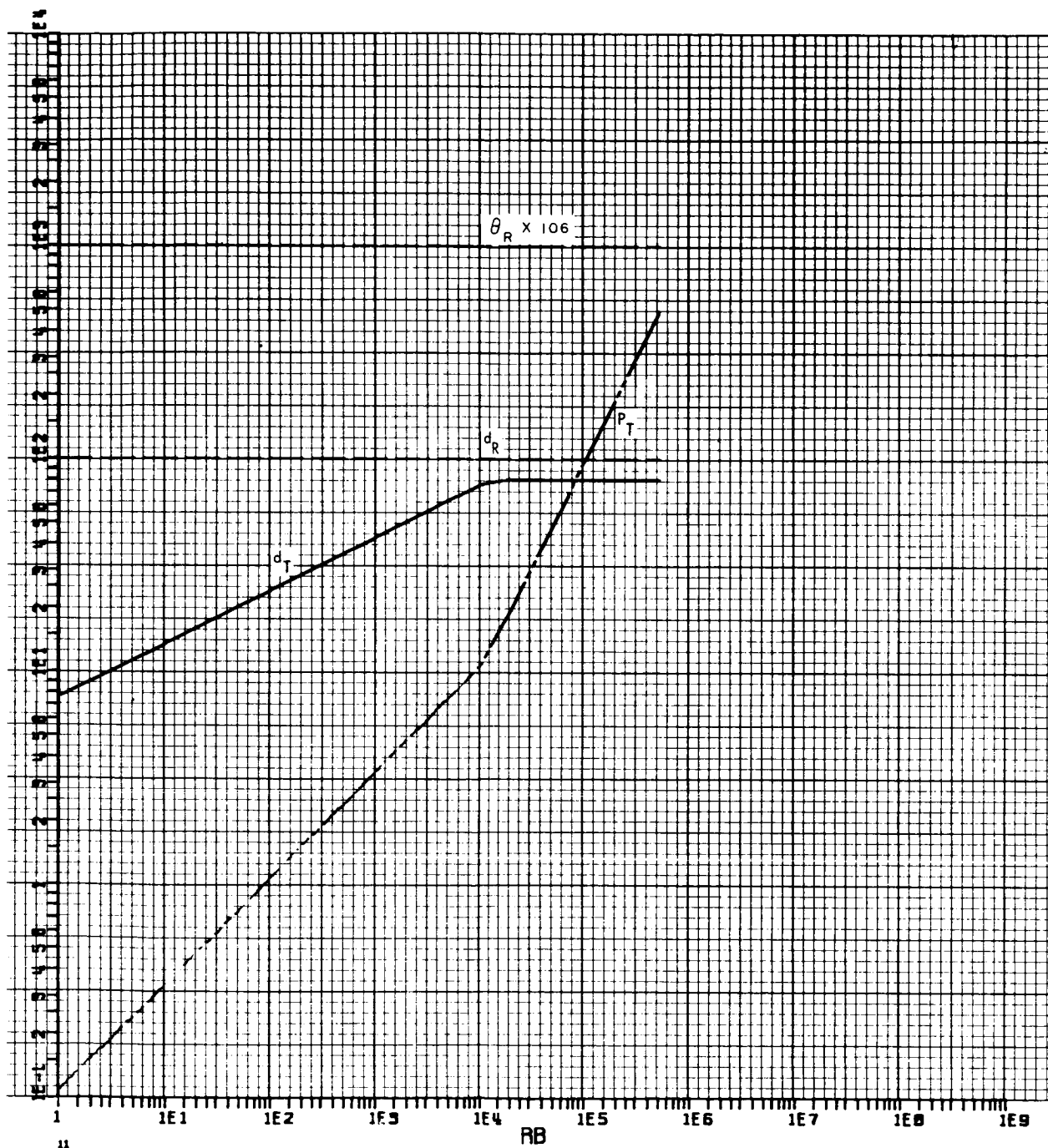
## SYSTEM BURDEN CONSTANTS

|     |    |     |             |     |             |     |    |     |    |     |    |
|-----|----|-----|-------------|-----|-------------|-----|----|-----|----|-----|----|
| KMI | 0. | KNI | 0.26207E 02 | KOT | 0.          | KMR | 0. | KNR | 0. | KOR | 0. |
| KGI | 0. | KHI | 0.32800E 04 | KJT | 0.10619E 05 |     |    |     |    |     |    |

## PARAMETER CONSTRAINTS

|     |             |     |    |     |             |     |    |     |             |       |             |
|-----|-------------|-----|----|-----|-------------|-----|----|-----|-------------|-------|-------------|
| DTI | 0.50000E 02 | GTI | 0. | DRI | 0.10000E 03 | GRI | 0. | PTI | 0.25000E 03 | THERI | 0.10000E-02 |
| DTM | 0.          | GTM | 0. | DRM | 0.10000E 03 | GRM | 0. | PIM | 0.          | THERM | 0.10000E-02 |
| DTB | 0.50000E 02 | GTB | 0. | DRB | 0.10000E 03 | GRB | 0. | PTB | 0.10000E 04 | THERB | 0.10000E-02 |





11

**Example D: Mars Spacecraft Transmitter to Earth Receiver Link**

13 cm wavelength

PCM phase shift keying

Thermal noise limited operation

Transmitter system weight and fabrication cost jointly optimized

Parameters to be optimized:

- a. Transmitter antenna diameter
- b. Transmitter power

Fixed Parameters:

- a. Receiver antenna diameter at 64 meters
- b. Receiver field of view of 1 milliradian

Parameter stops

- a. Transmitter power at 1 kw

Data values:

- a. Transmitter antenna efficiency = 60%
- b. Revised transmitter burdens (1980 estimates)

NAME \_\_\_\_\_ DATE \_\_\_\_\_ PROBLEM EXAMPLE D

COPTRAN INSTRUCTIONS AND DATA

| INSTRUCTION TYPE | 1  | 2  | 3  | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|------------------|----|----|----|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 1                | SP | XM | TR |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 2                | EA | RC | VR |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 3                | RA | NM | AR |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 4                | LA | M  | 13 | C |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 5                | BK | GA | LT |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 6                | PC | M  | /  | P | M |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 6                | RA | D  | H  | O | M |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7                | XM | WT | O  | P |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 7                | XM | F  | C  | O | P |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 8                | GT | G  | R  | O | P |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 9                | NX | P  | W  | S | A |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10               | RB | F  | R  | Q | 0 |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10               | RB | I  | N  | T | 0 |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 10               | RB | F  | I  | N | 7 |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 11               | PR | T  | D  | A | T |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 12               | PL | T  | O  | P | T |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 12               | PL | T  | C  | S |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 12               | PL | T  | W  | A |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 13               | EN | D  | I  | N | S |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
|                  |    |    |    |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 21               | RH | O  | T  |   |   |   |   |   |   |    |    |    |    |    |    | 6  | 0  |    |    |    |    |    |    |    |
| 22               | KP | T  |    |   |   |   |   |   |   |    |    |    |    |    |    | 9  | 6  |    |    |    |    |    |    |    |
| 23               | KW | T  |    |   |   |   |   |   |   |    |    |    |    |    |    |    | 0  | 8  |    |    |    |    |    |    |
| 24               | KH |    |    |   |   |   |   |   |   |    |    |    |    |    |    |    |    | 4  | 6  |    |    |    |    |    |
| 25               | KX |    |    |   |   |   |   |   |   |    |    |    |    |    |    |    | 5  | 6  |    |    | E  | 0  | 3  |    |

SPACECRAFT TRANSMITTER  
EARTH RECEIVER  
MARS RANGE  
13 CM TRANSMISSION WAVELENGTH  
GALACTIC BACKGROUND  
PCM PHASE SHIFT KEYING  
COHERENT RADIO HOMODYNE DETECTION  
XMTR SYSTEM WEIGHT AND XMTR SYSTEM  
FABRICATION COST JOINTLY OPTIMIZED  
TRANSMITTER & RECEIVER ANT GAIN OPTIMIZATION  
RTG XMTR POWER SUPPLY BURDENS  
DATA POINTS AT  $R_B = 10^0, 0.2 \times 10^1, 0.3 \times 10^1,$   
...,  $10^7$  BITS PER SECOND

PRINT SYSTEM DATA AND CONSTANTS  
PLOT OPTIMUM SYSTEM PARAMETERS  
TOTAL COST, AND TRANSMITTER  
OPTIMUM WEIGHT  
END OF COPTRAN INSTRUCTIONS

TRANSMITTER ANTENNA EFFICIENCY  
REVISED TRANSMITTER BURDENS

\*See TABLE IV-1

NAME \_\_\_\_\_ DATE \_\_\_\_\_ PROBLEM EXAMPLE D (continued)

## COPTRAN INSTRUCTIONS AND DATA

INSTRUCTION  
TYPE

|    | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
|----|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 1  | K | E |   |   |   |   |   |   |   |    |    |    |    |    | 2  | 5  |    |    |    |    |    |    |    |    |
| 2  | C | X |   |   |   |   |   |   |   |    |    | 8  | 7  | 5  | 0  |    |    |    |    | E  | +  | 0  | 3  |    |
| 3  | C | H |   |   |   |   |   |   |   |    |    | 6  | 8  | 7  | 5  |    |    |    |    | E  | +  | 0  | 3  |    |
| 4  | W | K | P |   |   |   |   |   |   |    |    | 2  | 5  |    |    |    |    |    |    |    |    |    |    |    |
| 5  | W | K | H |   |   |   |   |   |   |    |    |    |    |    | 0  |    |    |    |    |    |    |    |    |    |
| 6  | G | T |   |   |   |   |   |   |   |    |    | 1  |    |    |    |    |    |    |    |    |    |    |    |    |
| 7  | H | T |   |   |   |   |   |   |   |    |    | 1  |    |    |    |    |    |    |    |    |    |    |    |    |
| 8  | J | T |   |   |   |   |   |   |   |    |    | 1  |    |    |    |    |    |    |    |    |    |    |    |    |
| 9  | G | R | M |   |   |   |   |   |   |    |    | 1  | 9  |    |    |    |    |    |    | E  | +  | 0  | 6  |    |
| 10 | P | T | B |   |   |   |   |   |   |    |    | 1  |    |    |    |    |    |    |    | E  | +  | 0  | 3  |    |
| 11 | T | H | E | R | M |   |   |   |   |    |    | 1  |    |    |    |    |    |    |    | E  | -  | 0  | 3  |    |
| 12 | N | C | R | M | N | T |   |   |   |    |    | 1  | 5  |    |    |    |    |    |    |    |    |    |    |    |
| 13 | S | N |   |   |   |   |   |   |   |    |    | 2  | 0  |    |    |    |    |    |    |    |    |    |    |    |
| 14 | F | I | N | A | L | E |   |   |   |    |    | 5  | 0  |    |    |    |    |    |    |    |    |    |    |    |
| 15 | E | N | D | D | A | T |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 16 | E | N | D | C | A | S |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 17 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 18 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 19 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 20 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 21 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 22 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 23 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 24 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
| 25 |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |

REVISED TRANSMITTER BURDENS

GAIN FOR 64 METER FIXED RECEIVER ANT. DIAM.

1 KW STOP ON XMTR POWER

1 MILLIRADIAN FIXED RECEIVER FIELD ON VIEW

INCREMENT SN FROM 20 TO 50

IN STEP SIZES OF 15

END OF COPTRAN DATA

END OF CASES

\*See TABLE IV-1

|   |           |
|---|-----------|
| SPACECRAFT TRANSMITTER  |           |
| EARTH RECEIVER  |           |
| MARS RANGE (1.68 KM)  |           |
| TRANSMISSION WAVELENGTH LAMBDA = 13 CM                          |           |
| GALACTIC BACKGROUND   |           |
| PCM PHASE MODULATION  |           |
| RADIO HOMODYNE DETECTION  |           |
| TRANSMITTER WEIGHT OPTIMIZATION                                 |           |
| TRANSMITTER FABRICATION COST OPTIMIZATION                       |           |
| TRANSMITTER ANTENNA GAIN AND RECEIVER ANTENNA GAIN OPTIMIZATION |           |
| *** COPTRAN PROGRAM ***   |           |
| SPXNTR  |           |
| EACVTR  |           |
| RAHAR   |           |
| LAM13C  |           |
| BKGALT  |           |
| PCM/PM  |           |
| RADNOM  |           |
| XMTOP   |           |
| XMFCOP  |           |
| GIGROP  |           |
| NXPNSA  |           |
| R8FR00  |           |
| R8INT0  |           |
| R8EINZ  |           |
| PRFALL  |           |
| PLIOPT  |           |
| PLICS   |           |
| PLIWA   |           |
| ENDINS  |           |
| RHOT  | 0.600     |
| KPT   | 96.0      |
| KMI   | 0.800E-01 |
| KH  | 0.460     |
| KX  | 0.560E-02 |
| KE  | 0.250     |
| CX  | 0.875E 04 |
| CH  | 0.688E 04 |
| WKP   | 2.50      |
| WKH   | 0.        |
| GT  | 1.00      |
| HT  | 1.00      |
| JT  | 1.00      |
| GRM   | 0.190E 07 |
| PIB   | 0.100E 04 |
| THERM   | 0.100E-02 |
| MCRMNT  | 15.0      |
| SN  | 20.0      |
| FINALE  | 50.0      |
| ENDAT   | 0.        |



[illegible]

### SIGNAL-TO-NOISE RATIO CONSTANTS

|   |    |    |    |    |    |    |             |    |    |
|---|----|----|----|----|----|----|-------------|----|----|
| K | 0. | KM | 0. | KM | 0. | KR | 0.09534E-07 | KS | 0. |
|---|----|----|----|----|----|----|-------------|----|----|

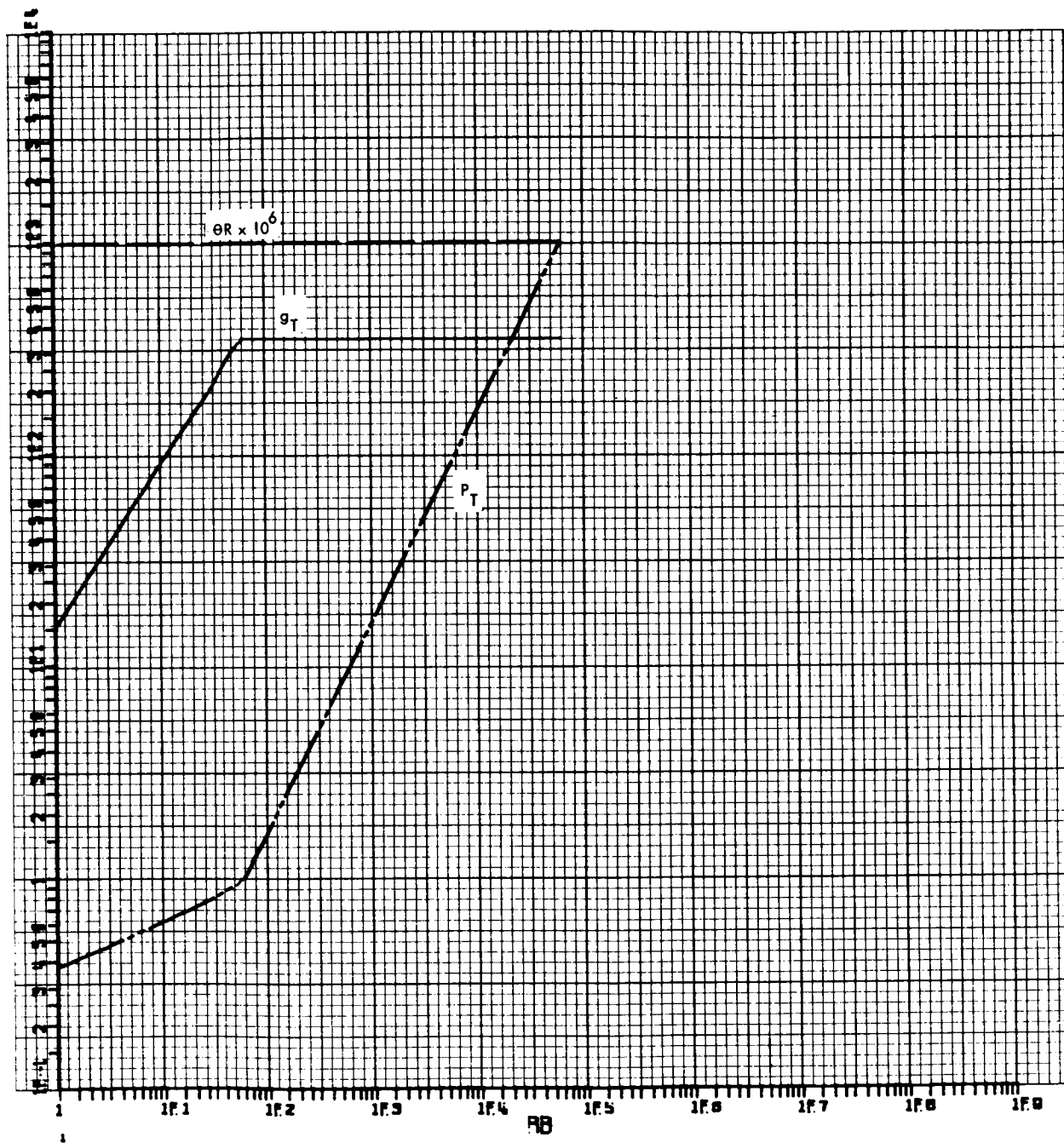
### SYSTEM BURDEN CONSTANTS

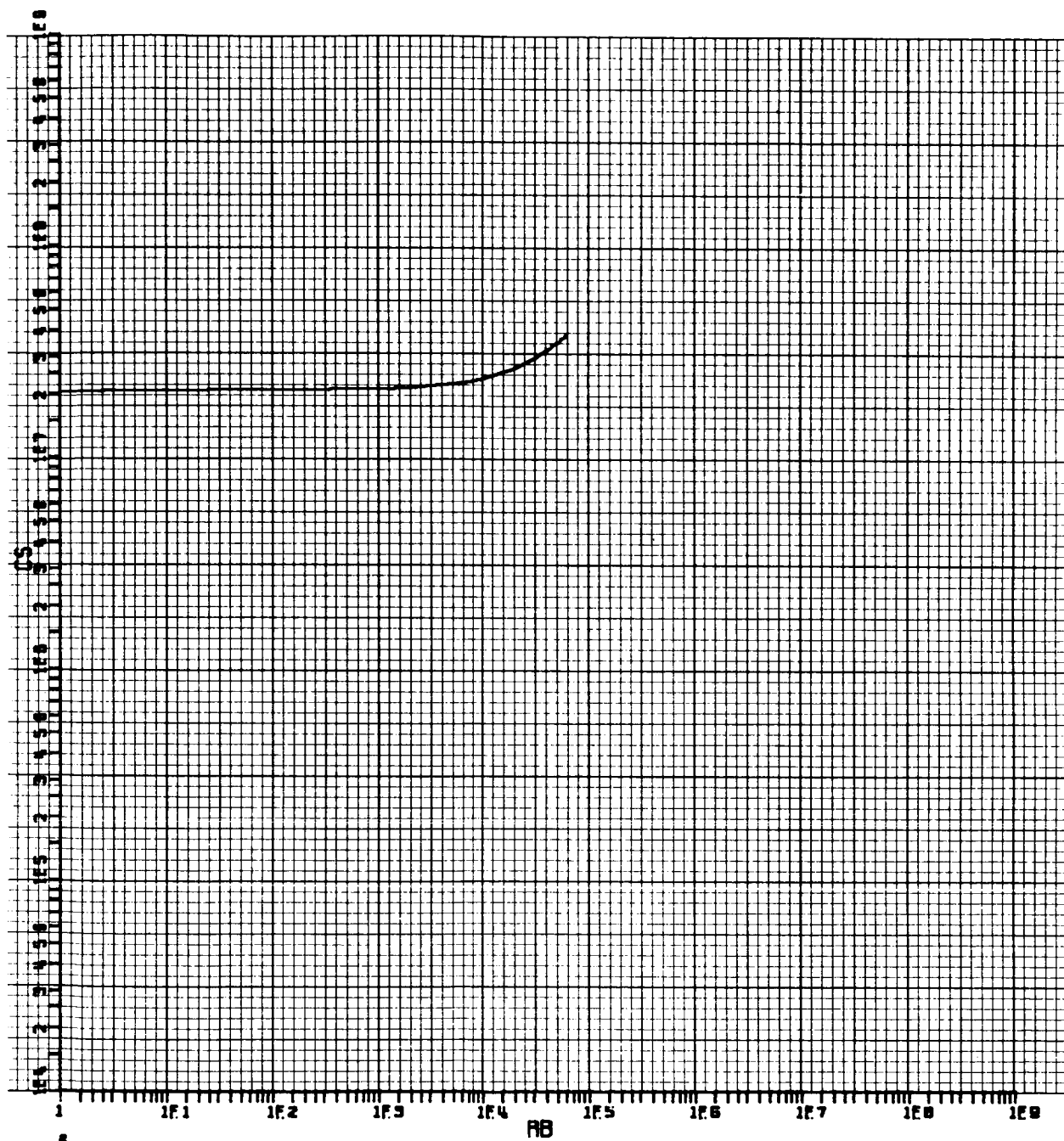
|     |    |     |            |     |    |     |    |
|-----|----|-----|------------|-----|----|-----|----|
| KNT | 0. | KOT | 0.7100E 05 | KNR | 0. | KOR | 0. |
|-----|----|-----|------------|-----|----|-----|----|

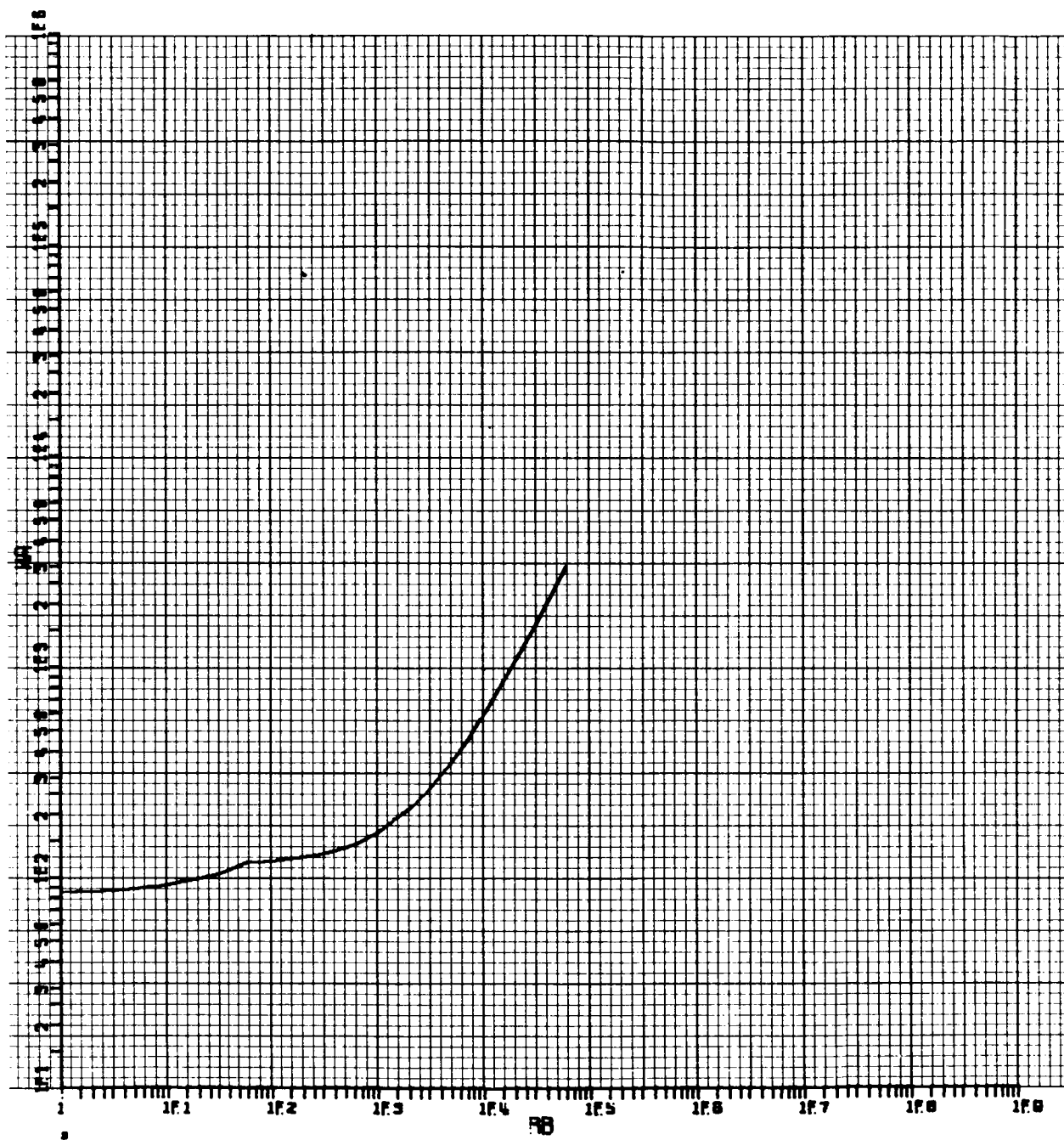
|     |             |     |             |     |             |
|-----|-------------|-----|-------------|-----|-------------|
| KG7 | 0.96000E 02 | KWT | 0.13120E 03 | KJT | 0.16621E 05 |
|-----|-------------|-----|-------------|-----|-------------|

## PARAMETER CONSTRAINTS

|      |    |     |             |     |    |     |             |     |             |       |             |
|------|----|-----|-------------|-----|----|-----|-------------|-----|-------------|-------|-------------|
| DTII | 0. | GII | 0.17400E 03 | DRI | 0. | GRI | 0.19000E 07 | PII | 0.50000E 03 | IHERI | 0.10000E-02 |
| DTM  | 0. | GTW | 0.          | DRM | 0. | GRM | 0.19000E 07 | PTM | 0.          | THERM | 0.10000E-02 |
| DTB  | 0. | GIB | 0.34800E 03 | DRB | 0. | GRB | 0.19000E 07 | PIB | 0.10000E 04 | IHERB | 0.10000E-02 |







|   |           |
|---|-----------|
| SPACECRAFT TRANSMITTER  |           |
| EARTH RECEIVER  |           |
| MARS RANGE (1.68 KM)  |           |
| TRANSMISSION WAVELENGTH LAMBDA = 13 CM                          |           |
| GALACTIC BACKGROUND   |           |
| PCM PHASE MODULATION  |           |
| RADIO HOMODYNE DETECTION  |           |
| TRANSMITTER WEIGHT OPTIMIZATION                                 |           |
| TRANSMITTER FABRICATION COST OPTIMIZATION                       |           |
| TRANSMITTER ANTENNA GAIN AND RECEIVER ANTENNA GAIN OPTIMIZATION |           |
| *** COPTRAM PROGRAM ***   |           |
| SPXMR   |           |
| EARCVR  |           |
| RAHAR   |           |
| LAMJC   |           |
| BKGALT  |           |
| PCM/PM  |           |
| RADROM  |           |
| XMTOP   |           |
| XMFCOP  |           |
| GTGRP   |           |
| NXPHSA  |           |
| RBFR00  |           |
| RBINT0  |           |
| RBFIN7  |           |
| PRTALL  |           |
| PLIOPT  |           |
| PLICS   |           |
| PLTMA   |           |
| ENDINS  |           |
| RHOT  | 0.600     |
| KPT   | 96.0      |
| KWT   | 0.800E-01 |
| KH  | 0.460     |
| KX  | 0.560E-02 |
| KE  | 0.250     |
| CX  | 0.875E 04 |
| CH  | 0.688E 04 |
| WKP   | 2.50      |
| WKH   | 0.        |
| GT  | 1.00      |
| HT  | 1.00      |
| JT  | 1.00      |
| GRM   | 0.190E 07 |
| PTB   | 0.100E 04 |
| THERM   | 0.100E-02 |
| NCRMNT  | 15.0      |
| SN  | 20.0      |
| FINALE  | 50.0      |
| ENDDAT  | 0.        |

| SYSTEM BURDENS DATA                               |        |           |       |          |      |          |       |         |         |         |         |          |
|---|--------|-----------|-------|----------|------|----------|-------|---------|---------|---------|---------|----------|
| TRANSMITTER<br>ANTENNA                            | HTHT   | 520.00000 | HDI   | 0.01350  | CKT  | 5000.00  | WKT   | 0.      | MT      | 1.00    | MT      | 1.00000  |
| RECEIVER<br>ANTENNA                               | HTHR   | 0.06600   | HDR   | 0.       | CKR  | 0.       | WKR   | 0.      | MR      | 1.35    | MR      | 0.       |
| TRANSMITTER<br>ACQUISITION<br>AND TRACK<br>SYSTEM | KAT    | 71000.    | KWAT  | 0.75000  | KPOT | 10.00000 | CAI   | 140000. | WBT     | 10.000  | QT      | 0.30000  |
| RECEIVER<br>ACQUISITION<br>AND TRACK<br>SYSTEM    | KAR    | 0.        | KWAR  | 0.       | KPOR | 0.       | CAR   | 0.      | WBR     | 0.      | QR      | 0.       |
| TRANSMITTER                                       | KPT    | 96.00000  | KWT   | 0.08000  | KH   | 0.46000  | KX    | 0.00560 | KE      | 0.25000 | CKP     | 17500.00 |
| CKH   | 23800. | WKP       | 2.500 | WKH      | 0.   | JT       | 1.000 | GT      | 1.00000 | HT      | 1.00000 |          |
| MODULATION<br>EQUIPMENT                           | KFM    | 0.        | KM    | 0.       | KPM  | 0.       | CKM   | 0.      | WKM     | 0.      |         |          |
| DEMODULATION<br>EQUIPMENT                         | KFD    | 0.        | KD    | 0.       | KPD  | 0.       | CKD   | 0.      | WKD     | 0.      |         |          |
| TRANSMITTER<br>POWER SUPPLY                       | KST    | 3000.000  | KWST  | 0.700000 | CKE  | 0.       | WKE   | 0.      |         |         |         |          |
| RECEIVER<br>POWER SUPPLY                          | KSR    | 25.000    | KWSR  | 0.       | CKF  | 10000.   | WKF   | 0.      |         |         |         |          |
| BOOSTER<br>BURDENS                                | KSA    | 1640.000  | KSB   | 1640.000 |      |          |       |         |         |         |         |          |
| .....   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
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|   |        |           |       |          |      |          |       |         |         |         |         |          |
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|   |        |           |       |          |      |          |       |         |         |         |         |          |
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|   |        |           |       |          |      |          |       |         |         |         |         |          |
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|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
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|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
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|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
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|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
|   |        |           |       |          |      |          |       |         |         |         |         |          |
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# SYSTEM PHYSICAL DATA

R 0.1000E 14 LAMBDA 0.1300E 02 S/N 0.3500E 02 C/M 0. 0. USREQ 0. 0. TAU-Y 0.7500E 00

TAU-R 0.3500E 00 TAU-A 0.9500E 00 TE 0.2700E 02 E/A 0. 0. RL 0. 0. LMBD-I 0.

QB 0. RHO-T 0.6000E 00 RHO-R 0.8000E 00

## SIGNAL-TO-NOISE RATIO CONSTANTS

K 0. 0. KN 0. 0. KM 0. 0. KR 0.51162E-07 KS 0. 0.

## SYSTEM BURDEN CONSTANTS

KNT 0. 0. KNT 0. 0. KUT 0.7100E 05 KMR 0. 0. KNR 0. 0. KOR 0. 0.

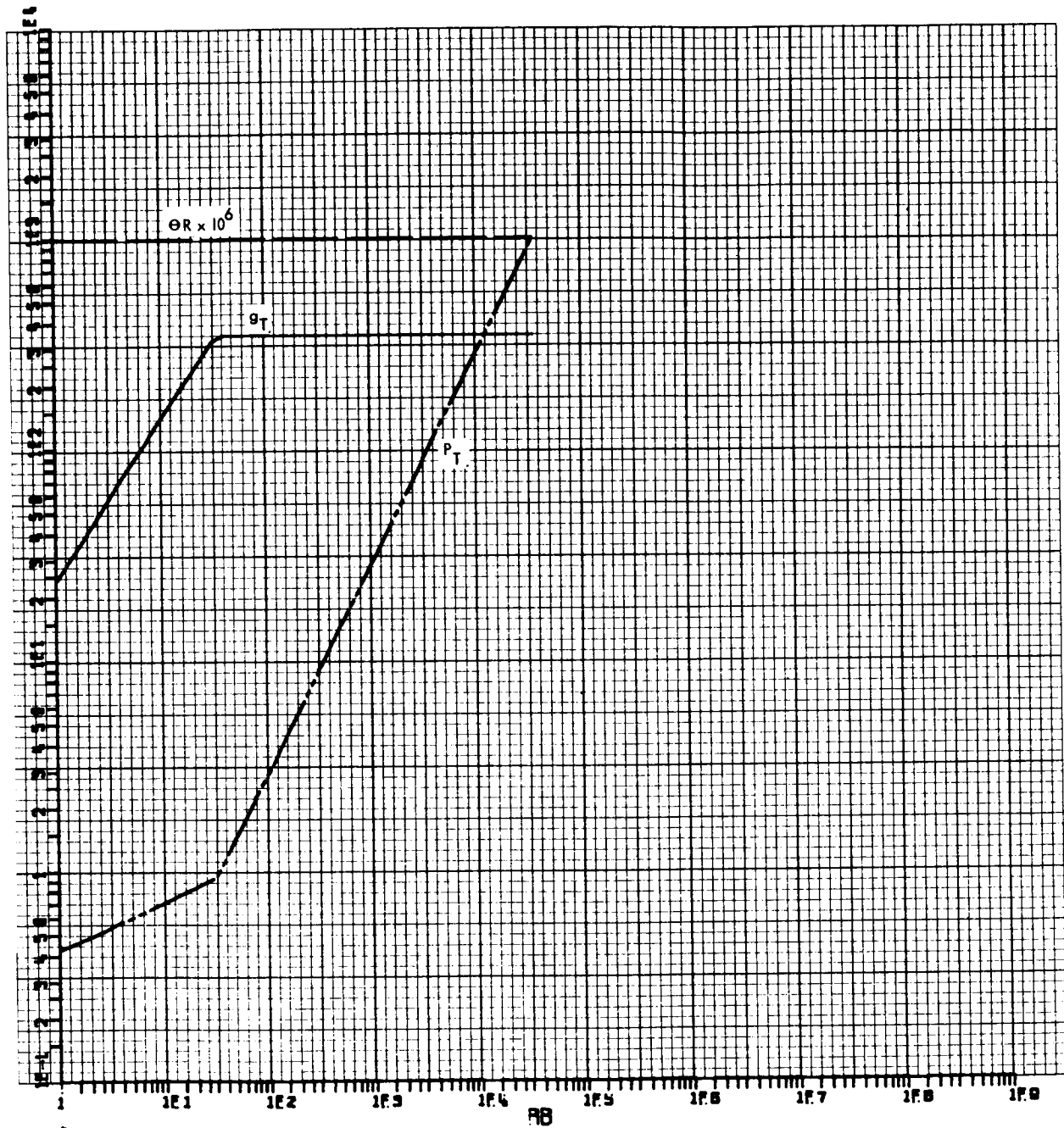
KGT 0.9600E 02 KHT 0.1312E 03 KJT 0.16521E 05

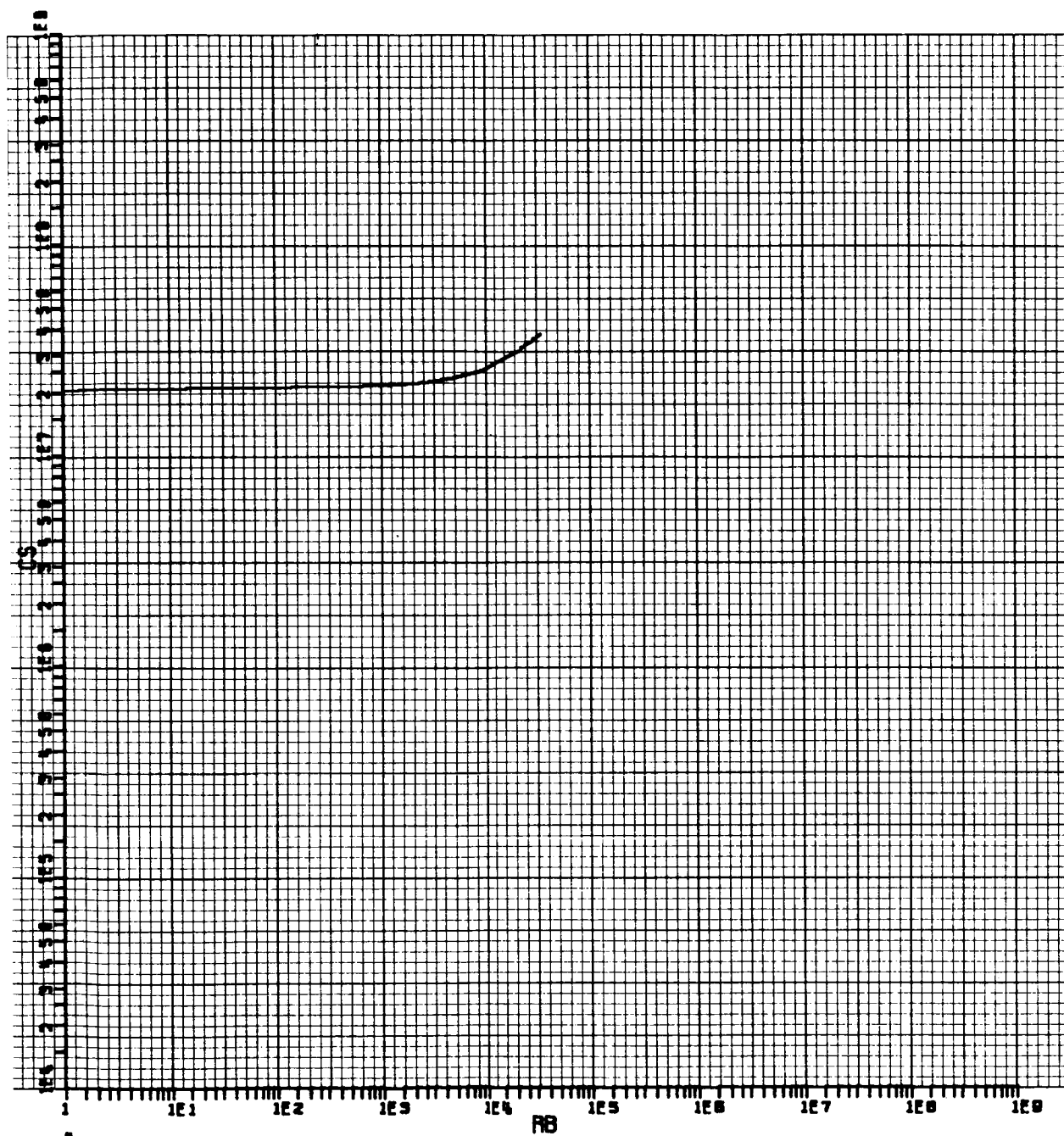
## PARAMETER CONSTRAINTS

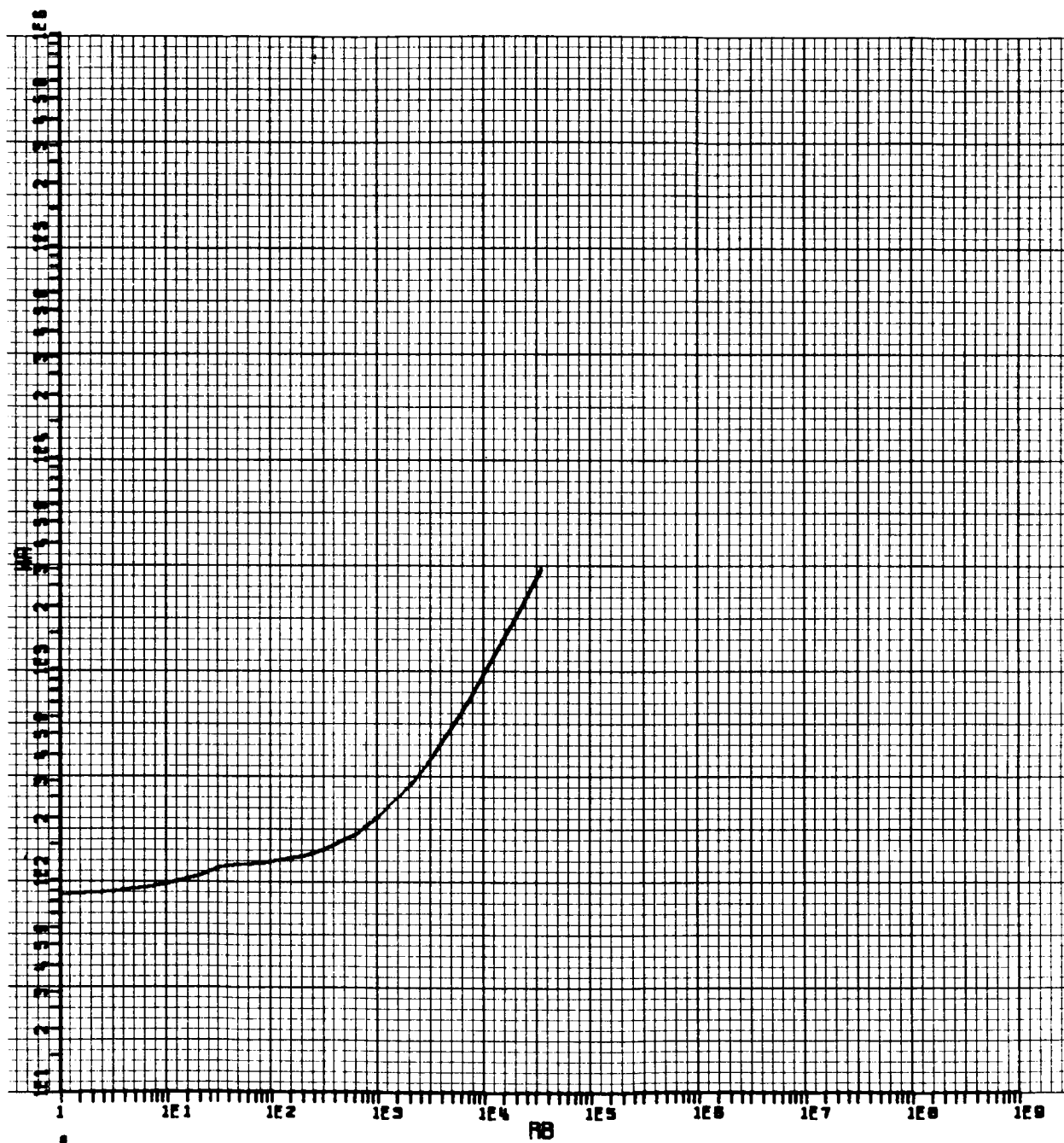
DII 0. 0. GTI 0.1740E 03 DRI 0. 0. GRI 0.1900E 07 PTI 0.5000E 03 THERI 0.1000E-02

DTM 0. 0. GTM 0. 0. DRM 0. 0. GRM 0.1900E 07 PTM 0. 0. THERM 0.1000E-02

DIB 0. 0. GIB 0.3460E 03 DRB 0. 0. GRB 0.1900E 07 PIB 0.1000E 04 THERB 0.1000E-02







# SPACECRAFT TRANSMITTER

EARTH RECEIVER  
MARS RANGE (1.48 KM)  
TRANSMISSION WAVELENGTH LAMBDA = 13 CM  
GALACTIC BACKGROUND  
PCM PHASE MODULATION  
RADIO HOMOZYNE DETECTION  
TRANSMITTER WEIGHT OPTIMIZATION  
TRANSMITTER FABRICATION COST OPTIMIZATION  
TRANSMITTER ANTENNA GAIN AND RECEIVER ANTENNA GAIN OPTIMIZATION

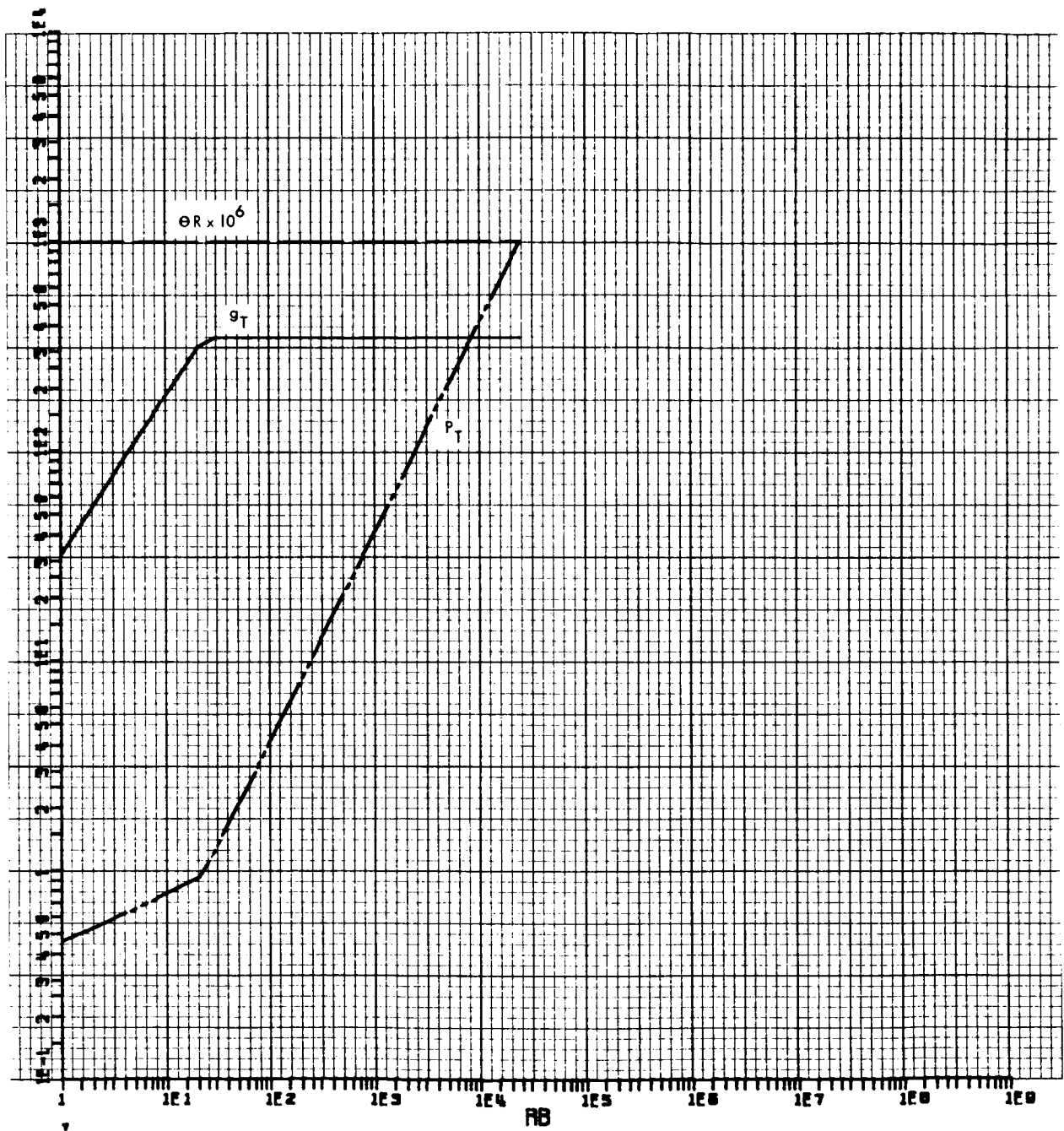
## \*\*\* COPTRAM PROGRAM \*\*\*

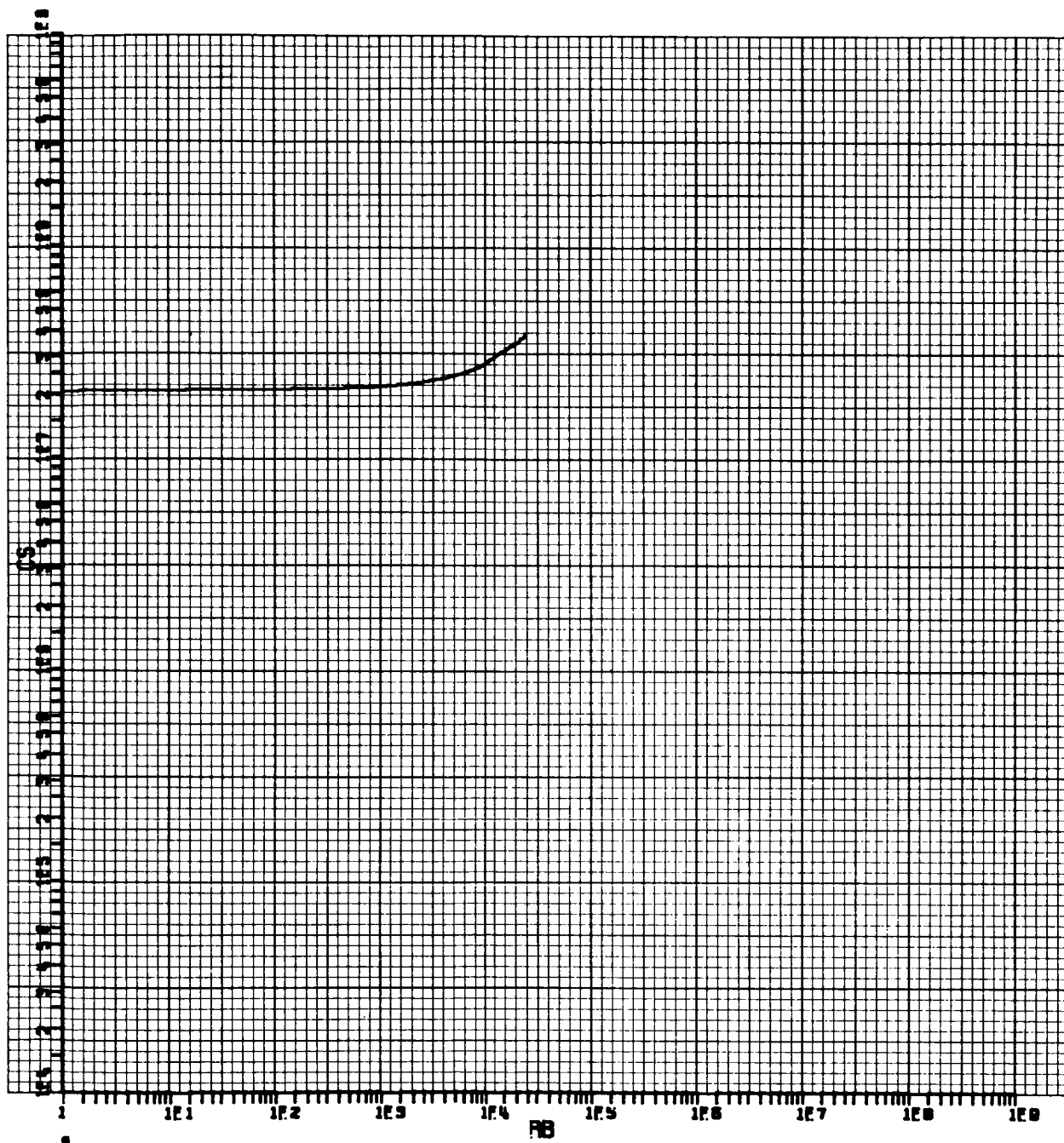
|         |           |
|---------|-----------|
| SPXMTX  |           |
| EARCVR  |           |
| KANMAR  |           |
| LAMBDA  |           |
| BKGALT  |           |
| PCM/PM  |           |
| RADHOM  |           |
| XMTDOP  |           |
| XMF CUP |           |
| GIGROP  |           |
| NXPWSA  |           |
| RBFRQU  |           |
| RBINT0  |           |
| RBFIN7  |           |
| PTALL   |           |
| PLIOPT  |           |
| PLTCS   |           |
| PLTWA   |           |
| ENDINS  | 0.600     |
| RHOT    |           |
| KPT     | 96.0      |
| KWT     | 0.800E-01 |
| KH      | 0.460     |
| KX      | 0.560E-02 |
| KE      | 0.250     |
| CX      | 0.875E 04 |
| CH      | 0.608E 04 |
| MKP     | 2.50      |
| WKH     | 0.        |
| GT      | 1.00      |
| HT      | 1.00      |
| JT      | 1.00      |
| GRM     | 0.190E 07 |
| PIB     | 0.100E 04 |
| THERM   | 0.100E-02 |
| NCRMNT  | 15.0      |
| SN      | 20.0      |
| FINALE  | 50.0      |
| ENDDAT  | 0.        |

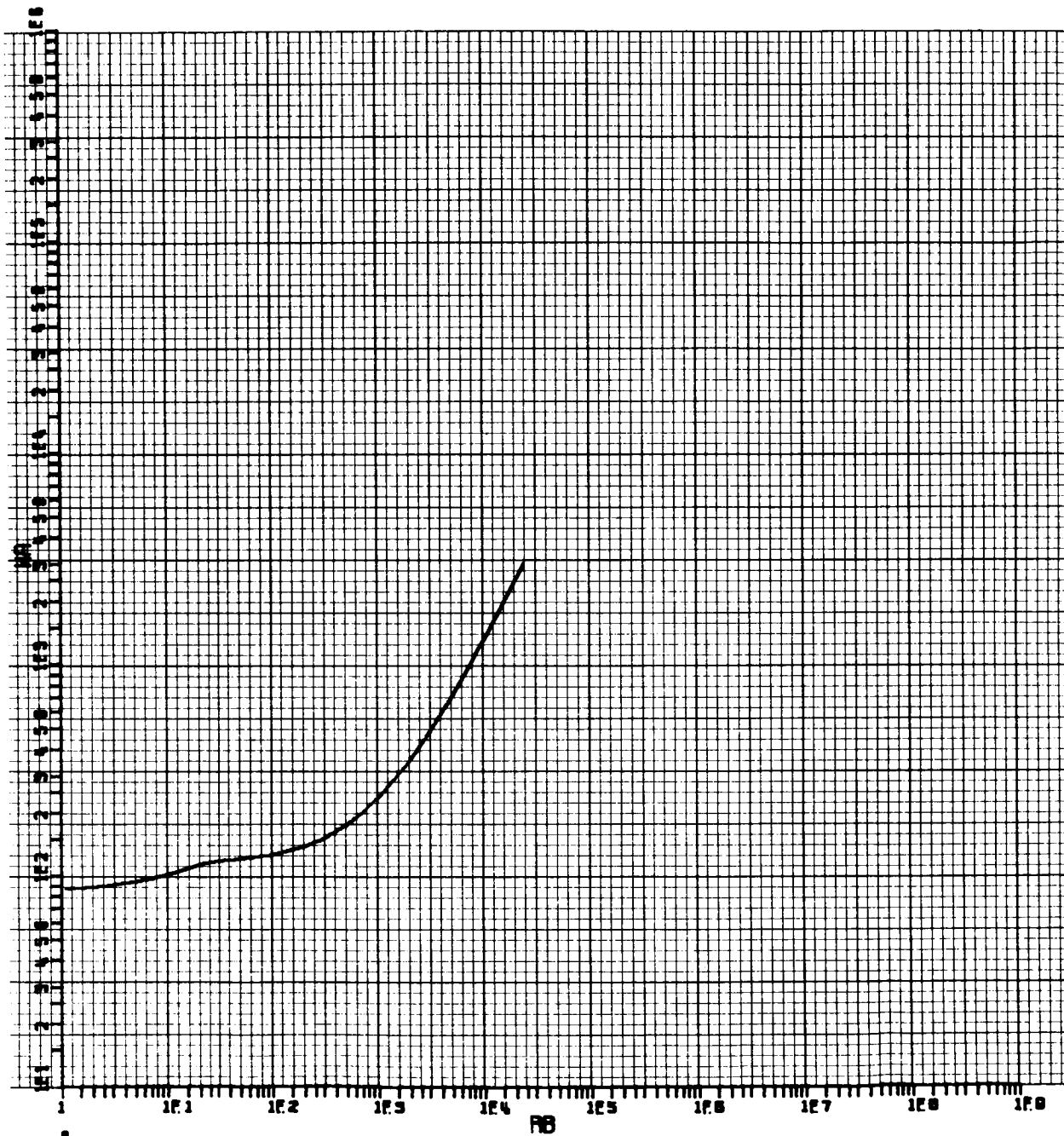
| SYSTEM BURDENS DATA                               |        |           |       |          |      |          |       |         |         |         |         |          |
|---|--------|-----------|-------|----------|------|----------|-------|---------|---------|---------|---------|----------|
| TRANSMITTER<br>ANTENNA                            | MTHT   | 520.00000 | HDT   | 0.01350  | CKT  | 5000.00  | WKT   | 0.      | MT      | 1.00    | MT      | 1.00000  |
| RECEIVER<br>ANTENNA                               | HTHR   | 0.06600   | HDR   | 0.       | CKR  | 0.       | WKR   | 0.      | MR      | 1.35    | MR      | 0.       |
| TRANSMITTER<br>ACQUISITION<br>AND TRACK<br>SYSTEM | KAT    | 71000.    | KWAT  | 0.75000  | KPOT | 10.00000 | CAT   | 140000. | WBT     | 10.000  | GT      | 0.30000  |
| RECEIVER<br>ACQUISITION<br>AND TRACK<br>SYSTEM    | KAR    | 0.        | KWAR  | 0.       | KPOR | 0.       | CAR   | 0.      | WOR     | 0.      | OR      | 0.       |
| TRANSMITTER                                       | KPT    | 96.00000  | KWT   | 0.00000  | KH   | 0.46000  | KX    | 0.00560 | KE      | 0.25000 | CKP     | 17500.00 |
| CKH   | 23000. | WKP       | 2.500 | WKH      | 0.   | JT       | 1.000 | GT      | 1.00000 | MT      | 1.00000 |          |
| MODULATION<br>EQUIPMENT                           | KFM    | 0.        | KM    | 0.       | KPM  | 0.       | CKM   | 0.      | WKM     | 0.      |         |          |
| DEMODULATION<br>EQUIPMENT                         | KFD    | 0.        | KN    | 0.       | KPD  | 0.       | CKD   | 0.      | WKD     | 0.      |         |          |
| TRANSMITTER<br>POWER SUPPLY                       | KST    | 3000.000  | KWST  | 0.700000 | CKE  | 0.       | WKE   | 0.      |         |         |         |          |
| RECEIVER<br>POWER SUPPLY                          | KSR    | 25.000    | KWSR  | 0.       | CKF  | 10000.   | WKF   | 0.      |         |         |         |          |
| BOOSTER<br>BURDENS                                | KSA    | 1640.000  | KSB   | 1640.000 |      |          |       |         |         |         |         |          |
| *****   |        |           |       |          |      |          |       |         |         |         |         |          |

[illegible]

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|-------|----|-----|-------------|-----|----|-----|-------------|-----|-------------|-------|-------------|
| DTI   | 0. | GII | 0.17400E 03 | DRI | 0. | GRI | 0.19000E 07 | PTI | 0.50000E 03 | INERI | 0.10000E-02 |
| DTM   | 0. | GIM | 0.          | DRM | 0. | GRM | 0.19000E 07 | PTM | 0.          | INERM | 0.10000E-02 |
| DTB   | 0. | GIB | 0.34800E 03 | DRB | 0. | GRB | 0.19000E 07 | PTB | 0.10000E 04 | INERB | 0.10000E-02 |
| ***** |    |     |             |     |    |     |             |     |             |       |             |
| ***** |    |     |             |     |    |     |             |     |             |       |             |
| ***** |    |     |             |     |    |     |             |     |             |       |             |
| ***** |    |     |             |     |    |     |             |     |             |       |             |
| ***** |    |     |             |     |    |     |             |     |             |       |             |







#### 4.5 Library of Nominal System Burdens Data for COPTRAN

The following pages contain listings of the nominal System Burdens Data used in the COPTRAN program. (See Table IV-I, instruction No. 9.) Each of those detailed listings is summarized by a single COPTRAN instruction mnemonic.

|        |      |  |  |
|--------|------|--|--|
| NXANTA |      | XMTR ANT BURDENS, 0.51, SPACECRAFT                   |  |
| KHT    | 14.  |  | CONSTANT RELATING XMTR ANT FAB COST TO XMTR ANT DIAMETER |
| KDT    | 1.   | E-02   | CONSTANT RELATING XMTR ANT WEIGHT TO XMTR ANT DIAMETER   |
| CKT    | 20.  | E+03   | XMTR ANT FAB COST INDEPENDENT OF XMTR ANT DIAMETER       |
| WKT    | 25.  |  | XMTR ANT WEIGHT INDEPENDENT OF XMTR ANT DIAMETER         |
| MT     | 2.   |  | EXPONENT RELATING XMTR ANT FAB COST TO XMTR ANT DIAMETER |
| NT     | 2.   |  | EXPONENT RELATING XMTR ANT WEIGHT TO XMTR ANT DIAMETER   |
| NXANTC |      | XMTR ANT BURDENS, 0.84, SPACECRAFT                   |  |
| KHT    | 14.  |  | CONSTANT RELATING XMTR ANT FAB COST TO XMTR ANT DIAMETER |
| KDT    | 1.   | E-02   | CONSTANT RELATING XMTR ANT WEIGHT TO XMTR ANT DIAMETER   |
| CKT    | 20.  | E+03   | XMTR ANT FAB COST INDEPENDENT OF XMTR ANT DIAMETER       |
| WKT    | 25.  |  | XMTR ANT WEIGHT INDEPENDENT OF XMTR ANT DIAMETER         |
| MT     | 2.   |  | EXPONENT RELATING XMTR ANT FAB COST TO XMTR ANT DIAMETER |
| NT     | 2.   |  | EXPONENT RELATING XMTR ANT WEIGHT TO XMTR ANT DIAMETER   |
| NXANTD |      | XMTR ANT BURDENS, 10.6, SPACECRAFT                   |  |
| KHT    | 14.  |  | CONSTANT RELATING XMTR ANT FAB COST TO XMTR ANT DIAMETER |
| KDT    | 1.   | E-02   | CONSTANT RELATING XMTR ANT WEIGHT TO XMTR ANT DIAMETER   |
| CKT    | 20.  | E+03   | XMTR ANT FAB COST INDEPENDENT OF XMTR ANT DIAMETER       |
| WKT    | 25.  |  | XMTR ANT WEIGHT INDEPENDENT OF XMTR ANT DIAMETER         |
| MT     | 2.   |  | EXPONENT RELATING XMTR ANT FAB COST TO XMTR ANT DIAMETER |
| NT     | 2.   |  | EXPONENT RELATING XMTR ANT WEIGHT TO XMTR ANT DIAMETER   |
| NXANF  |      | XMTR ANT BURDENS, 13CM, DIAMETER BURDENS, SPACECRAFT |  |
| KHT    | 16.7 |  | CONSTANT RELATING XMTR ANT FAB COST TO XMTR ANT DIAMETER |
| KDT    | 4.32 | E-04   | CONSTANT RELATING XMTR ANT WEIGHT TO XMTR ANT DIAMETER   |
| CKT    | 5.   | E+03   | XMTR ANT FAB COST INDEPENDENT OF XMTR ANT DIAMETER       |
| WKT    | 0.   |  | XMTR ANT WEIGHT INDEPENDENT OF XMTR ANT DIAMETER         |
| MT     | 2.   |  | EXPONENT RELATING XMTR ANT FAB COST TO XMTR ANT DIAMETER |
| NT     | 2.   |  | EXPONENT RELATING XMTR ANT WEIGHT TO XMTR ANT DIAMETER   |
| NXANTG |      | XMTR ANT BURDENS, 13CM, GAIN BURDENS, SPACECRAFT     |  |
| KHT    | 5.2  | E+02   | CONSTANT RELATING XMTR ANT FAB COST TO XMTR ANT DIAMETER |
| KDT    | 1.35 | E-02   | CONSTANT RELATING XMTR ANT WEIGHT TO XMTR ANT DIAMETER   |
| CKT    | 5.   | E+03   | XMTR ANT FAB COST INDEPENDENT OF XMTR ANT DIAMETER       |
| WKT    | 0.   |  | XMTR ANT WEIGHT INDEPENDENT OF XMTR ANT DIAMETER         |
| MT     | 1.   |  | EXPONENT RELATING XMTR ANT FAB COST TO XMTR ANT DIAMETER |
| NT     | 1.   |  | EXPONENT RELATING XMTR ANT WEIGHT TO XMTR ANT DIAMETER   |

|         |          |  |
|---------|----------|--|
| NRANT A |          | RCVR ANT BURDENS, 0.51, OPT DIRECT DETECTION, EARTH      |
| KTHR    | 8.75     | CONSTANT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| KDR     | .023     | CONSTANT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER   |
| CKR     | 25. E+03 | RCVR ANT FAB COST INDEPENDENT OF RCVR ANT DIAMETER       |
| WKR     | 20.      | RCVR ANT WEIGHT INDEPENDENT OF RCVR ANT DIAMETER         |
| MR      | 2.       | EXPONENT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| NR      | 2.       | EXPONENT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER   |
| NRANT B |          | RCVR ANT BURDENS, 0.51, OPT HET OR HOM DETECTION, EARTH  |
| KTHR    | 8.75     | CONSTANT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| KDR     | .023     | CONSTANT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER   |
| CKR     | 25. E+03 | RCVR ANT FAB COST INDEPENDENT OF RCVR ANT DIAMETER       |
| WKR     | 20.      | RCVR ANT WEIGHT INDEPENDENT OF RCVR ANT DIAMETER         |
| MR      | 2.       | EXPONENT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| NR      | 2.       | EXPONENT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER   |
| NRANT C |          | RCVR ANT BURDENS, 0.84, OPT DIRECT DETECTION, EARTH      |
| KTHR    | 8.75     | CONSTANT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| KDR     | .023     | CONSTANT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER   |
| CKR     | 25. E+03 | RCVR ANT FAB COST INDEPENDENT OF RCVR ANT DIAMETER       |
| WKR     | 20.      | RCVR ANT WEIGHT INDEPENDENT OF RCVR ANT DIAMETER         |
| MR      | 2.       | EXPONENT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| NR      | 2.       | EXPONENT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER   |
| NRANT D |          | RCVR ANT BURDENS, 10.6, OPT DIRECT DETECTION, EARTH      |
| KTHR    | 8.75     | CONSTANT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| KDR     | .023     | CONSTANT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER   |
| CKR     | 25. E+03 | RCVR ANT FAB COST INDEPENDENT OF RCVR ANT DIAMETER       |
| WKR     | 20.      | RCVR ANT WEIGHT INDEPENDENT OF RCVR ANT DIAMETER         |
| MR      | 2.       | EXPONENT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| NR      | 2.       | EXPONENT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER   |
| NRANT E |          | RCVR ANT BURDENS, 10.6, OPT HET OR HOM DETECTION, EARTH  |
| KTHR    | 8.75     | CONSTANT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| KDR     | .023     | CONSTANT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER   |
| CKR     | 25. E+03 | RCVR ANT FAB COST INDEPENDENT OF RCVR ANT DIAMETER       |
| WKR     | 20.      | RCVR ANT WEIGHT INDEPENDENT OF RCVR ANT DIAMETER         |
| MR      | 2.       | EXPONENT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| NR      | 2.       | EXPONENT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER   |

|        |     |   |
|--------|-----|---|
| NRANTF |     | RCVR ANT BURDENS, 13CM, DIAMETER BURDENS, EARTH               |
| KTHR   | 6.4 | E-04 CONSTANT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| KDR    | .0  | CONSTANT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER        |
| CKR    | 0.  | RCVR ANT FAB COST INDEPENDENT OF RCVR ANT DIAMETER            |
| WKR    | .0  | RCVR ANT WEIGHT INDEPENDENT OF RCVR ANT DIAMETER              |
| MR     | 2.7 | EXPONENT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER      |
| NR     | .0. | EXPONENT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER        |

|        |      |   |
|--------|------|---|
| NRANTG |      | RCVR ANT BURDENS, 13CM, GAIN BURDENS, EARTH                   |
| KTHR   | 6.6  | E-02 CONSTANT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER |
| KDR    |      | CONSTANT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER        |
| CKR    |      | RCVR ANT FAB COST INDEPENDENT OF RCVR ANT DIAMETER            |
| WKR    |      | RCVR ANT WEIGHT INDEPENDENT OF RCVR ANT DIAMETER              |
| MR     | 1.35 | EXPONENT RELATING RCVR ANT FAB COST TO RCVR ANT DIAMETER      |
| NR     |      | EXPONENT RELATING RCVR ANT WEIGHT TO RCVR ANT DIAMETER        |

|        |          |   |
|--------|----------|---|
| NXACTA |          | XMTR ACQ AND TRACK BURDENS, OPTICAL FREQUENCY, SPACECRAFT |
| KAT    | .71 E+05 | CONSTANT RELATING XMTR TRACK EQUIP FAB COST TO XMTR BEAM  |
| KWAT   | .46      | CONSTANT RELATING XMTR TRACK EQUIP WEIGHT TO XMTR ANT WT  |
| KPQT   | .48      | CONSTANT RELATING XMTR ACQ-TRACK EQUIP PWR REQ TO WEIGHT  |
| CAT    | .4 E+06  | XMTR ACQ-TRACK EQUIP FAB COST INDEPENDENT OF XMTR BEAM    |
| WBT    | 5.       | XMTR ACQ-TRACK EQUIP WEIGHT INDEPENDENT OF XMTR BEAM      |
| QT     | .3       | EXPONENT RELATING XMTR TRACK EQUIP FAB COST TO XMTR BEAM  |

|        |          |  |
|--------|----------|--|
| NXACTB |          | XMTR ACQ AND TRACK BURDENS, RADIO FREQUENCY, SPACE, DIAM |
| KAT    | .71 E+05 | CONSTANT RELATING XMTR TRACK EQUIP FAB COST TO XMTR BEAM |
| KWAT   | .75      | CONSTANT RELATING XMTR TRACK EQUIP WEIGHT TO XMTR ANT WT |
| KPQT   | 10.      | CONSTANT RELATING XMTR ACQ-TRACK EQUIP PWR REQ TO WEIGHT |
| CAT    | .14 E+06 | XMTR ACQ-TRACK EQUIP FAB COST INDEPENDENT OF XMTR BEAM   |
| WBT    | 10.      | XMTR ACQ-TRACK EQUIP WEIGHT INDEPENDENT OF XMTR BEAM     |
| QT     | .3       | EXPONENT RELATING XMTR TRACK EQUIP FAB COST TO XMTR BEAM |

|        |          |  |
|--------|----------|--|
| NXACTC |          | XMTR ACQ AND TRACK BURDENS, RADIO FREQUENCY, SPACE, GAIN |
| KAT    | .71 E+05 | CONSTANT RELATING XMTR TRACK EQUIP FAB COST TO XMTR BEAM |
| KWAT   | .75      | CONSTANT RELATING XMTR TRACK EQUIP WEIGHT TO XMTR ANT WT |
| KPQT   | 10.      | CONSTANT RELATING XMTR ACQ-TRACK EQUIP PWR REQ TO WEIGHT |
| CAT    | .14 E+06 | XMTR ACQ-TRACK EQUIP FAB COST INDEPENDENT OF XMTR BEAM   |
| WBT    | 10.      | XMTR ACQ-TRACK EQUIP WEIGHT INDEPENDENT OF XMTR BEAM     |
| QT     | .3       | EXPONENT RELATING XMTR TRACK EQUIP FAB COST TO XMTR BEAM |

|        |          |  |
|--------|----------|--|
| NRAC†A |          | RCVR ACQ AND TRACK BURDENS, OPTICAL FREQUENCY, EARTH     |
| KAR    | .71 E+05 | CONSTANT RELATING RCVR TRACK EQUIP FAB COST TO RCVR BEAM |
| KWAR   | .46      | CONSTANT RELATING RCVR TRACK EQUIP WEIGHT TO RCVR ANT WT |
| KPQR   | .48      | CONSTANT RELATING XMTR ACQ-TRACK EQUIP PWR REQ TO WEIGHT |
| EAR    | .2 E+06  | RCVR ACQ-TRACK EQUIP FAB COST INDEPENDENT OF RCVR BEAM   |
| WBR    | 5.0      | RCVR ACQ-TRACK EQUIP WEIGHT INDEPENDENT OF RCVR BEAM     |
| QR     | .3       | EXPONENT RELATING RCVR TRACK EQUIP FAB COST TO RCVR BEAM |

|        |    |  |
|--------|----|--|
| NRAC†B |    | RCVR ACQ AND TRACK BURDENS, RADIO FREQUENCY, EARTH, DIAM |
| KAR    | .0 | CONSTANT RELATING RCVR TRACK EQUIP FAB COST TO RCVR BEAM |
| KWAR   | .0 | CONSTANT RELATING RCVR TRACK EQUIP WEIGHT TO RCVR ANT WT |
| KPQR   | .0 | CONSTANT RELATING XMTR ACQ-TRACK EQUIP PWR REQ TO WEIGHT |
| EAR    | .0 | RCVR ACQ-TRACK EQUIP FAB COST INDEPENDENT OF RCVR BEAM   |
| WBR    | .0 | RCVR ACQ-TRACK EQUIP WEIGHT INDEPENDENT OF RCVR BEAM     |
| QR     | .0 | EXPONENT RELATING RCVR TRACK EQUIP FAB COST TO RCVR BEAM |

|        |    |  |
|--------|----|--|
| NRAC†C |    | RCVR ACQ AND TRACK BURDENS, RADIO FREQUENCY, EARTH, GAIN |
| KAR    | .0 | CONSTANT RELATING RCVR TRACK EQUIP FAB COST TO RCVR BEAM |
| KWAR   | .0 | CONSTANT RELATING RCVR TRACK EQUIP WEIGHT TO RCVR ANT WT |
| KPQR   | .0 | CONSTANT RELATING XMTR ACQ-TRACK EQUIP PWR REQ TO WEIGHT |
| EAR    | .0 | RCVR ACQ-TRACK EQUIP FAB COST INDEPENDENT OF RCVR BEAM   |
| WBR    | .0 | RCVR ACQ-TRACK EQUIP WEIGHT INDEPENDENT OF RCVR BEAM     |
| QR     | .0 | EXPONENT RELATING RCVR TRACK EQUIP FAB COST TO RCVR BEAM |

|        |     |      |  |
|--------|-----|------|--|
| NMODEA |     |      | MODULATION EQUIP BURDENS, 0.51, CW LASER, SPACECRAFT     |
| KFM    | 7.5 | E-05 | CONSTANT RELATING MOD EQUIP FAB COST TO INFORMATION RATE |
| KM     | 5.  | E-08 | CONSTANT RELATING MOD EQUIP WEIGHT TO INFORMATION RATE   |
| KPM    | 5.  |      | CONSTANT RELATING MOD EQUIP PWR REQ TO EQUIP WEIGHT      |
| CKM    | 7.5 | E+03 | MOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE       |
| WKM    | 5.  |      | MOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE         |
| NMODEB |     |      | MODULATION EQUIP BURDENS, 0.84, CW LASER, SPACECRAFT     |
| KFM    | 7.5 | E-05 | CONSTANT RELATING MOD EQUIP FAB COST TO INFORMATION RATE |
| KM     | 5.  | E-08 | CONSTANT RELATING MOD EQUIP WEIGHT TO INFORMATION RATE   |
| KPM    | 5.  |      | CONSTANT RELATING MOD EQUIP PWR REQ TO EQUIP WEIGHT      |
| CKM    | 7.5 | E+03 | MOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE       |
| WKM    | 5.  |      | MOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE         |
| NMODEC |     |      | MODULATION EQUIP BURDENS, 0.84, PULSED LASER, SPACECRAFT |
| KFM    | .5  | E-03 | CONSTANT RELATING MOD EQUIP FAB COST TO INFORMATION RATE |
| KM     | .3  | E-06 | CONSTANT RELATING MOD EQUIP WEIGHT TO INFORMATION RATE   |
| KPM    | 5.  |      | CONSTANT RELATING MOD EQUIP PWR REQ TO EQUIP WEIGHT      |
| CKM    | 15. | E+03 | MOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE       |
| WKM    | 10. |      | MOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE         |
| NMODED |     |      | MODULATION EQUIP BURDENS, 10.6, CW LASER, SPACECRAFT     |
| KFM    | .5  | E-03 | CONSTANT RELATING MOD EQUIP FAB COST TO INFORMATION RATE |
| KM     | .3  | E-06 | CONSTANT RELATING MOD EQUIP WEIGHT TO INFORMATION RATE   |
| KPM    | 5.  |      | CONSTANT RELATING MOD EQUIP PWR REQ TO EQUIP WEIGHT      |
| CKM    | 15. | E+03 | MOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE       |
| WKM    | 10. |      | MOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE         |
| NMODEE |     |      | MODULATION EQUIP BURDENS, 13CM, SPACECRAFT               |
| KFM    | .0  |      | CONSTANT RELATING MOD EQUIP FAB COST TO INFORMATION RATE |
| KM     | .0  |      | CONSTANT RELATING MOD EQUIP WEIGHT TO INFORMATION RATE   |
| KPM    | .0  |      | CONSTANT RELATING MOD EQUIP PWR REQ TO EQUIP WEIGHT      |
| CKM    | .0  |      | MOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE       |
| WKM    | .0  |      | MOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE         |

|        |     |   |  |
|--------|-----|---|--|
| NMODEF |     | MODULATION EQUIP BURDENS, 0.51, CW LASER, EARTH |  |
| KFM    | 7.5 | E-05  | CONSTANT RELATING MOD EQUIP FAB COST TO INFORMATION RATE |
| KM     | 5.  | E-08  | CONSTANT RELATING MOD EQUIP WEIGHT TO INFORMATION RATE   |
| KPM    | 5.  |   | CONSTANT RELATING MOD EQUIP PWR REQ TO EQUIP WEIGHT      |
| CKM    | 7.5 | E+03  | MOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE       |
| WKM    | 5.  |   | MOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE         |

|        |     |   |  |
|--------|-----|---|--|
| NMODEG |     | MODULATION EQUIP BURDENS, 0.84, CW LASER, EARTH |  |
| KFM    | 7.5 | E-05  | CONSTANT RELATING MOD EQUIP FAB COST TO INFORMATION RATE |
| KM     | 5.  | E-08  | CONSTANT RELATING MOD EQUIP WEIGHT TO INFORMATION RATE   |
| KPM    | 5.  |   | CONSTANT RELATING MOD EQUIP PWR REQ TO EQUIP WEIGHT      |
| CKM    | 7.5 | E+03  | MOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE       |
| WKM    | 5.  |   | MOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE         |

|        |     |   |  |
|--------|-----|---|--|
| NMODEH |     | MODULATION EQUIP BURDENS, 0.84, PULSED LASER, EARTH |  |
| KFM    | .5  | E-03  | CONSTANT RELATING MOD EQUIP FAB COST TO INFORMATION RATE |
| KM     | .3  | E-06  | CONSTANT RELATING MOD EQUIP WEIGHT TO INFORMATION RATE   |
| KPM    | 5.  |   | CONSTANT RELATING MOD EQUIP PWR REQ TO EQUIP WEIGHT      |
| CKM    | 15. | E+03  | MOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE       |
| WKM    | 10. |   | MOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE         |

|        |     |   |  |
|--------|-----|---|--|
| NMODEI |     | MODULATION EQUIP BURDENS, 10.6, CW LASER, EARTH |  |
| KFM    | .5  | E-03  | CONSTANT RELATING MOD EQUIP FAB COST TO INFORMATION RATE |
| KM     | .3  | E-06  | CONSTANT RELATING MOD EQUIP WEIGHT TO INFORMATION RATE   |
| KPM    | 5.  |   | CONSTANT RELATING MOD EQUIP PWR REQ TO EQUIP WEIGHT      |
| CKM    | 15. | E+03  | MOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE       |
| WKM    | 10. |   | MOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE         |

|        |    |                                       |  |
|--------|----|---------------------------------------|--|
| NMODEJ |    | MODULATION EQUIP BURDENS, 13CM, EARTH |  |
| KFM    | .0 |                                       | CONSTANT RELATING MOD EQUIP FAB COST TO INFORMATION RATE |
| KM     | .0 |                                       | CONSTANT RELATING MOD EQUIP WEIGHT TO INFORMATION RATE   |
| KPM    | .0 |                                       | CONSTANT RELATING MOD EQUIP PWR REQ TO EQUIP WEIGHT      |
| CKM    | .0 |                                       | MOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE       |
| WKM    | .0 |                                       | MOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE         |

|        |      |   |  |
|--------|------|---|--|
| NDMODA |      | DEMODULATION EQUIP BURDENS, OPTICAL DIR DET, EARTH        |  |
| KFD    | 5.5  | E-05  | CONSTANT RELATING DEMOD EQUIP FAB COST TO INFO RATE      |
| KD     | 1.1  | E-07  | CONSTANT RELATING DEMOD EQUIP WEIGHT TO INFORMATION RATE |
| KPD    | 3.33 |   | CONSTANT RELATING DEMOD EQUIP PWR REQ TO EQUIP WEIGHT    |
| CKD    | 15.  | E+03  | DEMOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE     |
| WKD    | 30.  |   | DEMOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE       |
| NDMOBB |      | DEMODULATION EQUIP BURDENS, OPTICAL HET DET, EARTH        |  |
| KFD    | .1   | E-03  | CONSTANT RELATING DEMOD EQUIP FAB COST TO INFO RATE      |
| KD     | .2   | E-06  | CONSTANT RELATING DEMOD EQUIP WEIGHT TO INFORMATION RATE |
| KPD    | 3.33 |   | CONSTANT RELATING DEMOD EQUIP PWR REQ TO EQUIP WEIGHT    |
| CKD    | 27.5 | E+03  | DEMOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE     |
| WKD    | 55.  |   | DEMOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE       |
| NDMOBC |      | DEMODULATION EQUIPMENT BURDENS, OPTICAL HOM DET, EARTH    |  |
| KFD    | .1   | E-03  | CONSTANT RELATING DEMOD EQUIP FAB COST TO INFO RATE      |
| KD     | .2   | E-06  | CONSTANT RELATING DEMOD EQUIP WEIGHT TO INFORMATION RATE |
| KPD    | 3.33 |   | CONSTANT RELATING DEMOD EQUIP PWR REQ TO EQUIP WEIGHT    |
| CKD    | 27.5 | E+03  | DEMOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE     |
| WKD    | 55.  |   | DEMOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE       |
| NDMOBE |      | DEMODULATION EQUIPMENT BURDENS, 13CM RADIO HOM DET, EARTH |  |
| KFD    | .0   |   | CONSTANT RELATING DEMOD EQUIP FAB COST TO INFO RATE      |
| KD     | .0   |   | CONSTANT RELATING DEMOD EQUIP WEIGHT TO INFORMATION RATE |
| KPD    | .0   |   | CONSTANT RELATING DEMOD EQUIP PWR REQ TO EQUIP WEIGHT    |
| CKD    | .0   |   | DEMOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE     |
| WKD    | .0   |   | DEMOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE       |
| NDMODF |      | DEMODULATION EQUIPMENT BURDENS, OPTICAL DIRECT DET, SPACE |  |
| KFD    | 5.5  | E-05  | CONSTANT RELATING DEMOD EQUIP FAB COST TO INFO RATE      |
| KD     | 1.1  | E-07  | CONSTANT RELATING DEMOD EQUIP WEIGHT TO INFORMATION RATE |
| KPD    | 3.33 |   | CONSTANT RELATING DEMOD EQUIP PWR REQ TO EQUIP WEIGHT    |
| CKD    | 15.  | E+03  | DEMOD EQUIP FAB COST INDEPENDENT OF INFORMATION RATE     |
| WKD    | 30.  |   | DEMOD EQUIP WEIGHT INDEPENDENT OF INFORMATION RATE       |

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|        |          |   |
|--------|----------|---|
| NXPWSA |          | XMTR POWER SUPPLY BURDENS,RTG,SPACECRAFT              |
| KST    | 3. E+03  | CONSTANT RELATING XMTR PWR SUPPLY FAB COST TO PWR REQ |
| KWST   | .7       | CONSTANT RELATING XMTR PWR SUPPLY WEIGHT TO PWR REQ   |
| CKE    | 0.       | XMTR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ       |
| WKE    | 0.       | XMTR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ         |
| /      |          |   |
| NXPWSB |          | XMTR POWER SUPPLY BURDENS,REACTOR,SPACECRAFT          |
| KST    | 5. E+02  | CONSTANT RELATING XMTR PWR SUPPLY FAB COST TO PWR REQ |
| KWST   | .625     | CONSTANT RELATING XMTR PWR SUPPLY WEIGHT TO PWR REQ   |
| CKE    | 1.2 E+06 | XMTR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ       |
| WKE    | 400.     | XMTR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ         |
| /      |          |   |
| NXPWSC |          | XMTR POWER SUPPLY BURDENS,SOLAR CELL,SPACECRAFT,MARS  |
| KST    | 112.     | CONSTANT RELATING XMTR PWR SUPPLY FAB COST TO PWR REQ |
| KWST   | .11      | CONSTANT RELATING XMTR PWR SUPPLY WEIGHT TO PWR REQ   |
| CKE    | 0.       | XMTR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ       |
| WKE    | 0.       | XMTR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ         |
| /      |          |   |
| NXPWSD |          | XMTR POWER SUPPLY BURDENS,GENERATOR,EARTH             |
| KST    | 25.      | CONSTANT RELATING XMTR PWR SUPPLY FAB COST TO PWR REQ |
| KWST   | .0       | CONSTANT RELATING XMTR PWR SUPPLY WEIGHT TO PWR REQ   |
| CKE    | 10. E+03 | XMTR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ       |
| WKE    | .0       | XMTR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ         |
| /      |          |   |
| NXPWSE |          | XMTR POWER SUPPLY BURDENS,SOLAR CELL,SPACECRAFT,SAT   |
| KST    | 166.     | CONSTANT RELATING XMTR PWR SUPPLY FAB COST TO PWR REQ |
| KWST   | .157     | CONSTANT RELATING XMTR PWR SUPPLY WEIGHT TO PWR REQ   |
| CKE    | 0.       | XMTR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ       |
| WKE    | 0.       | XMTR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ         |
| /      |          |   |
| NXPWSF |          | XMTR POWER SUPPLY BURDENS,SOLAR CELL,SPACECRAFT,VENUS |
| KST    | 38.      | CONSTANT RELATING XMTR PWR SUPPLY FAB COST TO PWR REQ |
| KWST   | .04      | CONSTANT RELATING XMTR PWR SUPPLY WEIGHT TO PWR REQ   |
| CKE    | 0.       | XMTR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ       |
| WKE    | 0.       | XMTR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ         |

NXPWGG

XMTR POWER SUPPLY BURDENS, SOLAR CELL, SPACECRAFT, MERCURY

KST 43.  
KWST .04  
CKE 0.  
WKE 0.

CONSTANT RELATING XMTR PWR SUPPLY FAB COST TO PWR REQ  
CONSTANT RELATING XMTR PWR SUPPLY WEIGHT TO PWR REQ  
XMTR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ  
XMTR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ

|        |      |      |  |
|--------|------|------|--|
| NRPWSA |      |      | RCVR POWER SUPPLY BURDENS, RTG, SPACECRAFT               |
| KSR    | 3.   | E+03 | CONSTANT RELATING RCVR PWR SUPPLY FAB COST TO PWR REQ    |
| KWSR   | .7   |      | CONSTANT RELATING RCVR PWR SUPPLY WEIGHT TO PWR REQ.     |
| CKF    | 0.   |      | RCVR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ          |
| WKF    | 0.   |      | RCVR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ            |
| NRPWSB |      |      | RCVR POWER SUPPLY BURDENS, REACTOR, SPACECRAFT           |
| KSR    | 5.   | E+02 | CONSTANT RELATING RCVR PWR SUPPLY FAB COST TO PWR REQ    |
| KWSR   | .625 |      | CONSTANT RELATING RCVR PWR SUPPLY WEIGHT TO PWR REQ.     |
| CKF    | 1.2  | E+06 | RCVR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ          |
| WKF    | 400. |      | RCVR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ            |
| NRPWSC |      |      | RCVR POWER SUPPLY BURDENS, SOLAR CELL, SPACECRAFT, MARS  |
| KSR    | 112. |      | CONSTANT RELATING RCVR PWR SUPPLY FAB COST TO PWR REQ    |
| KWSR   | .11  |      | CONSTANT RELATING RCVR PWR SUPPLY WEIGHT TO PWR REQ.     |
| CKF    | 0.   |      | RCVR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ          |
| WKF    | 0.   |      | RCVR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ            |
| NRPWSD |      |      | RCVR POWER SUPPLY BURDENS, GENERATOR, EARTH              |
| KSR    | 25.  |      | CONSTANT RELATING RCVR PWR SUPPLY FAB COST TO PWR REQ    |
| KWSR   |      |      | CONSTANT RELATING RCVR PWR SUPPLY WEIGHT TO PWR REQ.     |
| CKF    | 10.  | E+03 | RCVR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ          |
| WKF    |      |      | RCVR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ            |
| NRPWSE |      |      | RCVR POWER SUPPLY BURDENS, SOLAR CELL, SPACECRAFT, SAT   |
| KSR    | 166. |      | CONSTANT RELATING RCVR PWR SUPPLY FAB COST TO PWR REQ    |
| KWSR   | .157 |      | CONSTANT RELATING RCVR PWR SUPPLY WEIGHT TO PWR REQ.     |
| CKF    | 0.   |      | RCVR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ          |
| WKF    | 0.   |      | RCVR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ            |
| NRPWSF |      |      | RCVR POWER SUPPLY BURDENS, SOLAR CELL, SPACECRAFT, VENUS |
| KSR    | 38.  |      | CONSTANT RELATING RCVR PWR SUPPLY FAB COST TO PWR REQ    |
| KWSR   | .04  |      | CONSTANT RELATING RCVR PWR SUPPLY WEIGHT TO PWR REQ.     |
| CKF    | 0.   |      | RCVR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ          |
| WKF    | 0.   |      | RCVR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ            |

NRPWSG

RCVR POWER SUPPLY BURDENS, SOLAR CELL, SPACECRAFT, MERCURY

KSR 43.  
KWSR .04  
CKF 0.  
WKF 0.

CONSTANT RELATING RCVR PWR SUPPLY FAB COST TO PWR REQ  
CONSTANT RELATING RCVR PWR SUPPLY WEIGHT TO PWR REQ.  
RCVR PWR SUPPLY FAB COST INDEPENDENT OF PWR REQ  
RCVR PWR SUPPLY WEIGHT INDEPENDENT OF PWR REQ

| NXMTRA |      | XMTR BURDENS,0.51 ,SPACECRAFT                           |
|--------|------|---|
| KPT    | 150. | CONSTANT RELATING XMTR FAB COST TO XMTR PWR             |
| KWT    | 51.  | CONSTANT RELATING XMTR WEIGHT TO XMTR PWR               |
| KH     | .58  | CONSTANT RELATING XMTR HEAT EX FAB COST TO XMTR PWR DIS |
| KX     | .7   | CONSTANT RELATING XMTR HEAT EX WEIGHT TO XMTR PWR DIS   |
| KE     | .001 | XMTR PWR EFFICIENCY                                     |
| CKP    | 3.5  | XMTR FAB COST INDEPENDENT OF XMTR PWR                   |
| CKH    | 13.8 | XMTR HEAT EX FAB COST INDEPENDENT OF XMTR PWR           |
| WKP    | 40.  | XMTR WEIGHT INDEPENDENT OF XMTR PWR                     |
| WKH    | 0.   | XMTR HEAT EX WEIGHT INDEPENDENT OF XMTR PWR             |
| GT     | 1.   | EXPONENT RELATING XMTR FAB COST TO XMTR PWR             |
| HT     | 1.   | EXPONENT RELATING XMTR WEIGHT TO XMTR PWR               |
| JT     | 1.   | EXPONENT RELATING XMTR PWR SUP-HEAT EX BURD TO XMTR PWR |

| NXMTRB |      | XMTR BURDENS,0.51 ,EARTH                                |
|--------|------|---|
| KPT    | 150. | CONSTANT RELATING XMTR FAB COST TO XMTR PWR             |
| KWT    | 51.  | CONSTANT RELATING XMTR WEIGHT TO XMTR PWR               |
| KH     | 0.   | CONSTANT RELATING XMTR HEAT EX FAB COST TO XMTR PWR DIS |
| KX     | 0.   | CONSTANT RELATING XMTR HEAT EX WEIGHT TO XMTR PWR DIS   |
| KE     | .001 | XMTR PWR EFFICIENCY                                     |
| CKP    | 3.5  | XMTR FAB COST INDEPENDENT OF XMTR PWR                   |
| CKH    | 0.   | XMTR HEAT EX FAB COST INDEPENDENT OF XMTR PWR           |
| WKP    | 40.  | XMTR WEIGHT INDEPENDENT OF XMTR PWR                     |
| WKH    | 0.   | XMTR HEAT EX WEIGHT INDEPENDENT OF XMTR PWR             |
| GT     | 1.   | EXPONENT RELATING XMTR FAB COST TO XMTR PWR             |
| HT     | 1.   | EXPONENT RELATING XMTR WEIGHT TO XMTR PWR               |
| JT     | 1.   | EXPONENT RELATING XMTR PWR SUP-HEAT EX BURD TO XMTR PWR |

| NXMTBE |      | XMTR BURDENS,10.6 ,SPACECRAFT                           |
|--------|------|---|
| KPT    | 1.43 | CONSTANT RELATING XMTR FAB COST TO XMTR PWR             |
| KWT    | 2.   | CONSTANT RELATING XMTR WEIGHT TO XMTR PWR               |
| KH     | 1.97 | CONSTANT RELATING XMTR HEAT EX FAB COST TO XMTR PWR DIS |
| KX     | 2.5  | CONSTANT RELATING XMTR HEAT EX WEIGHT TO XMTR PWR DIS   |
| KE     | .1   | XMTR PWR EFFICIENCY                                     |
| CKP    | 2.   | XMTR FAB COST INDEPENDENT OF XMTR PWR                   |
| CKH    | 13.8 | XMTR HEAT EX FAB COST INDEPENDENT OF XMTR PWR           |
| WKP    | 25.  | XMTR WEIGHT INDEPENDENT OF XMTR PWR                     |
| WKH    | 0.   | XMTR HEAT EX WEIGHT INDEPENDENT OF XMTR PWR             |
| GT     | 1.   | EXPONENT RELATING XMTR FAB COST TO XMTR PWR             |
| HT     | 1.   | EXPONENT RELATING XMTR WEIGHT TO XMTR PWR               |
| JT     | 1.   | EXPONENT RELATING XMTR PWR SUP-HEAT EX BURD TO XMTR PWR |

|        |      |   |
|--------|------|---|
| NXMTRF |      | XMTR BURDENS, 10.6 , EARTH                              |
| KPT    | 1.43 | CONSTANT RELATING XMTR FAB COST TO XMTR PWR             |
| KWT    | 2.   | CONSTANT RELATING XMTR WEIGHT TO XMTR PWR               |
| KH     | 0.   | CONSTANT RELATING XMTR HEAT EX FAB COST TO XMTR PWR DIS |
| KX     | 0.   | CONSTANT RELATING XMTR HEAT EX WEIGHT TO XMTR PWR DIS   |
| KE     | .1   | XMTR PWR EFFICIENCY                                     |
| CKP    | 2.   | E+03 XMTR FAB COST INDEPENDENT OF XMTR PWR              |
| CKH    | 0.   | XMTR HEAT EX FAB COST INDEPENDENT OF XMTR PWR           |
| WKP    | 25.  | XMTR WEIGHT INDEPENDENT OF XMTR PWR                     |
| WKH    | 0.   | XMTR HEAT EX WEIGHT INDEPENDENT OF XMTR PWR             |
| GT     | 1.   | EXPONENT RELATING XMTR FAB COST TO XMTR PWR             |
| HT     | 1.   | EXPONENT RELATING XMTR WEIGHT TO XMTR PWR               |
| JT     | 1.   | EXPONENT RELATING XMTR PWR SUP-HEAT EX BURD TO XMTR PWR |

|        |      |  |
|--------|------|--|
| NXMTRG |      | XMTR BURDENS, 13CM, SPACECRAFT                             |
| KPT    | 120. | CONSTANT RELATING XMTR FAB COST TO XMTR PWR                |
| KWT    | .1   | CONSTANT RELATING XMTR WEIGHT TO XMTR PWR                  |
| KH     | .58  | CONSTANT RELATING XMTR HEAT EX FAB COST TO XMTR PWR DIS    |
| KX     | .7   | E-02 CONSTANT RELATING XMTR HEAT EX WEIGHT TO XMTR PWR DIS |
| KE     | .25  | XMTR PWR EFFICIENCY  |
| CKP    | 17.5 | E+03 XMTR FAB COST INDEPENDENT OF XMTR PWR                 |
| CKH    | 13.8 | E+03 XMTR HEAT EX FAB COST INDEPENDENT OF XMTR PWR         |
| WKP    | 5.   | XMTR WEIGHT INDEPENDENT OF XMTR PWR                        |
| WKH    | 0.   | XMTR HEAT EX WEIGHT INDEPENDENT OF XMTR PWR                |
| GT     | 1.   | EXPONENT RELATING XMTR FAB COST TO XMTR PWR                |
| HT     | 1.   | EXPONENT RELATING XMTR WEIGHT TO XMTR PWR                  |
| JT     | 1.   | EXPONENT RELATING XMTR PWR SUP-HEAT EX BURD TO XMTR PWR    |

|        |      |   |
|--------|------|---|
| NXMTRH |      | XMTR BURDENS, 13CM, EARTH                               |
| KPT    | 120. | CONSTANT RELATING XMTR FAB COST TO XMTR PWR             |
| KWT    | .1   | CONSTANT RELATING XMTR WEIGHT TO XMTR PWR               |
| KH     | 0.   | CONSTANT RELATING XMTR HEAT EX FAB COST TO XMTR PWR DIS |
| KX     | 0.   | CONSTANT RELATING XMTR HEAT EX WEIGHT TO XMTR PWR DIS   |
| KE     | .25  | XMTR PWR EFFICIENCY                                     |
| CKP    | 17.5 | E+03 XMTR FAB COST INDEPENDENT OF XMTR PWR              |
| CKH    | 0.   | XMTR HEAT EX FAB COST INDEPENDENT OF XMTR PWR           |
| WKP    | 5.   | XMTR WEIGHT INDEPENDENT OF XMTR PWR                     |
| WKH    | 0.   | XMTR HEAT EX WEIGHT INDEPENDENT OF XMTR PWR             |
| GT     | 1.   | EXPONENT RELATING XMTR FAB COST TO XMTR PWR             |
| HT     | 1.   | EXPONENT RELATING XMTR WEIGHT TO XMTR PWR               |
| JT     | 1.   | EXPONENT RELATING XMTR PWR SUP-HEAT EX BURD TO XMTR PWR |

#### 4.6 Automatic COPTRAN Burden Data Selection Logic

Automatic burden data selection by the COPTRAN program is made according to the selection tables in the following sections. This selection will always be made unless other specific instructions or data are included. In such a case, the specific instructions or data over-ride the automatic selection logic.

##### 4.6.1 Nominal Systems Burdens Selection Logic

###### TRANSMITTER ANTENNA

|                           | 0.51 $\mu$ | 0.84 $\mu$ | 10.6 $\mu$ | 13 cm<br>Diameter<br>Burdens | 13 cm<br>Gain<br>Burdens |
|---------------------------|------------|------------|------------|------------------------------|--------------------------|
| Spacecraft<br>Transmitter | NXANTA     | NXANTC     | NXANTD     | NXANTF                       | NXANTG                   |

###### RECEIVER ANTENNA

|                   |                           | 0.51 $\mu$ | 0.84 $\mu$ | 10.6 $\mu$ | 13 cm<br>Diameter<br>Burdens | 13 cm<br>Gain<br>Burdens |
|-------------------|---------------------------|------------|------------|------------|------------------------------|--------------------------|
| Earth<br>Receiver | Direct<br>Detection       | NRANTA     | NRANTC     | NRANTD     | NRANTF                       | NRANTG                   |
|                   | Het. or Hom.<br>Detection | NRANTB     | X          | NRANTE     |                              |                          |

X - Forbidden combination

TRANSMITTER ACQUISITION  
AND TRACK SYSTEM

|                           | Optical<br>Frequency | Radio Freq.<br>Diam. Burdens | Radio Freq.<br>Gain Burdens |
|---------------------------|----------------------|------------------------------|-----------------------------|
| Spacecraft<br>Transmitter | NXACTA               | NXACTB                       | NXACTC                      |

RECEIVER ACQUISITION  
AND TRACK SYSTEM

|                   | Optical<br>Frequency | Radio Freq.<br>Diam. Burdens | Radio Freq.<br>Gain Burdens |
|-------------------|----------------------|------------------------------|-----------------------------|
| Earth<br>Receiver | NRACTA               | NRACTB                       | NRACTC                      |

MODULATION  
EQUIPMENT - SPACE

|        | 0.51 $\mu$ | 0.84 $\mu$ | 10.6 $\mu$ | 13 cm  |
|--------|------------|------------|------------|--------|
| PCM/AM | NMODEA     | NMODEB     | NMODED     | NMODEE |
| PCM/PL | NMODEA     | NMODEB     | NMODED     | X      |
| PCM/FM | NMODEA     | NMODEB     | NMODED     | NMODEE |
| PCM/PM | NMODEA     | NMODEB     | NMODED     | NOMDEE |
| PPM/AM | NMODEA     | NMODEC     | NMODED     | X      |

X - Forbidden combination

MODULATION  
EQUIPMENT - EARTH

|        | 0.51 $\mu$ | 0.84 $\mu$ | 10.6 $\mu$ | 13 cm  |
|--------|------------|------------|------------|--------|
| PCM/AM | NMODEF     | NMODEG     | NMODEI     | NMODEJ |
| PCM/PL | NMODEF     | NMODEG     | NMODEI     | X      |
| PCM/FM | NMODEF     | NMODEG     | NMODEI     | NMODEJ |
| PCM/PM | NMODEF     | NMODEG     | NMODEI     | NMODEJ |
| PPM/AM | NMODEF     | NMODEH     | NMODEI     | X      |

X - Forbidden combination

DEMODULATION  
EQUIPMENT - EARTH

|        | Optical Direct Detection |            |            | Optical Heterodyne Detection |            |            | Optical Homodyne Detection |            |            | Radio Direct Detection<br>13 cm | Radio Homodyne Detection<br>13 cm |
|--------|--------------------------|------------|------------|------------------------------|------------|------------|----------------------------|------------|------------|---------------------------------|-----------------------------------|
|        | 0.51 $\mu$               | 0.84 $\mu$ | 10.6 $\mu$ | 0.51 $\mu$                   | 0.84 $\mu$ | 10.6 $\mu$ | 0.51 $\mu$                 | 0.84 $\mu$ | 10.6 $\mu$ |                                 |                                   |
| PCM/AM | NDMODA                   | NDMODA     | NDMODA     | X                            | X          | X          | X                          | X          | X          | X                               | NDMODE                            |
| PCM/PL | NDMODA                   | NDMODA     | NDMODA     | X                            | X          | X          | X                          | X          | X          | X                               | X                                 |
| PCM/FM | X                        | X          | X          | NDMODB                       | NDMODB     | NDMODB     | X                          | X          | X          | X                               | NDMODE                            |
| PCM/PM | X                        | X          | X          | X                            | X          | X          | NDMODC                     | NDMODC     | NDMODC     | X                               | NDMODE                            |
| PPM/AM | NDMODA                   | NDMODA     | NDMODA     | X                            | X          | X          | X                          | X          | X          | X                               | X                                 |

X - Forbidden combination

DEMODULATION  
EQUIPMENT - SPACE

|        | Optical Direct Detection |            |            | Optical Heterodyne Detection |            |            | Optical Homodyne Detection |            |            | Radio Direct Detection<br>13 cm | Radio Homodyne Detection<br>13 cm |
|--------|--------------------------|------------|------------|------------------------------|------------|------------|----------------------------|------------|------------|---------------------------------|-----------------------------------|
|        | 0.51 $\mu$               | 0.84 $\mu$ | 10.6 $\mu$ | 0.51 $\mu$                   | 0.84 $\mu$ | 10.6 $\mu$ | 0.51 $\mu$                 | 0.84 $\mu$ | 10.6 $\mu$ |                                 |                                   |
| PCM/AM | NDMODF                   | NDMODF     | NDMODF     | X                            | X          | X          | X                          | X          | X          | NDMODI                          | NDMODJ                            |
| PCM/PL | NDMODF                   | NDMODF     | NDMODF     | X                            | X          | X          | X                          | X          | X          | X                               | X                                 |
| PCM/FM | X                        | X          | X          | NDMODG                       | NDMODG     | NDMODG     | X                          | X          | X          | NDMODI                          | NDMODJ                            |
| PCM/PM | X                        | X          | X          | X                            | X          | X          | NDMODH                     | NDMODH     | NDMODH     | NDMODI                          | NDMODJ                            |
| PPM/AM | NDMODF                   | NDMODF     | NDMODF     | X                            | X          | X          | X                          | X          | X          | X                               | X                                 |

X - Forbidden combination

# TRANSMITTER SYSTEM POWER SUPPLY

| Spacecraft Transmitter |         |                 |                      |                  |                    | Earth Transmitter |
|------------------------|---------|-----------------|----------------------|------------------|--------------------|-------------------|
| RTG                    | Reactor | Solar Cell Mars | Solar Cell Satellite | Solar Cell Venus | Solar Cell Mercury | Generator         |
| NXPWSA                 | NXPWSB  | NXPWSC          | NXPWSE               | NXPWSF           | NXPWSG             | NXPWSD            |

# RECEIVER SYSTEM POWER SUPPLY

| Spacecraft Receiver |         |                 |                      |                  |                    | Earth Transmitter |
|---------------------|---------|-----------------|----------------------|------------------|--------------------|-------------------|
| RTG                 | Reactor | Solar Cell Mars | Solar Cell Satellite | Solar Cell Venus | Solar Cell Mercury | Generator         |
| NRPWSA              | NRPWSB  | NRPWSC          | NRPWSE               | NRPWSF           | NRPWSG             | NRPWSD            |

# TRANSMITTER

|                        | 0.51 $\mu$ | 0.84 $\mu$ | 10.6 $\mu$ | 13 cm  |
|------------------------|------------|------------|------------|--------|
| Spacecraft Transmitter | NXMTRA     | X          | NXMTRE     | NXMTRG |
| Earth Transmitter      | NXMTRB     | X          | NXMTRF     | NXMTRH |

## 4.6.2 System Physical Data Selection Logic

R, transmission range

|        |                         |
|--------|-------------------------|
| RANMAR | $1.0 \times 10^{13}$ cm |
| RANJUP | $7.5 \times 10^{13}$ cm |
| RANSAT | $3.6 \times 10^9$ cm    |

$\lambda$ , transmission wavelength

|        |                          |
|--------|--------------------------|
| LAM051 | $0.51 \times 10^{-4}$ cm |
| LAM084 | $0.84 \times 10^{-4}$ cm |
| LAM106 | $10.6 \times 10^{-4}$ cm |
| LAM13C | 13 cm                    |

S/N, signal-to-noise power ratio

|        | OPTDIR | OPTHET | OPTHOM | RADHET | RADHOM |
|--------|--------|--------|--------|--------|--------|
| PCM/AM | 26     | 30     | 15     | 20     | 15     |
| PCM/PL | 12     | X      | X      | X      | X      |
| PCM/FM | X      | 15     | X      | 19     | 15     |
| PCM/PM | X      | X      | 7      | X      | 8      |
| PCM/AM | 19     | X      | X      | 25     | X      |

X - Forbidden Combination

C/N, carrier-to-background radiation power ratio

|        | <u>OPTDIR</u> |
|--------|---------------|
| PCM/IM | 6             |
| PCM/PL | 3             |
| PPM/IM | 1             |

$(u_s, \tau)_{REQ}$ , required signal photoelectron count per time period  $\tau$

|        | <u>OPTDIR</u> |
|--------|---------------|
| PCM/IM | 30            |
| PCM/PL | 15            |
| PPM/IM | 20            |

$\tau_t$ , transmitter system transmissivity

|        | LAM051 | LAM084 | LAM106 | LAM13C |
|--------|--------|--------|--------|--------|
| PCM/AM | .8     | .8     | .8     | .75    |
| PCM/IM | .8     | .8     | .8     | .75    |
| PCM/PL | .8     | .8     | .8     | .75    |
| PCM/FM | .8     | .8     | .8     | .75    |
| PCM/PM | .8     | .8     | .8     | .75    |
| PPM/IM | .8     | .8     | .8     | .75    |

$\tau_r$ , receiver system transmissivity

|                     | LAM051 | LAM084 | LAM106 | LAM13C |
|---------------------|--------|--------|--------|--------|
| OPTDIR              | .7     | .7     | .7     | X      |
| OPTHET or<br>OPTHOM | .6     | .6     | .6     | X      |
| RADHET or<br>RADDIR | X      | X      | X      | .35    |

X — Forbidden Combination

$\tau_a$ , atmospheric transmissivity

|   | LAM051 | LAM084 | LAM106 | LAM13C |
|---|--------|--------|--------|--------|
| SPXMTR and SPRCVR                         | .8     | .8     | .8     | .95    |
| SPXMTR and EARCVR or<br>EAXMTR and SPRCVR | .8     | .8     | .8     | .95    |
| EAXMTR and EARCVR                         | .8     | .8     | .8     | .95    |

$\rho_T$ , transmitter antenna aperture efficiency

|        |      |
|--------|------|
| LAM051 | 0.98 |
| LAM084 | 0.98 |
| LAM106 | 0.98 |
| LAM13C | 0.60 |

$\rho_R$ , receiver antenna aperture efficiency

|        |      |
|--------|------|
| LAM051 | 0.98 |
| LAM084 | 0.98 |
| LAM106 | 0.98 |
| LAM13C | 0.80 |

$T_E$ , receiver equivalent temperature

|        | LAM13C | LAM084 or LAM106 |
|--------|--------|------------------|
| BKGALT | 27     | X                |
| OPTDIR | X      | 300              |

$\eta$ , detector quantum efficiency

|        |    |
|--------|----|
| LAM051 | .2 |
| LAM084 | .5 |
| LAM106 | .5 |

X - Forbidden Combination

$R_L$ , receiver output load resistance

$$R_L = 100 \text{ ohms}$$

$\lambda_i$ , optical filter bandwidth

$$\lambda_i = 10^{-3} \text{ microns}$$

$Q_B$ , background radiation photon spectral radiance

|        | <u>LAM051</u>        |
|--------|----------------------|
| BKMARS | X                    |
| BKJUPT | X                    |
| BKMOON | X                    |
| BKERTH | X                    |
| BKDSKY | $.2 \times 10^{-17}$ |
| BKNSKY | $.75 \times 10^9$    |
| BKGALT | 0.                   |

$d_{TB}$ , transmitter antenna diameter stop

|        | LAM051 | LAM084 | LAM106 | LAM13C |
|--------|--------|--------|--------|--------|
| SPXMTR | 10     | 16     | 100    | 100    |
| EAXMTR | 10     | 16     | 210    | 1000   |

$G_{TB}$ , transmitter antenna gain stop

|        | <u>LAM13C</u> |
|--------|---------------|
| SPXMTR | 348           |
| EAXMTR | 34,800        |

X - Forbidden Combination

$d_{RB}$ , receiver antenna diameter stop

|                                    | LAM051 | LAM084 | LAM106 | LAM13C |
|------------------------------------|--------|--------|--------|--------|
| SPRCVR and OPTDIR                  | 100    | 100    | 100    | X      |
| SPRCVR and either OPTHET or OPTHOM | 10     | 16     | 100    | X      |
| SPRCVR and either RADDIR or RADHOM | X      | X      | X      | 1000   |
| EARCVR and OPTDIR                  | 1000   | 1000   | 1000   | 1000   |
| EARCVR and either OPTHET or OPTHOM | 10     | 16     | 100    | X      |
| EARCVR and either RADDIR or RADHOM | X      | X      | X      | 6400   |

$G_{RB}$ , receiver antenna gain stop

|        | <u>LAM13C</u> |
|--------|---------------|
| SPRCVR | 46,500        |
| EARCVR | 1,900,000     |

$P_{TB}$ , transmitter power stop

|        | LAM051 | LAM084 | LAM106 | LAM13C |
|--------|--------|--------|--------|--------|
| SPXMTR | 50     | 5      | 500    | 1,000  |
| EAXMTR | 100    | 25     | 1000   | 10,000 |

$\theta_{RB}$ , receiver field of view stop

|        | LAM051    | LAM084    | LAM106    | LAM13C    |
|--------|-----------|-----------|-----------|-----------|
| SPRCVR | $10^{-5}$ | $10^{-5}$ | $10^{-5}$ | $10^{-4}$ |
| EARCVR | $10^{-5}$ | $10^{-5}$ | $10^{-5}$ | $10^{-4}$ |

X — Forbidden Combination

#### 4.7 COPTRAN Coding Sheets and Data Forms

The following pages contain the blank sheets and forms which may be used in the preparation of COPTRAN programs. The sheets are: the COPTRAN Coding Sheet A, the COPTRAN Coding Sheet B, the COPTRAN Coding Sheet C, the System Burdens Data Sheet, the System Physical Data Sheet, and the System Parameter Constraints Sheet.

The COPTRAN Coding Sheet A is generally the only coding sheet needed. Its usage is described in Section 4.3.1 and 4.3.2, where it is noted that the COPTRAN Instruction mnemonics and the COPTRAN Data may be tabulated on this form. COPTRAN Coding Sheets B and C, described in Section 4.3.2, are used if many of the Systems Burdens Data values and the System Physical Data values are to be changed. COPTRAN Coding Sheets B and C list all the labels and indicate where the decimal point is to be placed, saving some effort in preparation.

The Systems Burdens Data Sheet, the Systems Physical Data Sheet, and the Systems Parameter Constraints Sheets are provided to enable the user to consider more conveniently changes he may wish to make. Their use is not required in any part of the COPTRAN program.

**COPTRAN CODING SHEET A**

## COPTRAN INSTRUCTIONS AND DATA

The image displays two identical, blank graph paper sheets stacked vertically. Each sheet is a grid of 25 rows and 24 columns. The columns are numbered 1 through 24 at the top of each sheet. The rows are numbered 1 through 25 on the left side of each sheet. The grid lines are thin and black, creating a uniform pattern of squares across the entire area of each sheet. There is no text or other markings on the grid.

NAME \_\_\_\_\_ DATE \_\_\_\_\_ PROBLEM: \_\_\_\_\_

## SYSTEM BURDENS DATA

[illegible]

## SYSTEM BURDENS DATA

[illegible]

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

# SYSTEM BURDENS DATA

TRANSMITTER LOCATION: \_\_\_\_\_

DATE: \_\_\_\_\_

RECEIVER LOCATION: \_\_\_\_\_

TRANSMISSION WAVELENGTH: \_\_\_\_\_

| COMPONENT                                | PARAMETER      | UNIT    | VALUE | USE | COMPONENT                | PARAMETER  | UNIT    | VALUE | USE |
|--|----------------|---------|-------|-----|--------------------------|------------|---------|-------|-----|
| TRANSMITTER ANTENNA                      | $K_{\theta T}$ | \$/     |       | TF  | MODULATION EQUIPMENT     | $K_{FM}$   | \$/BIT  |       | TF  |
|  | $K_{d T}$      | LB/     |       | TW  |                          | $K_M$      | LB/BIT  |       | TW  |
|  | $C_{KT}$       | \$      |       | TF  |                          | $K_{PM}$   | WATT/LB |       | TWF |
|  | $W_{KT}$       | LB      |       | TW  |                          | $C_{KM}$   | \$      |       | TF  |
|  | $\eta_T$       | --      |       | TF  |                          | $W_{KM}$   | LB      |       | TW  |
|  | $\eta_T$       | --      |       | TW  | DEMODULATION EQUIPMENT   | $K_{FD}$   | \$/BIT  |       | RF  |
| RECEIVER ANTENNA                         | $K_{\theta R}$ | \$/     |       | RF  |                          | $K_D$      | LB/BIT  |       | RW  |
|  | $K_{d R}$      | LB/     |       | RW  |                          | $K_{PD}$   | WATT/LB |       | RWF |
|  | $C_{KR}$       | \$      |       | RF  |                          | $C_{KD}$   | \$      |       | RF  |
|  | $W_{KR}$       | LB      |       | RW  |                          | $W_{KD}$   | LB      |       | RW  |
|  | $\eta_R$       | --      |       | RF  | TRANSMITTER POWER SUPPLY | $K_{ST}$   | \$/WATT |       | TF  |
|  | $\eta_R$       | --      |       | RW  |                          | $K_{WST}$  | LB/WATT |       | TW  |
| TRANSMITTER ACQUISITION AND TRACK SYSTEM | $K_{AT}$       | \$/     |       | TF  |                          | $C_{KE}$   | \$      |       | TF  |
|  | $K_{WAT}$      | LB/     |       | TW  |                          | $W_{KE}$   |         |       | TW  |
|  | $K_{PQT}$      | WATT/LB |       | TWF | RECEIVER POWER SUPPLY    | $K_{SR}$   | \$/WATT |       | RF  |
|  | $C_{AT}$       | \$      |       | TF  |                          | $K_{WSR}$  | LB/WATT |       | RW  |
|  | $W_{BT}$       | LB      |       | TW  |                          | $C_{KF}$   | \$      |       | RF  |
|  | $\eta_T$       | --      |       | TF  |                          | $W_{KE}$   | LB      |       | RW  |
| RECEIVER ACQUISITION AND TRACK SYSTEM    | $K_{AR}$       | \$/     |       | RF  | TRANSMITTER              | $K_{PT}$   | \$/     |       | TF  |
|  | $K_{WAR}$      | LB/     |       | RW  |                          | $K_{WT}$   | LB/     |       | TW  |
|  | $K_{PQR}$      | WATT/LB |       | RWF |                          | $K_H$      | \$/WATT |       | TF  |
|  | $C_{AR}$       | \$      |       | RF  |                          | $K_X$      | LB/WATT |       | TW  |
|  | $W_{BR}$       | LB      |       | RW  |                          | $k_c$      | --      |       | TWF |
|  | $\eta_R$       | --      |       | RF  |                          | $C_{KP}$   | \$      |       | TF  |
| GENERAL                                  | $K_{SA}$       | \$/LB   |       | TW  |                          | $C_{KH}$   | \$      |       | TF  |
|  | $K_{SB}$       | \$/LB   |       | RW  |                          | $W_{KP}$   | LB      |       | TW  |
|  |                |         |       |     |                          | $W_{KH}$   | LB      |       | TW  |
|  |                |         |       |     |                          | $\theta_T$ | --      |       | TF  |
|  |                |         |       |     |                          | $h_T$      | --      |       | TW  |
|  |                |         |       |     |                          | $i_T$      | --      |       | TWF |

Use Code: TW -- Data for transmitter weight optimization  
 TF -- Data for transmitter fabrication cost optimization  
 RW -- Data for receiver weight optimization  
 RF -- Data for receiver fabrication cost optimization  
 TWF -- Data for transmitter weight and fabrication cost optimization  
 RWF -- Data for receiver weight and fabrication cost optimization

# SYSTEM PHYSICAL DATA

TRANSMITTER LOCATION: \_\_\_\_\_ DATE: \_\_\_\_\_  
 RECEIVER LOCATION: \_\_\_\_\_

| PROGRAM   |     |     |     | PARAMETER                      | NAME  | UNITS  | VALUE |
|---|-----|-----|-----|--------------------------------|---|--|-------|
| SOP   | TOP | HOP | ROP |                                |   |  |       |
| *   | *   | *   | *   | R                              | Range   | cm   |       |
| *   | *   | *   | *   | $\lambda$                      | Transmission wavelength                                   | cm   |       |
|   | *   | *   | *   | S/N                            | Signal-to-noise power ratio                               |  |       |
| *   |     |     |     | C/N                            | Signal to background radiation power ratio                |  |       |
| *   |     |     |     | $(\mu_{S, \pi})_{\text{Req.}}$ | Required signal photoelectron count per decision interval |  |       |
| *   | *   | *   | *   | $\tau_t$                       | Transmitter transmissivity                                |  |       |
| *   | *   | *   | *   | $\tau_r$                       | Receiver transmissivity                                   |  |       |
| *   | *   | *   | *   | $\tau_a$                       | Atmospheric transmissivity                                |  |       |
| *   | *   | *   | *   | $\rho_t$                       | Transmitter antenna aperture efficiency                   |  |       |
| *   | *   | *   | *   | $\rho_r$                       | Receiver antenna aperture efficiency                      |  |       |
|   | *   |     | *   | $T_E$                          | Receiver temperature                                      | °K   |       |
| *   | *   | *   |     | $\eta$                         | Detector quantum efficiency                               |  |       |
|   | *   |     |     | $R_L$                          | Receiver output load resistance                           | ohms   |       |
| *   |     |     |     | $\lambda_c$                    | Optical filter bandwidth                                  | micron                                       |       |
| *   |     |     |     | $Q_B$                          | Photon spectral radiance                                  | photons per cm <sup>2</sup> micron steradian |       |
| Rule: Parameter may be set equal to zero if asterisk is absent in program column. |     |     |     |                                |   |  |       |

# SYSTEM PARAMETER CONSTRAINTS

| PARAMETER  | UNITS | INITIAL         | FIXED           | STOP            |
|--|-------|-----------------|-----------------|-----------------|
| Transmitter antenna diameter   | cm    | d <sub>TI</sub> | d <sub>TM</sub> | d <sub>TB</sub> |
|  |       |                 |                 |                 |
| Transmitter antenna gain   | —     | G <sub>TI</sub> | G <sub>TM</sub> | G <sub>TB</sub> |
|  |       |                 |                 |                 |
| Receiver antenna diameter  | cm    | d <sub>RI</sub> | d <sub>RM</sub> | d <sub>RB</sub> |
|  |       |                 |                 |                 |
| Receiver antenna gain  | —     | G <sub>RI</sub> | G <sub>RM</sub> | G <sub>RB</sub> |
|  |       |                 |                 |                 |
| Transmitter power  | watt  | P <sub>TI</sub> | P <sub>TM</sub> | P <sub>TB</sub> |
|  |       |                 |                 |                 |
| Receiver field of view   | rad.  | $\theta_{RI}$   | $\theta_{RM}$   | $\theta_{RB}$   |
|  |       |                 |                 |                 |
| Rules:   |       |                 |                 |                 |
| 1. If a parameter is to be fixed, set the stop and initial values of the parameter to its fixed value                          |       |                 |                 |                 |
| 2. If a parameter is not to be fixed, set the fixed value equal to zero, and set the initial value to one half the stop value. |       |                 |                 |                 |
| 3. If a parameter is not to be optimized, nor fixed, its values may be set to zero.  |       |                 |                 |                 |

## 5.0 INTERFACE EQUIPMENT SUMMARY

### 5.1 Introduction

The COPS digital computer program can be controlled using COPTRAN, an interpretive computer language. These programs at present operate in a pure batch processing mode. Program controls and data are input by means of a prepared card deck. The program operates on the input and produces a tabular and graphical output.

To fully utilize the computer as a design tool, an interactive console terminal should be provided. Then, with the appropriate conversational software, the designer will be able to communicate directly with the COPS program through his console. Results could be made available immediately and changes in input parameters could be made quickly to determine their effects. Additionally, the conversational software can be designed so that the user need have very little familiarity with computers and card preparation. He would be able to converse with the computer in terms familiar to him or merely supply information to the computer as required in a question-and-answer session. The prime objectives in converting to a remote conversational mode of operation are: ease of use, flexibility, and rapid production of results.

There is a wide spectrum of capability which can be made available to the user. The features which can be provided at a remote terminal include:

- Input: Keyboard
  - Light pen graphics
  - Stylus graphics
- Output: Printer (High- or Low-Speed)
  - Plotter
  - CRT Alpha-Numerics
  - CRT Display graphics

These features may be combined in various ways to achieve many different degrees of sophistication. Configurations might run from something as simple as a teletype and plotter to a general purpose graphic display terminal with independent software, central processing unit, light pen, high speed printer, and graphic hard copy capability.

The following is a survey of currently available equipment which could form a remote terminal. The assumptions are that the first computer used will be a Honeywell DDP 516, with possible conversion at a later date to a larger computer in the SDS Sigma 5 class. Input/Output capability should conform as closely as possible to the requirements of COPS and COPTRAN. FORTRAN IV is available on the DDP-516 and it is understood that, because COPS and COPTRAN are written in FORTRAN IV, remote terminals should be evaluated also on their ability to be driven by and be compatible with FORTRAN IV.

The present ERC configuration of the DDP-516 installation includes CRT graphics as well as a large memory and secondary storage for implementation of a graphics-oriented time-sharing system. The selection of the graphics system for the DDP-516 facility has already been made (Information Displays, Inc.). Although this seems to dictate the choice of terminals for a prospective user, consideration is given here to a variety of terminals and terminal manufacturers. This is to provide an insight into the capabilities available today at a remote terminal. It is also intended to provide a perspective in planning future interactive systems.

## 5.2 Possible Systems

There are several general configurations which are available for remote terminals. In almost all cases the equipment can communicate with the central processor either directly or through a standard "Data-Set" communications link. A direct path to the computer is a simpler approach but restricts the distance between the central processing unit and the terminal. By using "Data-Sets" and regular telephone lines greater flexibility is available.

In order to indicate the wide variety of options which can be made available at the remote terminal, three general configurations will be presented with their advantages and disadvantages.

The configuration shown in Figure 5-1 is certainly the most straightforward approach and probably the least costly. Conversational interaction takes place via the teletype and output is on the plotter and teletype. The chief drawback to this configuration is its slow speed. The information rate

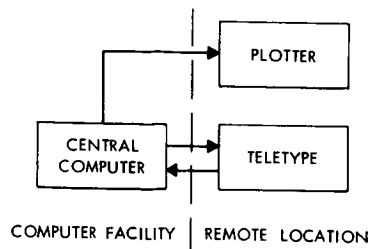


Figure 5-1. Teletype/Plotter  
Remote Station

for the available typewriter terminals is 10-12 characters/second. This means that the equivalent of one page of printer output would require on the order of 10 minutes to produce on the typewriter. The plotter shown is also a relatively slow device, a factor of importance if plots are to play an important role in the design process.

The configuration of Figure 5-2 has reduced the problem of low interactive speeds. Program output during the conversational mode of operation and throughout the intermediate design stages is on the CRT Alphanumeric display. Operator response is by means of the keyboard and graphic output is on the plotter at the remote location. Hard copy of the tabular results could be output on the line printer at the computer to be picked up later. As in the system shown in Figure 5-1, the design process can be hampered by slow interactive speeds if intermediate plotter output is required.

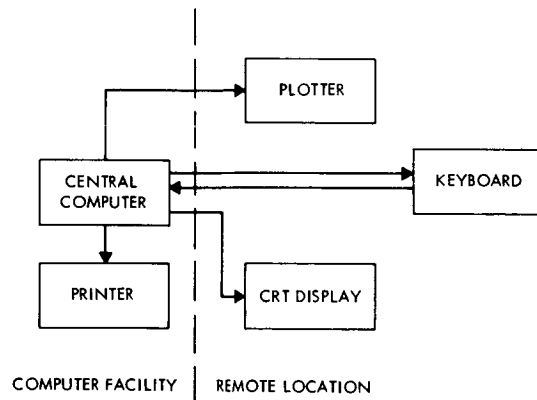


Figure 5-2. Keyboard/CRT  
Alphanumeric Output/  
Plotter/Printer  
Remote Station

Figure 5-3 illustrates the most versatile and most costly of the possible terminal configurations. Because it has its own processor and memory, it can be programmed to do a large number of tasks independent of the central computer. A high rate of interaction can be maintained through the CRT alphanumeric and graphical displays, keyboard and light pen. Hard copy can be produced on the line printer and the plotter (or photographically from the CRT display (not shown here)). Additionally a system such as this provides graphical capability perhaps desirable in later system configurations.

### 5.3 Software Requirements

Three software packages should be considered in converting the COPS/COPTRAN system into a remote, conversational system. They are: user (conversational) software, input/output software, and display software. These will now be described briefly.

Conversational software. — This programming effort would be proportional to the sophistication of the conversational language. It could require virtually no effort if user would input information in the present COPTRAN form. On the other hand, a relatively small amount of programming at the FORTRAN level will yield a system which is a great deal easier to use.

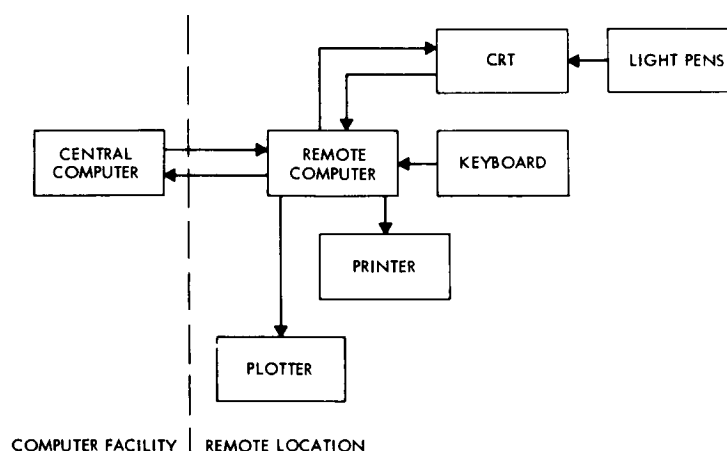


Figure 5-3. Complete Remote Graphic Processing Remote Terminal

Input/output software. — In all but the simplest configurations some amount of programming, probably at the assembly language level, will be required to interface the remote stations with the FORTRAN operating system. In some instances this will amount to routines to supply the control pulses to the devices which are not standard to the FORTRAN I/O package. In addition, encoding and decoding is required if the devices require a different bit code than that used by the DDP-516.

Display software. — Under this heading come the routines which drive the display device: CRT or plotter. They usually enable the user to specify the graphic entity to be displayed without regard to the actual control sequences which must be sent to the device. In some cases, this might also include display regeneration routines. In a large number of cases, this software can be provided by the manufacturer. In the case of the display terminal with its own self contained processor, this package can be very sophisticated.

#### 5.4 Available Equipment

Table V-I gives a brief summary of the various terminals and terminal components considered. For each piece of equipment considered, Table V-I provides the following information:

1. Brief description of capabilities and drawbacks with regard to the DDP-516 system.
2. Approximate cost (where provided by the manufacturer).
3. Type of alphanumeric input provided.
4. Type of alphanumeric output provided.
5. Type of graphic input provided.
6. Type of graphic output provided.
7. Whether or not hard copy is provided.
8. Whether software support is provided by the manufacturer.
9. Whether terminal has its own programmable central processor (thus providing a great deal of flexibility).

TABLE V-I  
EQUIPMENT SUMMARY

| Name                       | 1. Description  | 2. Approximate Cost    | 3. Alpha-numeric Input | 4. Alpha-numeric Output | 5. Graphic Input | 6. Graphic Output | 7. Produces Hard Copy | 8. Software Supplied | 9. Program-mable Remote Processor |
|----------------------------|---|------------------------|------------------------|-------------------------|------------------|-------------------|-----------------------|----------------------|-----------------------------------|
| AGT/10<br>AGT/30<br>AGT/50 | This is a family of highly sophisticated graphics terminals — very flexible and expensive. Extensive software is provided for remote processor. AGT/10 probably sufficient for conversational COPS — later version. | 60 K<br>125 K<br>175 K | KBD                    | a. PRT<br>b. CRT        | LPEN             | CRT               | Yes                   | Yes<br>Extended      | Yes                               |
| Grafacon                   | Highly sophisticated. A major item is the graphic stylus which is probably unnecessary for COPS. Does include CRT, keyboard.  | N/A                    | KBD                    | CRT                     | Stylus           | CRT               | —                     | —                    | —                                 |
| CALCOMP                    | Incremental plotter. S16 interface available but manufacturer does not yet have S16 plotting routines. These may be available from other DDP S16/CALCOMP installations.   | \$4500                 | None                   | None                    | None             | Plotter           | Yes                   | No                   | No                                |
| CC-30                      | Modular remote system designed for data phone use. Uses standard TV set for alphanumeric and graphic output.  | \$12 K<br>minimum      | KBD                    | TV,<br>PTR              | LPEN             | TV                | Yes                   | No                   | Yes,<br>limited                   |
| DEC-338                    | Provides remote graphic capability. PDP-8 computer serves as remote processor — much software available with it.  | \$56 K                 | KBD                    | CRT,<br>PTR             | LPEN             | CRT               | Yes                   | Yes                  | Yes                               |
| Friden<br>7100             | Typewriter terminal. 130 characters/line. Up to 12 characters/second.   | \$3200                 | KBD                    | TYP                     | None             | None              | Yes                   | No                   | No                                |
| Gerber 22                  | Smallest of Gerber line is 4 by 5-foot drafting table. Provides fairly high accuracy.   | N/A                    | None                   | None                    | None             | Plotter           | Yes                   | —                    | No                                |
| ASR 33                     | Teletype unit supplied with Honeywell computers. Easiest to interface. 72 characters/line, 12 characters/second maximum.  | \$1200                 | KBD                    | TYP                     | None             | None              | Yes                   | Yes                  | No                                |
| S54-00                     | Honeywell's alphanumeric CRT remote terminal.   | N/A                    | KBD                    | CRT                     | None             | None              | No                    | No                   | No                                |
| IBM-2740                   | IBM selectric remote terminal. Uses 6 bit code. 130 characters/line.  | N/A                    | KBD                    | TYP                     | None             | None              | Yes                   | Some                 | No                                |
| IBM-2250                   | IBM's sophisticated remote graphic terminal. Probably interface problems. 6-bit code.   | N/A                    | KBD                    | CRT                     | LPEN             | CRT               | Optional              | Some                 | Limited                           |
| IDHOM                      | Sophisticated graphics terminal. Versatile.   | N/A                    | KBD                    | CRT/<br>TYP             | LPEN             | CRT               | Yes                   | Yes                  | Yes                               |
| TEC-LITE                   | Small CRT alphanumeric terminal. Keyboard and function displays. Character display capability somewhat limited — to be increased this year (1968).  | N/A                    | KBD                    | CRT                     | None             | None              | No                    | —                    | No                                |

Abbreviations used in Table V-I are as follows:

CRT            Cathode ray tube  
KBD            Keyboard  
LPEN           Light pen  
N/A            Not available  
PTR            Line printer — usually 300-600 lines/minute  
STYLUS        Graphic stylus  
TYP            Typewriter or teletype printer

Table V-II provides the manufacturer's name and address for each device listed in Table V-I.

The equipment included in this survey does not constitute an exhaustive list. Rather, it is intended to be representative of the available hardware most suited for a conversational COPS/COPTRAN system.

TABLE V-II  
LIST OF MANUFACTURERS

| <u>Equipment<br/>Name</u>  | <u>Manufacturer</u>   |
|----------------------------|---|
| AGT/10<br>AGT/30<br>AGT/50 | Adage, Inc.<br>1079 Commonwealth Ave.<br>Boston, Massachusetts 02115<br>(617) 783-1100  |
| GRAFACON                   | Bolt Beranek and Newman, Inc.<br>Data Equipment Division<br>2126 South Lyon Street<br>Santa Ana, California 92705<br>(714) 546-5300 |
| CALCOMP                    | California Computer Products, Inc.<br>305 Muller<br>Anaheim, California 92803<br>(714) 774-9141                                     |
| CC-30                      | Computer Communications, Inc.<br>701 West Manchester Boulevard<br>Inglewood, California 90301<br>(213) 674-5300                     |
| DEC-338                    | Digital Equipment Corporation<br>Maynard, Massachusetts<br>(617) 897-8821   |
| FRIDEN 7100                | Friden, Inc.<br>1720 Beverly Boulevard<br>Los Angeles 26, California<br>(213) 483-4800  |
| GERBER 22                  | The Gerber Scientific Instrument Co.<br>16024 Ventura Boulevard<br>Suite 110<br>Encino, California<br>(213) 981-2044                |
| ASR-33<br>S54-00           | Honeywell<br>Computer Control Division<br>9171 Wilshire Boulevard<br>Suite 610<br>Beverly Hills, California 90210<br>(213) 278-1901 |

TABLE VII (continued)  
LIST OF MANUFACTURERS

| <u>Equipment<br/>Name</u> | <u>Manufacturer</u>   |
|---------------------------|---|
| IBM 2740<br>IBM 2250      | IBM<br>1031 North Brand Boulevard<br>Glendale, California 91202<br>(213) 246-1651                     |
| IDHOM                     | Information Displays, Inc.<br>333 North Bedford Road<br>Mount Kisco, New York 10549<br>(914) 666-2936 |
| TEC-LITE                  | Transistor Electronics Corporation<br>Box 6191<br>Minneapolis, Minnesota 55424<br>(612) 941-1100      |

### 5.5 Conclusions

Considering the stage of development of the COPS/COPTRAN system, the scale of the DDP-516, and the wide range of remote terminal accessories, it seems evident that an evolutionary approach to the conversational COPTRAN mode is the most advisable. Before examining the options for the first system, there are several general observations which should be made. First, the desired interactive rate of the system should be given careful consideration. If the design process for which COPS was designed involves a large number of iterations before a final solution is reached, then a CRT graphics system would provide results — both tabular and graphical — very rapidly. This would allow much more interaction between COPS and the designer than would a system which was typewriter/plotter oriented. On the other hand, if the terminal is primarily to provide convenience and ease of use to the engineer with few iterations in the design process, then the slower systems will suffice. The tradeoff here is cost. CRT display systems are bigger, more versatile, and much more expensive. Future demands on the terminal should not be ignored in making this decision.

Only two of the typewriter consoles and none of the CRT displays considered provided 130 character/line capability. For this reason, compatibility with present COPS output format places serious limitations on the options available. The cost of reprogramming the COPS output format statements would be small compared to that of attempting to interface an otherwise unsuitable terminal.

Almost all of the terminal equipment considered had the capability of interfacing to at least one of the Data-Sets commercially available. The DDP-516 also has that capability. Taking advantage of this fact, where possible, can reduce some of the hardware interface requirements. (This in essence makes the Data-phone line the common denominator between two dissimilar devices. Depending on the locale, however, the charge for Data-phone service may not be insignificant.)

While the COPS/COPTRAN conversational system is under development, perhaps the most prudent approach is with a terminal similar to that given in Figure 5-1: a typewriter or teletype with a plotter. There are two reasons for this choice: 1) Cost and ease of interfacing, and 2) with a small initial investment an operational conversational mode can be made operational allowing further study regarding future development of COPS systems and its remote terminal requirements.

The most logical unit to serve as the interactive device is Honeywell's ASR 33. It undoubtedly would present the least interfacing problem and could be either the existing console teletype or logically be made to appear the same. This unit does not have the ability to output 130 characters per line. If printer format compatibility is to be maintained, the Friden 7100 is probably best. There would be some interfacing problems: an interface could cost up to \$10,000 to develop. As mentioned above, the format changes to the program appear to be a relatively easy task compared to that of interfacing the Friden 7100. Hard copy graphic output would be produced on a Cal Comp plotter. The present DDP-516 system configuration does not include a plotter. A standard interface to the 516 does exist, however, and there is a strong possibility that a plotter will be added to the ERC computer installation.

Because the DDP-516 system is at the outset a graphics oriented system another option well worth considering is the use of an IDI display device (at a cost of about \$15,000). The 516 facility will have the capability to drive eight such devices. If the software and hardware are available at an early date, this could provide high interactive and display capability at the start of the development of conversational COPTRAN.

It should be pointed out that until some sort of system software is provided, program loading from a remote location will be a problem.

Full use of the computer's capability and utilization of conversational COPTRAN will be realized in a time-shared environment with the ability to service more than one COPTRAN user at a time. In deciding which directions COPTRAN development should take in the future, the following considerations should be studied using early conversational COPTRAN and the first COPTRAN terminal:

1. Optimal or desirable degree of interaction
2. Type of graphic output
3. Permanent record requirements
4. Graphic input requirements
5. Possible use for related future design needs

Judicious selection of terminal capabilities and COPS system design can result in a very powerful and easy to use design tool for communications systems.

## 6.0 CONTRACT END ITEM

### 6.1 Introduction

A required end item for contract NAS 12-566 is as follows:

- "Item 3 Evaluate and determine the follow-on mathematical analysis for the next generation of communication systems models with respect to the following factors:
- a. Optimization criteria
  - b. Required degree of model versatility
  - c. Identify the parameters and their rating of importance
  - d. Determine the applicability and specifications for future remote and batch-type computer mathematical analyses."

The purpose of Item 3 was to place in perspective the analysis which yet needs to be done with that which has been completed under the present contract phase. The documentation of Item 3 is broken into three portions, Contract NAS 12-566 Statement of Work, a list of potential tasks for a continuing phase and a potential phase III. The phase II task listing is intended to satisfy the requirements of Item 3 above.

### 6.2 Phase I (NAS 12-566 Statement of Work)

The Hughes Aircraft Company shall supply the necessary personnel, facilities, services and materials to accomplish the work set forth below:

1. Apply and extend the mathematical analysis, the technical approach, and the supporting information generated under the two (2) referenced contracts of paragraph 2 above, to the specific Electronics Research Center requirements listed below:
  - a. The mathematical analysis shall have a dual capability of providing management with a comprehensive technique for evaluating and selecting future research efforts and to provide the scientists with a detailed analysis of the value and effect of their specific research to overall space communication systems.

- b. Extension of the present analytical model and corresponding computer program to include additional parameter stops, the necessary detection methods, and fixed value parameters. Deliverable items will include the analytical model and a computer implementation in the form of a FORTRAN IV printout and card deck.
  - c. The analytical model will be continually verified as best possible using experimental data such as that of Mariner IV.
  - d. The mathematical analysis must have a flexible input/output capability to optimize its utility to both management and the researchers and to fully exploit the latest technology of computer graphics and dynamic presentation.
  - e. The specific parameters for optimization by the mathematical analysis shall be determined to provide the maximum utilization by both management and the researchers.
  - f. A sensitivity analysis shall be performed concurrent with the primary mathematical analysis. The sensitivity of the systems response to each parameter variation is to be analyzed and, if possible, this sensitivity analysis is to be integrated into the mathematical model such that it will be an additional feature aiding in the identification of the most fruitful parameters upon which to work. Graphs of the effects of the more sensitive parameter variations will be included in a special report.
2. Investigation of an executive model will be done. The essential ingredients of this investigation will be tailoring the model to the equipment and personnel who will be making use of it. This requires substantial analysis of the variety of forms which the output might take. The steps required for implementation of the executive-decision making model will be delineated. This task will consist of examining a number of possible methods of implementation with appropriate recommendations included in the final contract report. A specific task will include the investigation of the desirability and the significant factors of remote computer applications in the control of the mathematical analysis, and determination of the

interface with a batch-type analysis. This investigation is to consider the following factors:

- a. Technical management usage
  - b. Engineering and scientific usage
3. Evaluate and determine the follow-on mathematical analysis for the next generation of communication systems models with respect to the following factors:
- a. Optimization criteria
  - b. Required degree of model versatility
  - c. Identify the parameters and their rating of importance
  - d. Determine the applicability and specifications for future remote and batch-type computer mathematical analyses.

### 6.3 Proposed Phase II

1. Model Refinement, Versatility

The following items of model refinement and versatility apply to the existing deep space communications system analysis. In general, they add to, and build upon that which has already been documented and put to use.

a. Inclusion of PPM

Pulse position modulation (PPM) for laser communications represents an attractive implementation for transmitting data from deep space. This is due to the high efficiency of detectors available at frequencies where this type of modulation might be used (near IR and visible spectra) and the transmissivity of the atmosphere at these frequencies. In addition, this means of transmission is effective since all the energy of the laser beam, is transmitted in a very narrow time interval during which there is very little background radiation.

The present COPS program is partially implemented to perform the type of communication analysis needed for PPM, in the subroutine known as SOPS. However, further refinement is needed to assure a true optimization is performed in this subprogram.

b. Documentation of Basic Program Mathematics

The basic concept used for deep space communication optimization programs have been partially documented in previous reports completed under contract NAS 5-9637. A complete documentation has not yet been made. Since a great deal of building has been done upon this foundation, it is felt wise that an adequate documentation be made such that future investigators may be able to follow the original derivations.

c. Visit Recognized Authorities to Check Burden Values

The burden values used are the result of literature searches and personal contacts of those who are recognized to have significant information on particular communication parameters. In order to have an "unbiased and agreed upon" set of parameters, it is proposed that a series of personal contacts be made to those in industry and NASA. Once these parameter values have been included in the present program, this program can be called upon to provide unbiased outputs.

d. Implement a Discrete Point Input Program

Burden relationships for the various communication parameters are presently represented by an equation describing their relationship against the given parameter. An alternate form of providing the burden data to the computer would be to provide discrete points relating burdens and the parameter value. This task would implement such an input program.

e. Program "As a Function of Frequency"

It is desirable to know the frequency relationship of various levels of performance in the communications optimization program. While it is not possible to represent such a program on a continuous frequency basis, due to the discrete limitations of certain parameter values, it may well be possible to represent many parametric relationships as a function of frequency and to express other frequency dependencies over a limited frequency range. This task will investigate these several possibilities.

- f. Represent Parameter Burden by More Than Three Constants  
The basic parameter burden relationship consists of expressing the burden in terms of a fixed constant, a multiplicative constant, and an exponential constant. This representation is undoubtedly an over-simplification in many of the parameter values. For instance, the acquisition and tracking weight is not a simple function of the diameter of the aperture used, for fine pointing and coarse pointing may provide accuracies which are relatively independent of their weight. The importance of representing parameters by more than three constants may be seen in the case of a rather complicated parameter such as, the cost of a large ground array. If a more representative burden model is made it may well show that one feature of the large array is a dominant feature in the overall burden. This would allow this isolated feature to be examined in greater detail before committing a large development effort to the complete receiving array. This task would analyze several parameter burden relationships.
- g. Investigate Certain Promising Techniques  
The sensitivity analysis completed during the first quarter of contract NAS 12-566 has shown several areas which are sensitive to inaccuracies of the burden constants. In addition, certain promising techniques have been proposed to implement various parameters. It is proposed that several of these be investigated further. Those technology areas to be investigated are: solid state microwave sources, antenna arrays, and power supplies.

## 2. Executive Model

Contract NAS 12-566 has developed an executive model for the existing program. This model is in the form of a simple user's handbook and batch computer processing (see Section 4.0). The proposed Phase II effort will include the following.

- a. Develop a Specific Executive Model No. 1  
Executive Model No. 1 is envisioned as the on-line remote teletypewriter used with the COPTRAN Program.
  - b. Develop a Specific Executive Model No. 2  
The Executive Model No. 2 is envisioned as a means of using the deep space communications optimization program with greater facility than that developed in Executive Model No. 1. It is also expected that this model will be designed to be used in conjunction with a specialized console. Such a console will form the interface between a user, who is not familiar with computer programming or computer language, and the computer program.
  - c. Develop an Executive Check  
The present computer program optimizes parameter values on the basis of minimizing the cost of the system or minimizing the weight of the spaceborne components. The cost optimization, in effect, provides the cost of developing a certain system. In many cases only relative cost values are important to the user. However, in many cases absolute values are of definite concern. It is recommended, therefore, that a method of checking these optimized values be determined. Such a method could be implemented by having a commercial company perform a pricing task for the check. Since this pricing is only a check and is not a bona fide request for proposal, it would be incumbent to have this clearly understood and have appropriate remuneration be made to the company making such a check.
3. Console for Executive/Computer Interface  
The deep space communication optimization program represents a very complex and detailed computer implementation. It has been a major purpose of contract NAS 12-566 to enable a person with a minimal amount of computer implementation and user knowledge to use this analysis effectively to solve problems of direct interest. Some features of the executive model and model refinement have been previously mentioned. These include such features as

implementation of discrete input points and the use of a simplified user's guide. There seems, however, a highly desirable step which may yet be taken. This step is that of implementing a specialized console with appropriate input and output displays and with appropriate controls to modify easily various parameter values. In addition, this console would enable any portion of the program (such as a particular burden relationship) to be recalled and be displayed appropriately. It is proposed that a design of such a console for executive/computer interface be included in the Proposed Phase II schedule.

4. Review Optimization Criteria

The present optimization criteria is one of weight optimization for spaceborne components or of cost optimization for the entire data link. Other criteria have been suggested but none have seemed immediately amenable to either the stated desires of the user or the present implementation of the optimization.

A proposed optimization criteria that may be useful is that of a reliability/cost interrelationship. Since reliability may always be increased by increasing cost, it, by itself, does not have an optimum value. However, by relating reliability to cost, an optimization may well be achieved which is meaningful both in view of the program and in view of the user's desires. A second factor which should be considered in the optimization review criteria task is that of expected response from the user during the first portion of the Proposed Phase II. Once users have begun to use the program they will undoubtedly request other types of criteria. These criteria suggestions will have to be evaluated for their general usage and worth to the overall objectives of the program. For these reasons this task has been included.

5. Deviation Analysis

The cost burden of individual parameter values has been delineated. If certain "stops" are included, the overall system cost has been found to increase as expected. A sample of this type of analysis

has been given in the paper by Ross E. Graves titled "Techniques for Planning R&D for Deep Space Communications" and included as Appendix C of the Interim Technical Report of contract NAS 12-5'6. A similar type of analysis could be given on other parameter values to determine the relative merit of extending the state of the art these parameters. Such is the purpose of this task.

#### 6.4 Potential Phase III

1. Study Antenna Arrays

The implementation of large antenna arrays, whether they be flat arrays or parabolic dishes connected as arrays, is an extremely complicated task. It includes interrelationships of area and antenna temperature, as well as other technical and economic considerations. A detailed task description for the study of antenna arrays is presently being prepared. This will be forwarded to NASA-ERC by February 16, 1968.

2. Studies of Individual Parameter Representation

This potential task represents an extension of a similar task mentioned in Task 1f of Proposed Phase II above. At the completion of the Proposed Phase II tasks, it is anticipated that further study of this nature would be in order.

3. Console for Executive/Computer Interface

The purpose and general design concepts for a console for executive/computer interface has been described under Proposed Phase II Task 3 above. The purpose of the task being listed in Potential Phase III is that of actually constructing the console.

4. Develop Certain Components

As a result of the deviation analysis (see Task 5 of Proposed Phase II) several components will undoubtedly be isolated as those whose further development would significantly extend the communication capability for deep space. It is proposed that these components then be developed in individual development efforts.

TABLE VI-I  
ANALYSIS FOR DEEP SPACE COMMUNICATIONS

| Phase I NAS 12-566  | Proposed Phase II  | Potential Phase III   |
|---|--|---|
| <p>1. <u>Extend Math Model</u></p> <ul style="list-style-type: none"> <li>a. Method of evaluating and selecting future work</li> <li>b. Additional stops, detection, fixed values, deliver a FORTRAN deck</li> <li>c. Use actual experimental data</li> <li>d. Flexible input/output</li> <li>e. Optimization criteria</li> <li>f. Sensitivity analysis</li> </ul> <p>2. <u>Investigate Executive Models</u></p> <p>Look at possible output forms, list steps for getting an executive program. Recommended approach</p> <ul style="list-style-type: none"> <li>Investigate remote computer usage</li> <li>Investigate batch usage</li> </ul> <p>3. <u>Evaluate Follow-on Math Analysis</u></p> <ul style="list-style-type: none"> <li>a. Optimization criteria</li> <li>b. Model versatility</li> <li>c. Parameters and their importance</li> <li>d. Applicability and specifications of future remote and batch analysis</li> </ul> | <p>1. <u>Model Refinement, Versatility</u></p> <ul style="list-style-type: none"> <li>a. Inclusion of PPM (1.06, 0.84, 0.51μ)</li> <li>b. Documentation of basic mathematics</li> <li>c. Visit recognized authorities to check values used</li> <li>d. Implement discrete point input program</li> <li>e. Represent parameter burden by more than three constants</li> <li>f. Investigate certain promising techniques</li> </ul> <ul style="list-style-type: none"> <li>Solid state microwave sources</li> <li>Antenna arrays</li> <li>Power supplies</li> </ul> <p>2. <u>Executive Model</u></p> <ul style="list-style-type: none"> <li>a. Develop a specific executive model No. 1</li> <li>b. Develop a specific executive model No. 2</li> <li>c. Develop an executive model check</li> </ul> <p>3. <u>Console for Executive/Computer Interface</u></p> <p>Design a console for executive/computer interface for executive model No. 2</p> <p>4. Review optimization criteria</p> <p>5. Deviation Analysis — What it is worth to extend state of the art in certain technology areas?</p> | <ul style="list-style-type: none"> <li>1. Study ground antenna arrays</li> <li>2. Studies of individual parameter representation</li> <li>3. Console for executive/computer interface</li> <li>4. Develop certain components</li> </ul> |